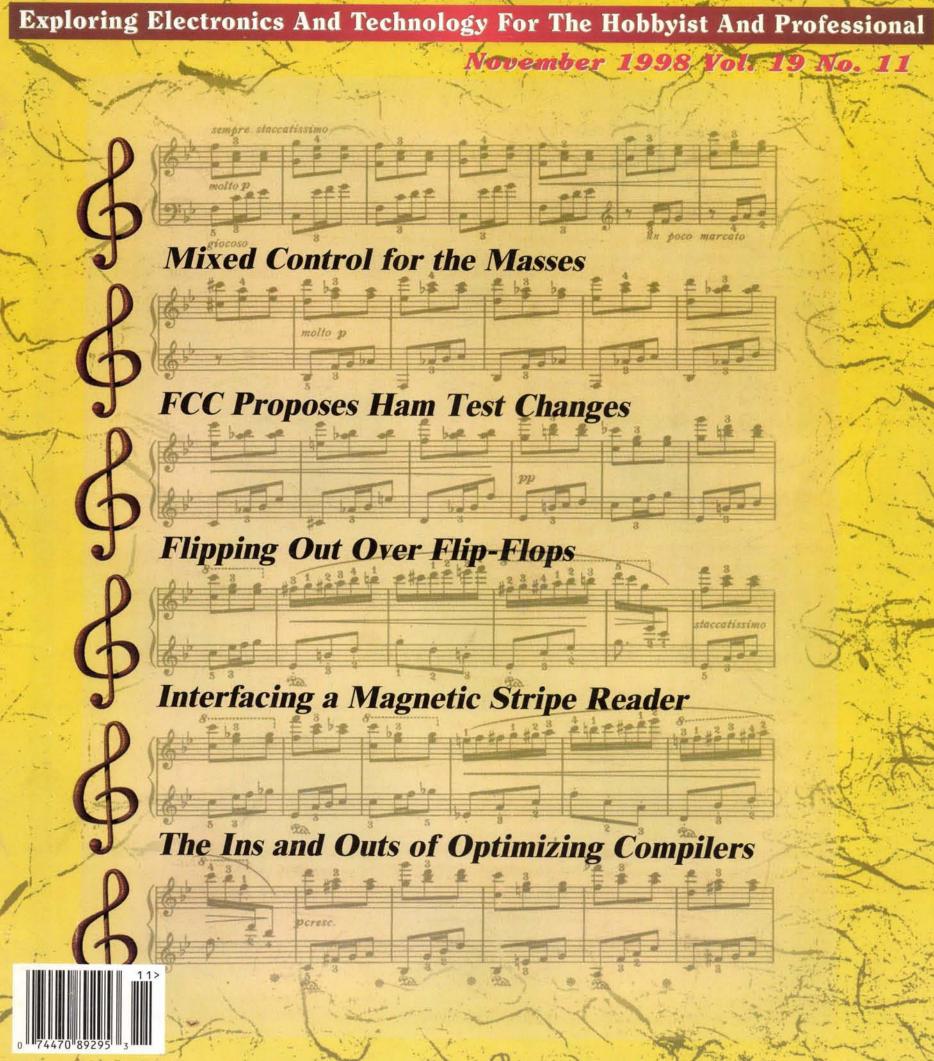
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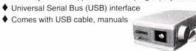
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power input (we do not have the adapter), and on the fro

Note: HP and Logitech will provide no information on these

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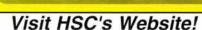




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DATA INTERFACE ADAPTERS

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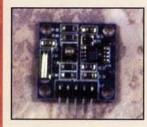
Two adapter models are provided to suit either the older NMEA or the latest NMEA specs.

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Nuts & Volts Magazine encourages article submissions and queries. Send a SASE for a copy of our writer's guidelines. All submissions should be on 5-1/4 or 3-1/2 inch diskettes and include hard copy as well. If return of materials is requested, include a SASE with your submission. Deadlines should be discussed in advance with the editor, but generally all material should be submitted two weeks prior to the 1st of the month for the next month's issue.



Gordon West WB6NOA says
"Write the FCC with your comments about the proposed rule
changes for ham testing today!"

The comment period closes on December 1st!!

Check out Santa's Special on page 96!!



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and EVERYONE interested in obtaining an amateur radio license are flooding the Federal Communications Commission (FCC) with comments about proposed rulemaking that could dramatically change ham test requirements. At the same time, amateur radio's largest non-profit steering organization the American Radio Relay League (ARRL) founded in 1914 - proposes the retaining of the no-code VHF/UHF license, and dropping the Morse Code telegraphy examination in speed for General class from the present 13 wpm down to five wpm. And, until the Morse Code requirements on an international basis ultimately go away, No Code International also recommends dropping the Morse Code test speed for General class down to a simple five wpm exam.

mateur radio operators

"No Code International would like to see CW testing for all classes of amateur license to a five wpm speed," comments Fred Maia W5YI, Executive Director. "NCI does not at all oppose the USE of Morse Code in the amateur bands by those amateurs who choose to use it in that mode ... we just don't believe that Morse Code is an important enough factor in today's communications world that it should be a licensing criterion at any level beyond the absolute mini-

mum required by international regulations," adds Maia. Ultimately, NCI stands for the complete elimination of Morse testing for all amateur licensing.

THIS ONE IS FOR REAL

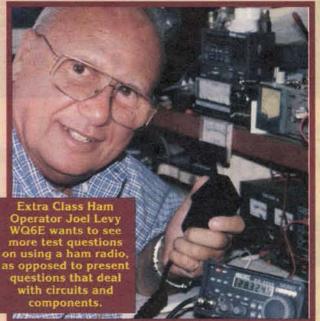
Every couple of years different organizations propose dropping code test speed requirements to the FCC. The ARRL will usually conduct a survey and normally reports back that this is an unpopular idea to change CW test speed requirements, and ultimately the FCC does nothing.

But this one is for real - the FCC has put the amateur radio service within its 1998 biennial Regulatory Review, and has officially released a Notice of Proposed Rulemaking Docket No. 98-143 to streamline the service and eliminate unnecessary and duplicative rules as they might effect ham testing. And this is not just an FCC Notice of Inquiry this is the real thing - Notice of Proposed Rulemaking where the FCC has put the amateur radio service on "fast track" and could get new rules in place by the first FCC PROPOSES HAM
TEST CHANGES

by Gordon West WB6NOA

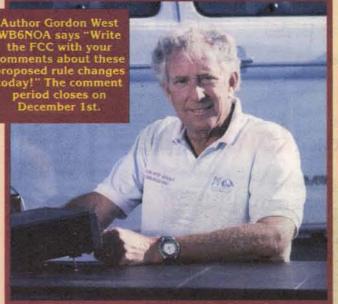
of next year.

The FCC proposes to modify the amateur



Most hams were surprised that it was the ARRL who came out first with a proposal to drop General class and Extra class code test speeds. Everyone knew that the FCC was soon to come out with some big changes for ham radio, and we all expected that the ARRL would wait until the NPRM was issued before they came up with a counter-proposal. So, approximately 30 days before the FCC NPRM, the ARRL decided on the recommendation of four classes of licenses, and a drop in the General class code speed from the present 13 wpm down to five wpm. They also suggested that the highest license — the amateur Extra — would require a code speed of only 12 wpm.

"Board members at the ARRL emphasized that the objective is to rationalize the amateur license structure without reducing their requirements for any class of license," comments the ARRL in their announcement. "Where reductions in Morse Code requirements are proposed by the League, there would be a corresponding increase in written examination standards." The Board members were adamant that simplifying the structure should not come at the expense



radio service rules as follows:

1. Reduce the number of license classes from six to four.

2. Provide greater opportunities to volunteer examiners (VEs) to participate in the examination process — in other words, make some changes to code and theory tests.

3. Eliminate Radio Amateur Civil Emergency Service (RACES) licenses because the emergency communications that are routinely transmitted by RACES stations can be transmitted by primary, club, or military recreational stations.

4. Finding out ways for improving the enforcement processes as they relate to amateur radio.



of privileges already earned by ham operators.

The ARRL also recommended renaming the classes of amateur radio license to classes A through D. Class D would be the present nocode Technician class license, and Class A would be the Extra class license. The slow-code five wpm General license would be Class C, and the Advanced class license would be Class B.

"We were surprised on how many negative comments we received regarding renaming the amateur licenses as ham Class A through D," comments ARRL President Ron Stafford W6ROD, at the recent ARRL Southwestern Division Convention. At the convention, most hams were quite upbeat with positive comments on the reduction of their General class code speed from 13 wpm down to five wpm

which would turn many entry-level hams into worldwide-band ham operators. Amateur operators already holding a five wpm certificate for Novice or Technician-plus would probably just take one or two more written exams to advance up to General class with no other code test required.

WHAT THE FCC DIDN'T SAY

But most surprising to seasoned ham radio operators was the FCC saying absolutely NOTHING about a specific code speed change for General class or Extra class. Rather, the FCC indicated they will take their incoming comments from hams as a good way to finally announce any code test or written test changes.

And here are some of the points that the FCC raised to solicit comments from hams and

non-hams on how the amateur tests would be structured in the future:

A. The present six classes of amateur license would be streamlined into four classes. The FCC was rather firm in indicating it will probably phase out the Novice license, as well as the five wpm Technicianplus class, leaving only the entry-level no-code Technician class. The present no-code Technician class is a popular one, and hams can get on the air above 50 MHz by simply completing two written

exams. Under the new rules, just one written exam would probably be administered for Technician class.

To get to the worldwide General class license, all that would be necessary is a code test and one more additional written General class exam. In fact, under the ARRL proposal, the ONLY way a new ham could get on the worldwide bands would be to pass the five wpm, and ALSO pass the General written test. The restricted operation on Novice CW frequencies

would go away, and also would the Technician-plus test for maybe coming up on a portion of the 10meter phone band.

Under the ARRL proposal to the FCC rules, only five wpm and passing one more written test gives you EVERY worldwide General class band. And you won't be restricted just to one or two bands - with five wpm and the General theory test, you can operate on General class segments of EVERY worldwide band, plus unlimited access to all frequencies above 50 MHz.

Now don't panic if you are already a Tech-plus operator or a Novice operator, chances are you won't lose any present privileges. Good news for you - since you

already have the five wpm satisfied, just a simple written examination and you could very well be turned into a grandfathered General class

But the FCC does not go as far as the ARRL in saying dump the code speed. "We seek comments on all aspects of the Morse Code standards used in our examinations," writes the FCC in Point #24 of their NPRM. "Do the three levels of five, 13, and 20 wpm remain relevant to today's communications practices? Should we continue to have three different levels, or should these be reduced to one or two - and, if so, what should be the required speed?" asks the FCC. They also indicate they are looking for comments on whether or not they would add elements to the written examination to insure a working knowledge of newer digital technology which, in part, is replacing the Morse Code.

The FCC also asks whether or not the code test of copying one minute out of five perfectly is appropriate. They ask whether or not the volunteer examiners could determine how to test for code speed. They suggest that volunteer examiners accredited by a volunteer examiner coordinator could take a greater role in the examination process, not necessarily restrained by specific FCC rules.

e almost anywhere!

At the recent Southwestern Division ARRL Convention, a 12year-old Technician-plus ham recounted his story about being tested by a local VEC where he missed passing the General class exam by having a single letter error in one minute of

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perfect copy. He told me there were several places in his copy where he copied almost perfectly, but it didn't quite add up to the required 64 letters in a row. I am surprised that the volunteer examination team didn't take an overall look at the entire copy, and come up some sort of comprehensive test where this young lad would certainly pass. After all, he knew the content of the code at 13 wpm - he just didn't write

it down letter perfect. Give me a

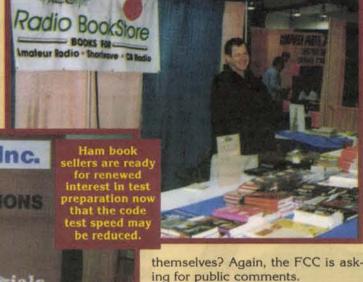
B. GREATER VOLUNTEER EXAMINER OPPORTUNITY. The FCC is suggesting that Advanced class operators be able to administer General class testing. The ARRL also recommends this, so we think that this will probably go through without any negative comments. The FCC and ARRL agree that ham operators who have passed a specific class test should be able to become certified through a participating volunteer exam coordinator and administer the same type of test that they have successfully passed.

But there IS some heated dis-

cussion about amateur operators who have been issued code test certificates of completion based on a handicap physician's statement. The discussion is about an alarming rate of handicap statements coming through without the FCC having the time and staff to actually verify the physician's report. Volunteer examiners are concerned that there is no

verification of the physician's statement, and they ask how can these operators administer code tests if they aren't

able to copy the code



ing for public comments.

The scope of the volunteer examiner might also be expanded to allow that examiner to specifically tailor written and five wpm examinations to very young and very old candidates. Presently, the ARRL VEC allows examiners to take age into consideration when conducting code and written tests. Yet, the rules are clear that written questions and the four distractors may not be varied by the examination team. The FCC raises the point on whether or not volunteer examiners may take a more interpretive look on how a candidate is suited for passing or failing

The FCC also suggests that new testing procedures could be implemented - maybe submitting a log book for upgrades to insure they have worked so many contacts before they next go higher up the ham radio upgrade ladder. Or, for new students, maybe home study where a local "elmer" may help sign off certain requirements before the written and code test. The FCC suggests we all take a look at ham testing, and come up with more creative ways to make our ham service more attractive to beginners.

C. RACES. In the FCC NPRM, they are suggesting eliminating the specific RACES license. But, if you are a member of RACES, don't hit the panic button - they don't want to eliminate the RACES service, only the formality of having a special license for a RACES station. RACES operation would continue as normal.

D. VIOLATION ENFORCEMENT. The FCC is in agreement that prosecution of radio violators is next to minimum on the ham bands. This is because all of the FCC efforts are more directed to safety of life violations - such as catching the bad guys jamming aeronautical frequency 121.5, or coming up on a local paramedic channel and asking for 10 grams of cocaine to be delivered to a specific address. They are also busy tracking down police radio jammers, as well as the idiot using a marine VHF on Coast Guard Channel 16 and repeatedly calling "Mayday, Mayday, Mayday. I have run out of beer."

This means that CB radio and ham radio, including most routine land-mobile radio systems, go unmonitored. When they do get proof of a rule violator, they generally don't have the resources to start any enforcement action. The FCC asks what might be done to get them out of the loop, and to have enough evidence that might go directly into the court system. All you

attorneys, here is your time to help reshape ham radio enforcement. The FCC is asking how this might be done.

F. WRITTEN TESTS. The FCC asks hams to take a more active part in redesigning the written examination. Should we come up with more questions on digital techniques, replacing the high-speed code requirements with more written digital questions? And how should these questions be administered - fill-in-the-bank, multiple-choice, or essay? The FCC wants as much input from hams as possible.

G. The FCC will also dispose of other smaller petitions that have been hanging around their office for years. Maybe they'll find mine where I suggest lifting the old ham radio rule that says a marine single-sideband radio shall not be used as a ham radio. The new technology of marine SSB equipment makes marine sideband radios perfect for both purposes without any necessary modification that could injure their operation on distress frequencies. One radio for two purposes makes good sense to me!

CONCLUSION

"Here at the FCC, we propose (1) to phase out the Novice class operator license and Techplus operator license; (2) to authorize Advanced class operators to prepare and administer General class operator license exams: and (3) to sunset RACES station licenses by not issuing any license renewals.

We invite comments of the amateur community with respect to improving our enforcement processes as they relate to amateur radio. We also invite comments regarding the specific telegraphy speed requirements for the various license classes, and comments on ways to

streamline and improve the operator written examinations," comments the FCC.

HERE'S HOW TO COMMENT

First, the date is right around the corner where your comments might go in the trash bin. Get your comments to the FCC BEFORE December of this year. Just days away.

The easiest way to file comments is through the FCC's electronic filing system (EFS). Comments filed through the EFS can be sent as electronic file via the Internet to http://www.fcc.gov/e-file/ecfs.html. Only one copy of an electronic submission must be filed. You may also submit an electronic comment by Internet E-Mail. To get filing instructions for E-Mail comments, commentors should send an E-Mail to ecfs@fcc.gov and include the following words in the body of the message ... "Get form - your E-Mail address."

You can also file by paper, submitting one original and six copies of your comments. File to FCC, Commission Secretary Magalie Salas, FCC Building, 1919 "M" Street, N.W., Room 222, Washington, DC 20554.

You can also choose to file on diskette. Diskettes should be submitted to N.J. DePont. Public Safety & Private Wireless Division, Wireless Telecommunications Bureau, Room 8332, 2025 "M" Street, N.W., Washington, DC 20554. Word Perfect 5.1 for Windows or compatible software, please.

You should also send your comments to the ARRL They will ultimately see them, and may offer a reply to your comments. But if you work closely with the ARRL now, you can help strengthen your agreement on what each of you will ultimately say. You can file your thoughts with www.arrl.org.

You can also look at the NRPM on the ARRL web page at http://www.arrl.org. You can also download it from the FCC at www.fcc.gov and follow the instructions to receive WT Docket 98-

Whether you are a ham radio operator or not, WRITE THE FCC WITH YOUR COM-MENTS! Get your thoughts down on paper or on computer, and get them into the FCC today.

I will look forward to reading your comments soon. NV

REQUIREMENTS FOR AMATEUR LICENSES UNDER THE ARRL PROPOSAL Level of Difficulty Same as present Technician

License Class Class D Upgrade from D to C Upgrade from C to B Element 4A (Advanced) Upgrade from More advanced technical

Written Exam Morse Exam Operational and technical None questions relevant to VHF/UHF

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STAMP by Jon Williams APPLICATIONS

Putting the Spotlight on BASIC Stamp Projects. Hints. and

Timing Is Everything

One of the regular pokes taken at the Stamp is its lack of interrupts. A fair complaint perhaps, but not all micros have them and quite a few products are built with micros that don't. With a little bit of programming discipline - and a helpful second Stamp - we can write code that emulates a software interrupt.

recently converted a PIC-based (16F84) project to the BS2. The trickiest part of the conversion was the way I monitored the four sensor (switch) inputs. In the PIC, I have a software interrupt that causes the inputs to be scanned several times per second. With no interrupts in the BS2, I had to use a different method.

It's simple, but not necessarily easy. The main code loop has to be fine-tuned so that no matter what path it takes, its execution time is always the same. Geez, how do we do that? The truth is that the process can be very tricky, especially with complex code (so we'll keep our demo simple). I believe the easiest way to write such a program is by creating a state machine. PBASIC makes this very easy with the BRANCH command.

Let's say we want to monitor a couple of inputs and, if each is active beyond some threshold, we take an action. This doesn't sound like a big request, does it? So how would you pull it off? The way that I chose to do it was by monitoring the inputs at a regular interval. If the input is active, a counter is incremented; otherwise, it's cleared. If the counter exceeds a given threshold, then some action is taken. The upside of this technique is that the inputs are debounced by

Listing 1 is a very simple demo using a Stamp II and the Parallax BASIC Stamp Activity Board (BSAC). Two switches (on pins 8 and 9) are monitored. If either of the inputs is held long enough, a corresponding LED is lit (in addition to the input LED). If both are lit at once, they are flashed.

Take a look at the code. What you should notice is that the subroutine **ChkSw** is always run through each execution of the loop. By trimming the loop timing so that it's constant, we're able to write our processing code based on predictable behavior. In this case, each run through the loop is about 100 milliseconds. So, to alarm on a two-second input, the input would have to be active for 20 iterations through the loop (20 * 100 ms = 2 seconds).

You might be wondering why I chose to use a loop in ChkSw with only two inputs. The reason is that it makes the code very easy to expand, even if it does make it a little tricky to time. There are a couple of PAUSE commands inserted in this code to make the timing as even as possible, regardless of the state of the inputs.

Another thing that I did was use a nibblesized variable for the alarm state. This technique will give you the ability to have differing alarm levels. As an example, a BS2-based product I developed (and upon which this demo is based) has a secondary threshold for each channel. By monitoring the alarm state for each channel, I was able to set the alarm threshold accordingly.

the Okay, code works, so how do we finetune the timing? Some assembly

language programmers actually go through the arduous process of counting machine cycles. Thankfully, we don't have to do that. What we're going to do is use a spare pin on our project to talk to another Stamp. The second Stamp will measure our code and display the timing on a Scott Edwards serial LCD.

Listing 2 is a program that performs the measurement. The code measures a high pulse on pin 15. Since the resolution of PULSIN is two microseconds, dividing by 500 gives us milliseconds - a timing unit that's a little easier to deal with. Keep in mind that this program is designed to measure short evens. Due to the constraints of PULSIN, the maximum duration that can be measured is 131 milliseconds.

Once you've connected the timing Stamp to your project, you'll need to isolate the section under test. With the section isolated, place the line HIGH x at the beginning of the section and LOW x at the end of the section (x is the pin number). So long as the fragment is within the limits of PULSIN, the time will be displayed on the LCD.

In the demo, ChkSw takes about nine milliseconds to run. I added a couple of pads (PAUSE statements) to keep things as even as possible, regardless of the inputs. With that done, each state routine is checked and padded so that they're equal. With the state processes equal, the last thing to do is pad the main loop to achieve

Nuts & Volts: Stamp Applications, November 1998		[Variables]	
File STATE.BS2 Purpose State machine framework Author Jon Williams E-mail jonwms@aol.com WWW http://members.aol.com/jonwms Started 03 CCT 98 Updated 04 CCT 98	state tics alarm swMax x o test	VAR Byte VAR Byte(2) VAR Byte(2) VAR Byte(2) VAR Byte VAR Byte VAR Byte	Listing 1
[Program Description]		[Initialization	
This program demonstrates the general operation of a purpose is to monitor and debounce several inputs wi precision (emulating a software interrupt-based proc	a state machine. Its '	DirC = %1100 state = 0	
Run the program on a Parallax BSAC		LEDO_ = Off LED1_ = Off	' start with LEDs off
[Revision History]		tics(0) = 0 tics(1) = 0	clear the input counters
		alarm(0) = Off alarm(1) = Off	· alarms clear
[I/O Definitions] WO_ VAR		swMax(0) = 20 swMax(1) = 50	' alarm on 20 "tics" (2 sec) ' alarm on 50 "tics" (5 sec)
EDO VAR Out10 LED outputs ED1 VAR Out11		[Main Code]	
[Constants]	Main:	' HIGH 0 GOSUB Chksw	
n CON 0 ractive low	output	' process the curren BRANCH state, [Proc0,1 COTO Main	

LEDO_ = alarm(0) Proc0: ' update the LEDs LED1_ = alarm(1) PAUSE 50 ' pad to simulate other code GOTO NXLSt test = alarm(0) + alarm(1)
IF test > 0 THEN Plx
LEDO_ = Off
LEDI_ = Off
PAUSE 50 Proc1: if both on, flash Plx: GOTO NXtSt ' do something else PAUSE 51 GOTO NXtSt NxtSt: ' main loop timing trim state = (state + 1) // 3' update the state LOW 0 ' end of timing pulse GOTO Main ---[Subroutines]-----ChkSw: ' check the state of the input switches FOR x = 0 TO 1 loop through inputs BRANCH x, [CS0, CS1] IF Sw0_ = OFF THEN SWNO CSO: CS1: IF Swl_ = OPF THEN SwNo GOTTO Swyes SwYes: PAUSE 1 ' timing trim ' update input counter tics(x) = tics(x)+1tics(x) < swMax(x) THEN SwNext alarm(x) = On 's ' set alarm for input · start new counter tics(x) = 0GOTO SwNext SwNo: PAUSE 2 ' timing trim ' clear the alarm bit alarm(x) = Off' reset the input counter tics(x) = 0SWNext: NEXT RETURN

the desired loop timing (100 ms).

website - www.arlabs.com

How long will trimming a program take? Obviously, that depends on the complexity of the program. And sometimes the process will seem like voodoo. I've found it helpful to make a copy of the program to extract code fragments for test. This prevents me from wrecking an otherwise working program.

Just remember that the purpose of this design style is to emulate a timed software interrupt process. If you need to deal with spurious events, stretch the input(s) with a one-shot (a 555 will do) so that you can see the event when you run your pseudo-interrupt process.

Serial Follow-Up

Every time I work on a project that involves the Stamp communicating with a PC, I'm reminded of Roger Arrick's Arrick Robotics) E-Mail tag line: It's harder than it looks. No kidding. I've done two Stamp designs recently that get set-up data from the PC. I thought I'd share what I've been through - perhaps I'll save you a bit of frustration in your projects.

I'm using Visual Basic to develop the PC side of my projects. One of the points that I want to reiterate is to use text mode (versus binary mode) with the MSComm control. Why? It's just plain easy. You take your data and convert it to a string (with Chr\$(x)) to send it. On receipt, you get a string back that can be parsed and converted with Asc(x). Simple, right? You bet. I'm sure there's somebody that will disagree with me, but I've found the binary mode a nightmare and just

plain choose not to use it.

MADE IN THE U.S.A

Recently, I had a short conversation about the merits of text versus binary with Jan Axelson. She expressed some concern that some bytes might not convert properly (since VB stores strings with Unicode). We independently ran experiments and concluded that this was not the case.

Just to be safe, you should run your own test, especially if you run a version of Windows that is not a western language (i.e., Japanese or Chinese).

On my end, I created a simple application that sent the value of a spin control to the Stamp.

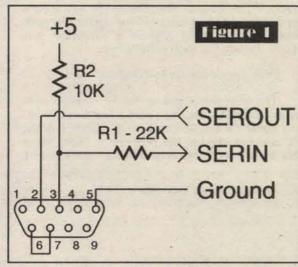
The Stamp program simply waited for the byte and sent it back. A quick check on the transmitted versus received bytes was enough to convince me that text mode would work with my projects.

One of my designs uses the BS2 programming port as the serial connection. I feel a bit like a dope for only recently noticing that the Stamp was echoing anything sent to it. The echo is caused by the hardware design of the serial connection. Take a look at the BS2 schematic in the Stamp manual. Notice the resistor connected between the transmit and receive lines? That's the culprit. It's not a problem though, especially since VB includes some nice string functions.

For example, you want to send a two-byte command to the Stamp and expect a response that is eight bytes long. What you'll want to do is wait for 10 characters to show up and strip the first two (the echoed transmission) with the Mid\$() function. The resultant string can be parsed to extract the Stamp's data.

One of the nice aspects of the BS2 SEROUT function is the optional pacing parameter. Unfortunately, VB doesn't have such a facility. There will be times when you'll want to insert a delay between the characters sent to the Stamp. I borrowed some code from Jan's book, Serial Port Complete, to perform a delay. Delays are particularly important when the Stamp needs to do some sort of processing between PC transmissions. Just keep in mind that you might need to adjust your SERIN timeout value if the PC has a delay on its end.

Enough chitchat, let's look at a program (Listing 3). I developed this project — EEMover — as a test-bed for uploading and downloading



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parameters from the Stamp. It also gave me a chance to work with polling versus interrupt reception in VB (we talked about that in the StampNet 1 project).

Let's look at the Stamp side first. Set-up parameters are stored in the first 64 bytes of the Stamp's EEPROM (note that for this demo program the data is completely arbitrary). After this data block is a three-byte revision code that will not be overwritten. Its purpose is to identify the code and features of the attached controller.

The first thing the program does is check to see if the PC is connected. This is accomplished by looking at the state of the receive line. Take a look at Figure 1. As you've seen in many Stamp projects, R1 limits the current into the Stamp from the RS-232 connection. The purpose of R2 is to pull the line high (1) when nothing is connected. As soon as you connect a PC, this line will go low (0). In my production project, I look to see if a PC is connected and jump the code that allows set-up parameters to be changed. Even if you don't need to detect a PC, it's good practice to tie the input line to Vcc or ground. This will prevent noise from causing a false start bit on a floating input and corrupting your serial input.

Back to the demo. Once we see the PC, we wait on a start byte (\$FF) and a command. It's a good idea to use the timeout parameter so that your program doesn't hang up if something goes wrong. In this case, we simply loop back to the beginning and look for the PC again. After the start byte and command arrive, the command is converted to a cleaner format with LOOKDOWN. and the program BRANCHes to the code that's appropriate for the command received.

The first possible command is the general query. This causes the Stamp to return the embedded revision code. Once again, the code takes advantage of PBASIC's symbolic constants. Notice the loop control line:

FOR addr = RevCode TO (RevCode + 2)

The loop reads and sends the revision code bytes to the PC. The nice part about this is that I can move the revision code to any portion of the EE and not change the processing code. Since this is my last opportunity to preach (more later),

I encourage you to write programs that are easy to read and maintain. Enough

Processing the upload command is identical; it just sends more information to the PC.

The trickiest part of the program is downloading new parameters. Once the download command is received, we wait for 64 bytes to be sent from the PC. In order to keep things synchronized and order, the PC actually sends a start byte (for

framing), and the address and data to be written to the address. After reception, the Stamp writes

the data to EE, reads it back, then sends the address and data back to the PC for confirmation. By reading back the just-written data, we're able to detect transmission and EE errors. As we'll see in just a minute, the PC will only tolerate a few errors before giving up.

Okay, let's look at the PC code for downloading (Listing 4). Here's a basic description before we get to the specifics:

SOURCES

For more information on the BASIC Stamp, contact:

Parallax, Inc.

3805 Atherton Road, #102 Rocklin, CA 95765 phone (916) 624-8333 http://www.parallaxinc.com

Jan Axelson Lakeview Research

2209 Winnebago St. Madison, WI 53704 Phone: (608) 241-5824 Fax: (608) 241-5848 jan@lvr.com

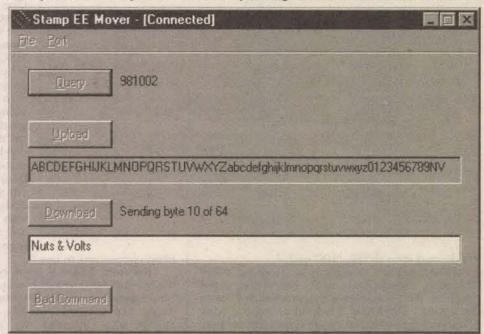
Scott Edwards Electronics, Inc.

2700 E. Fry Blvd. Suite A4 Sierra Vista, AZ 85635 phone 520-459-4802 fax 520-459-0623 www.seetron.com info@seetron.com

Jon Williams

3718 Valley View Lane #3040 Irving, TX 75062 (903) 509-1691 jonwms@aol.com http://members.aol.com/jonwms ftp://members.aol.com/jonwms/stamps

After sending the download command, the code will loop through 64 iterations. If there is no data



N2400 CON \$418D 2400b baud, inverted inst CON 254 backpack LCD instruction byte ClrLCD CON 1 clear the LCD crarHm CON 2 move to line 1, col 1
pTime VAR Word 'pulse width (2 us units) msTml VAR Word 'ms - whole portion msTm2 VAR Word 'ms - fractional portion
:[EEPROM Data]
[Initialization]
Init: PAUSE 1000
Main: PULSIN PInput, 1, prime msTm1 = prime / 500 msTm2 = prime / 5 // 100 SEROUT LCDpin,N2400,[Inst,CrsrHm,DEC msTm1,".",DEC2 msTm2," ms "]
GOTO Main

for the loop iteration, a zero is downloaded. After sending the start, address and data byte, the PC waits for the address and data to come back. If the address and data do not come back correctly, another attempt is made. If five attempts are made to the same address and the data still comes back bad, the process is aborted. Whew! There's a lot going on.

The first thing we do is prevent a premature program shutdown so that the Stamp's EE doesn't get trashed and cause problems. This is done by disabling the buttons and menus and setting a flag called "downloading." This flag is checked in the Query(Inload event in case the operator

clicks the form's close [x] button.

With the process safe from user-interruption, the command is sent and the program waits for 200 milliseconds for the Stamp to get ready. This is a case where the Stamp SERIN timeout for the downloaded data needs to be longer than 200 milliseconds.

```
Listing 3
Nuts & Volts: Stamp Applications, November 1998
                                                                                              ----[ Main Code ]----
  ---- Pitle |-----
                                                                                                                                             ' clear the TX/RX LEDs
                                                                                            Main:
                                                                                                      LEDtx = Off
                                                                                                      LEDrx = Off
  File..... EEMOVER.BS2
  Purpose... Stamp to PC Communications Experiments Author.... Jon Williams
                                                                                                      ' look for PC
                                                                                                      IF PCcon = Yes THEN M1 'look for low on input line SEROUT LCDpin, T9600, [12, "PC is not connected"]
  E-mail... jonwms@aol.com
Started... 30 SEP 98
                                                                                                         PAUSE 250
  Updated... 2 OCT 98
                                                                                                      GOTO Main
                                                                                            M1:
                                                                                                      SEROUT LCDpin, T9600, [12, "Connected. Waiting..."]
 ' ----[ Program Description ]-----
                                                                                                      SERIN RXpin, T9600, 5000, Main, [WAIT (Start), cmd]
                                                                                                      LEDrx = On
PAUSE 50
                                                                                                                                             ' show transmission received
  This program awaits a PC command and processes it accordingly: send the revision code, upload the EE-stored parameters or allow the download of a new (64 byte) parameters block.
                                                                                                      LOOKDOWN and, [CmdQr, CmdUp, CmdDn], and
                                                                                                                                                       ' decode command byte
  For convenience, this project was built on a Parallax BSAC. A SEETRON 4x40\ \mbox{LCD} module was used in debugging.
                                                                                                                                                      branch to processing
                                                                                                      BRANCH cmd, [CQry, CUpLd, CDnLd]
                                                                                                      GOTTO CBad
                                                                                                      SEROUT LCDpin, T9600, [12, "Query "]
                                                                                            COry:
' ---- | Revision History |-----
                                                                                                      GOSUB RCode
                                                                                                      PAUSE 1000
                                                                                                      GOTO Main
' 2 OCT 98 : Finally figured it all out and everything works!
                                                                                                      SEROUT LCDpin, T9600, [12, "Upload"]
                                                                                                      GOSUB Upload
PAUSE 1000
· ----[ I/O Definitions ]-----
                                                                                                      GOTO Main
                                                 ' serial output to PC
' serial input from PC
' debugging pin (SEETRON LCD)
TXpin
                                                                                                      SEROUT LCDpin, T9600, [12, "Download"]
RXpin
         CON
                                                                                                      COSUB DnLoad
PAUSE 1000
LCDpin
PGMpin
                                                 ' uses BS2 programming port
                                                 ' pc connected?
LEDIX
         VAR
                   Out8
                                                 ' receive LED
                                                                                            CRad:
                                                                                                      SEROUT LCDpin, T9600, [12, "Invalid Command"]
                                                 ' transmit LED
                                                                                                      PAUSE 1000
LEDIX
         VAR-
                                                                                                      COTO Main
· ----[ Constants ]-
                                                                                            ' ----[ Subroutines ]-----
N9600
                                                  non inverted (through driver)
         · CON
                                                 ' inverted (direct)
T9600
                   $4054
                                                                                                      ' send revision code to PC
                                                                                                     LEDtx = On
FOR addr = RevCode TO (RevCode + 2)
READ addr, dByte
SEROUT TXpin,T9600,[dByte]
OFF
                                                  ' active low
On
Yes
         CON
                   0
NO
                                                                                                      NEXT
                                                                                                      LEDtx = Off
Start
                   SFF
                                                 ' start byte
                                                                                                      RETURN
                                                 ' query - return date code
''upload ee
CmdQr
CmdUp
         CON
                   SA7
         CON
CmdDn
                                                 ' download new ee
                                                                                            UpLoad: LEDtx = On FOR addr = 0 TO 63
                                                                                                        'READ addr, dByte
· ----[ Variables ]-----
                                                                                                        SEROUT TXpin, T9600, [dByte]
                                                                                                      NEXT
                                                                                                      LEDtx = Off
                                                 ' command byte
                    Byte
                                                                                                      RETURN
addr
dByte
         VAR
VAR
                   Byte
                   Byte
                                                                                            DnLoad: ' download new set-up data
                                                                                                      LEDrx = On SERIN RXpin, T9600, 2000, DLx, [WAIT (Start), addr, dByte]
' ----[ EEPROM Data ]----
                                                                                                      LEDTX = Off
                                                                                                      ' show the transmission SEROUT LCDpin,T9600,[1,"Writing... ", DEC2 addr, "->",DEC3 dByte] SEROUT LCDpin,T9600,[" (",dByte, ") "]
Setup1
         DATA
                    "ABCDEFGHIJKLMNOPQRSTUVWXYZ"
                   "abcdefghijklmnopqrstuvwxyz"
"0123456789"
Setup2
         DATA
Setup3
         DATA
Setup4
                                                                                                      WRITE addr, dByte
                                                                                                                                             ' write to ee
                   98.10.02
                                       ' embedded revision code
RevCode DATA
                                                                                                                                                        ' read it back
                                                                                                      READ addr, dByte
                                                                                                      ' return address and data
' ----[ Initialization ]-----
                                                                                                      SEROUT TXpin, T9600, [addr,dByte]
         DirA = %0001
DirC = %0011
Init:
                                                                                                      LEDbx = Off
                                                                                                      IF addr < 63 THEN DnLoad
                                                                                                                                             ' do 64 bytes
```

' Nuts & Volts: Stamp Applications, November 1998 Private Sub cmdDnload Click() Dim addr As Byte Dim tries As Byte Dim temp As String Dim x As Byte Dim response Call EnableButtons (False) mnuFile.Enabled = False mnuPort.Enabled = False Screen.MousePointer = vbHourglass downloading = True send download command Call SendHeader (CmdDn) Call Delay (200) ' download the ee data addr = 1lblByteCount.Caption = "Sending byte" & Str(addr) & " of 64" tries = 0 Do temp = Mid\$(txtDnload.Text, addr, 1) if empty, program the location with 0

f (temp = "") Then temp = Chr\$(0)

build the buffer (adjusted address + byte)

xBuf = Chr\$(addr - 1) & temp

send Start byte and buffer

MSComm1.Output = ChrS(Start) & txBuf ' wait for two-byte response Do DoEvents x = MSCorm1.InBufferCount Loop Until (x = 2) rxBuf = MSComml.Input ' increment tries counter tries = tries + 1 Loop Until (tries = 5) Or (rxBuf = txBuf) ' exit if bad chip If (tries = 5) And (rxBuf <> txBuf) Then response = MsgBox("Error: Cell " & Str(addr), vbOKOnly) addr = 65 End If addr = addr + 1Call Delay(150) Loop While (addr <= 64) 1b1ByteCount.Caption = "" Call EnableButtons (True) mnuFile.Enabled = True mnuPort.Enabled = True Screen.MousePointer = vbDefault

A Do-Loop construct is used for the overall download structure. The control variable addr is initialized to 1 before starting the loop and checked for exceeding 64. This structure makes it easy to break out of the Do-Loop by setting the control value to greater than 64.

The first part of the loop core gets a piece of data to send. In this case, we're grabbing a character from a text input field. If you are dealing with non-string data, remember to convert the byte to a string with the Chr\$() function. In this program, a null string (the input is less than 64 characters) is converted to 0. I used this because some of the elements in my Stamp production are zero-terminated strings. With the character in hand, the start byte, and address and data are sent. As I stated earlier, I decided to send the start byte through each iteration to keep everything in sync.

After the transmission, we wait for two bytes to come back from the Stamp. Notice the use of the DoEvents function in the reception loop. This is really important, especially if something goes wrong on the Stamp end. DoEvents allows Windows to do other things while processing the loop.

The received input is checked against the data sent. If it's the same, we move on to the next address. If it's not, we'll try the same address again. If the same address fails five times, the loop is terminated and the user is noti-

It all looks pretty easy now that it works, but it was a bear in the process. Good luck with your PC/Stamp projects. They really are a lot of fun when everything is working right.

Farewell, Friends

As those of you that monitor the Stamp list know, this article will be my final regular Stamp Applications column for Nuts & Volts. I stress 'regular" because I am not walking away from Stamping and I really do enjoy writing about my projects. It's just that time is scarce for me right now. With a full-time engineering job and a budding career as an actor (and all the craziness that goes along with that ...), I honestly don't have the time to write a full column each month. I will submit articles as time permits — including the con-clusion of StampNet. I promise.

I really do want to thank Larry Lemieux and his staff at Nuts & Volts for allowing me to write the column this past year and for giving me com-

plete freedom to write about what I chose. Of course, I have to thank my buddy Scott Edwards for trusting me with his creation, for his support, his encouragement, and for his friendship. And I certainly couldn't have done what I've done without the support of Ken Gracey and the good folks at Parallax.

Thank you, Parallax, for everything.
Finally, I must thank my dearest friend, Kim Jaech. Who's Kim? Kim is the miracle worker that translates my techno-gibberish into intelligible English. And all along you folks thought I was a pretty good writer, didn't you? Well, not without Kim. Everything that I've ever had published has passed through her capable hands and so long as I have my way, everything I ever write in the future will too.

Thanks, Kim. I love you.

For those of you in the Metroplex, perhaps I'll see you at a DPRG meeting or at Tanner's on one of my Saturday afternoon parts runs. For those that I've met via E-Mail, snail mail, or the telephone, thanks for your kind words and valuable suggestions for the column. I sincerely appreciate your comments and your input. May God bless each of you always.

Happy Stamping. I'll see you in the movies! NV

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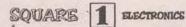
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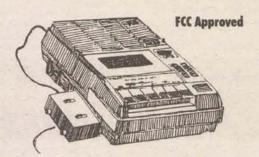




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always be prevented. I even encountered a high power audio amplifier (200W into 8 ohms) with a warning on the rear panel stating that the voltage at the speaker terminals (40V @ 5A when going full blast) is "hazardous to human life.

Michael Kiley Crestwood, IL

Dear Nuts & Volts:

I enjoyed the reference article by Gordon West (Apr. '98, "Copper Foil Grounding for RF.")

As an avid boater and an old-time electroniker, I am usually well read on RF things written for boaters. I have never seen copper foil grounding mentioned in the sailing literature that I have read. Perhaps I have missed it, but if such an article has never been printed, I am certain it would be well received by sailors.

I used to work on an underwater missle that had a wooden nose cone. Yes, it was made of spruce plywood, and it had a one foot wide copper foil strip that ran from its tip down to a wide contact that connected to the aluminum body of the rocket.

The explanation was that it carried static charges away from the metal nose tip fitting. This puzzled me as I never thought that static charges had much difficulty going wherever they pleased, and that a simple piece of wire would have done the job. As usual, I find that there is always more to learn.

Jess Talley via Internet

Dear Nuts & Volts:

In the Sept. '98 issue, Mr. H. Halney requests actual exam-ples of Y2K problems. He seems to have overlooked an actual problem included in his letter.

He states "some clock chips only tell you what the year is modulo 4, that is, will February have 28 days or 29?'

Those chips are an actual Y2K problem. They will tell you that the last year of the 20th Century is a Leap Year, which it is not! The next Leap Year is

> **Emil Rossdeutscher** New York, NY

Dear Nuts & Volts: In your Sept. '98 issue, pages 25 and 26, in answer to #89814 about charging a 72-volt battery system, Fernando Garcia said, "I don't think you would die from a 72-volt shock." Although 72 volts is less

dangerous than higher voltages, I have read documented reports of people being killed by 40 volts, and I have received a good jolt myself from 24 volts by get-

ting across it with wet fingers.
As a result, I would consider any electrical circuit with 24 or more volts between any conductor and ground - or between any two conductors - to be potentially dangerous.

Personal contact with such energized conductors must

The answer to the well-depth question (Aug. '98 Q & A) may provide a workable solution, but a pressure transducer would be a better choice. Mount the sensor near the pump and use its output to drive a meter or an LED bar graph as a depth indicator. You could use the voltage or current output from the sensor with a set of comparators to trigger events when the water goes down to limits that you preset. The pressure under about 35 feet of water is +1 atmosphere, so a 0-1 atmosphere absolute pressure gauge that can work submerged in water would nicely meet the needs of "Stano." Getting the transducer down the well pipe might take a bit of doing, but a piece of PVC pipe (larger inside diameter than the outside diameter of the water pipe) sawed in half lengthwise and clamped together around the water line would easily slide down to the pump. Using the pipe as a guide would also keep the sensor out of the muck at the bottom of the well.

> Test & Measurement World Magazine Newton, MA

Response:

This approach will work, but at a higher price. The problem isn't the cost of the pressure sensor, which you can buy from Omega Engineering (1-800-826-6342; http://www.omega.com) and EG&G IC Sensors (1-800-767-1888; http://www.egginc.com/bin/webmate/egg/page/egg/index) for about \$15.00, but the additional support electronics. These are piezoresistive pressure sensors, sultable for PC board mounting, that come in a TO-5 package. They are available in full-scale ranges from 5.0 to 100 PSI (pounds per square inch). All models are operated from a constant-current excitation supply of 1.5 mA. The problem is the low voltage output from the sensor, which is a mere 5.5 mV per PSI for Omega's PX71-030AV sensor. sor needed for a 35-foot well, as shown in the chart below.

Omega Engineering Pressure Sensor Products Pressure Range Sensitivity @1.5mA excitation Without Fitting With

0 to 5.0 PSI	20 mV per PSI	PX71-005AV	PX72-005AV
0 to 15 PSI	9.5 mV per PSI	PX71-015AV	PX72-015AV
0 to 30 PSI	5.5 mV per PSI	PX71-030AV	PX72-030AV
0 to 60 PSI	3.0 mV per PSI	PX71-060AV	PX72-060AV
0 to 100 PSI	2.0 mV per PSI	PX71-100AV	PX72-100AV

Subtracting for the earth's 14.7 PSI barometric pressure, this translates into about 2.3 mV per foot — or just 82 mV from full to empty. Given the harsh electrical environment at the well site, a signal this weak has to be amplified and filtered before it can be processed. The total cost is going to be more than the \$10.00 thermistor version. But as you point out, it's a reliable depth gauge that'll survive the ravages of time.

TJ Byers Q & A Editor

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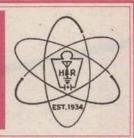
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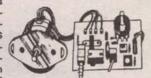
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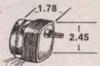
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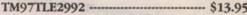


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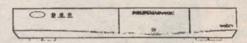
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Interfacing a Magnetic Stripe Reader

Magnetic Stripes

ards with magnetic stripes on the back are everywhere. Credit cards, ATM cards, student ID cards, and even driver's licenses have them. If you go to a trade show, they will give you an ID with a magnetic stripe. Even my grocery card has a magnetic stripe. You cannot get away from this technology.

You can read a card's magnetic stripe by wiring a magnetic stripe reader (MSR) to your computer's parallel port and running a simple program. Figure 1 shows my reader with the LPT port adapter — the only additional requirement is a five-volt supply to power the reader.

My interest in magnetic stripes was peaked by some recent events. During my last trip to the DMV, the clerk typed in all the info on my driver's license instead of swiping the card or just entering my license number - and he made mistakes! Then I was at a tradeshow where the organizers made a tidy profit renting MSR readers and printers to the exhibitors. I've also been curious about the information on the card - if you haven't noticed, many store credit card transactions now print your name on receipt. Does the store get that information from the card or from the credit card company's computer?

All this came to a head when I picked up a magnetic stripe reader for a few dollars at a local surplus store. A little poking around and a search of "magstripe" on the Web turned

Figure 1 Figure 2

up a lot of information.

Some of the information in this article comes from http://www.com/~tommy/files/magcard1.txt and http://www.ee.washington.edu/eeca/text/cardre ader.txt. If you want to try reading

a card with iron fillings and cellophane tape, look at http://b63334.student.cwru.edu/ projects/card/card.htm.

What's on the Back of the Card

The card geometry is 3.375

netic stripe on the back may have up to three tracks (ISO

3554), appropriately called Track 1, Track 2, and Track 3. Each track is 0.110 inches wide, and all data is recorded serially. The tracks are recorded at different densities and have

different formats.

- Track 1 is recorded at 210 bits per inch (BPI). The track contains information in seven-bit characters, and each character has six information bits plus one parity bit. Each track can hold 79 alphanumeric characters.

Track 2 is recorded at 75 BPI and five bits per character. Each character has four information bits and one parity bit. The track

holds 40 digits.

• Track 3 is recorded at 210 BPI and five bits per character. The track holds 107 digits.

Some cards have additional tracks, and some cards use different formats. The California driver's license, for example, records Track 1 at six bits per character (no parity) to squeeze more data on the track.

The magnetic card specifications are also covered in ANSI Standard X4.16 from American National Standards Institute, Inc., 1430 Broadway, New York, NY 10018. Other relevant standards are ISO 7810-1985, ISO 7811-2, and ISO 7811-6.

The Plan

Reading the magnetic stripe involves several tasks.

Signal A	MSR pin	Color	LPT DB25 pin	Port Bit Position	Description
+5 Volts 1	10	Red	NC	NA	Power
RCP2_L 6	5	Blue	13	0x10	Track 2 Clock
RDP2_L 5	5	Green	15	0x08	Track 2 Data
RCP1 L 4	1	Yellow	10	0x40	Track 1 Clock
RDP1_L 3	5	Orange	12	0x20	Track 1 Data
CLS L 2	2	Brown	11	0x80	Card Present
GND 1	Sell-	Black	18, 19, 20, 21, 22, 23, 24, 25	NA	Power and Signal Ground

Table 1. Magnetic Stripe Interface

1.	Connecting	the N	ISR to	the
compi	uter.			

Capturing the MSR bit stream into the computer.

Extracting the track characters from the bit stream.

Testing the track for errors and possibly correcting them.

5. Interpreting the information on the track.

The first task physically connects the reader to the computer, and the other tasks are performed in software by the C program MAG-CARD listed here in the article.

Connecting the MSR to the Computer

My magnetic stripe reader is

a Neuron Corp, Model MCR-133-2R-2020, Serial 2110249. Its interface signals and pinouts are given in Table 1. All signals are active low. Other MSRs will have similar signals, but their pinouts

Start sentinel

Separator '

Separator

Other data End sentinel

Format code = 'B'

Primary account number

Expiration date or separator

Last Name/First Initial

I picked up my reader at a surplus store, and you might do the same. If not, Digi-Key

will vary.

number Up to 19 characters following ANSI X4.13
1 character
Initial e.g., "Public/John Q"
1 character
or separator 4 (YYMM) or 1 characters
Variable
1 character
1 character
1 character
Table 2: Track 1 Format Code B

CR-133- (http://www.digikey.com) sells

1 character

1 character

(http://www.digikey.com) sells some Panasonic magnetic card readers. A reader that only reads Track 2 (ISO2) sells for \$30.00, and one that reads both Track 1 and Track 2 (ISO1/ISO2) sells for \$70.00. I haven't tried them, but they should be similar.

Wiring the MSR to the parallel port is easy because there are

```
/* -*- Mode: C -*- */
// Read a Credit Card Magnetic Stripe
// Copyright Gerald Roylance 1998. All rights reserved.
#include <stdio.h>
#include <assert.h>
#include <ctype.h>
#include <conio.h>
                                                   // for inp() and kbhit()
#define LPTOUT 0x378
  port+0 (bidirectional data)
  port+1 (pins are input only)
pin 15 = 0x08 | IRDP2
pin 13 = 0x10 | IRCF
                                  IRCP2
    pin 12 = 0x20
    pin 10 = 0x40
pin 11 = !0x80
                                  IRCP1
#define Active(b) ((b)&0x80)
// Define the bit test masks for a track struct MTrack
 unsigned char bClock; unsigned char bData;
struct MTrack mtTrack1 = {0x40, 0x20};
struct MTrack mtTrack2 = {0x10, 0x08};
// Define the codes used on each track
struct MCode
 unsigned int cBits;
unsigned int fParity;
unsigned char bSentinel;
unsigned char bTerminal;
struct MCode mc7Bit = {7, 1, 0x45, 0x1F};
                                                                    // Industry Standard
Track 1 struct MCode mc6Bit = {6, 0, 0x05, 0x1F};
                                                                 // California Drivers
struct MCode mc5Bit = {5, 1, 0x0B, 0x1F};
                                                                    // Industry Standard
// Capture raw signal data at the LPT input port
     < 0 if there is a problem capturing the data
// 0 if user types a key
// # of bytes of data
int CaptureRaw(int cbRaw, unsigned char *abRaw)
  int-portOut = LPTOUT;
 int portlnt = portOut+1;
int portlnt = portOut+2;
 unsigned char b;
unsigned char bLast;
                                                   // current I/O byte
// last I/O byte
// number of output bytes
  int cb = 0;
  // timeout counter ... don't hang the machine forever
 long dwDelay = 0;
long dwDelayLimit = 10000000L;
 // make sure the arguments are reasonable assert(cbRaw > 256 && abRaw != NULL);
 // Initialize the LPT port // put the open collector drivers on I/O port in a reasonable state
 // we don't need to do this ...
outp(portInt, 0x00);
 // no interrupts outp(portint, 0x00);
 assert(!Active(inp(portin)));
 // wait for -CLS to go active
```

```
// read the port
        b = inp(portIn);
// test if active
        if (Active(b))
          break:
        // if the user types a character, give up
            (void)getchar();
return 0;
   // remember this byte
   bLast = b;
// record the first active data byte
   abRaw[cb++] = b;
   // capture data while -CLS is active while (1)
       b = inp(portIn);
// record if I/O data byte changed
        if (b != bLast)
             // remember b for next data change
            // record the new data abRaw[cb++] = b;
             // bail out if we run out of buffer
             if (cb >= cbRaw)
                // Raw buffer full!
                return -1:
            // reset the failsafe counter
            dwDelay = 0;
        // quit when the select line goes inactive if (IActive(b))
          break:
       // failsafe counter ...
if (dwDelay++ > dwDelayLimit)
             // *** Failsafe counter expired!
   return cb;
// Turn array of port raw data values into a track byte string
// returns # of bytes in Track > 2 if successful int ExtractTrack(struct MTrack *pmtTrack, struct MCode *pmcCode, int cbRaw, unsigned char *abRaw, int cbTrack, unsigned char *abTrack)
   // the number of bits in a character
  // the number of bits in a character
unsigned int cBits = pmcCode->cBits;
unsigned char bWeight = (1 << (cBits-1));
unsigned char bSentinel = pmcCode->bSentinel;
unsigned char bTerminal = pmcCode->bTerminal;
// specify the Clock and Data bits of the interface byte
unsigned char bClock = pmtTrack->bClock;
unsigned char bData = pmtTrack->bData;
// initialize the state machine
   // initialize the state machine unsigned char bLast = abRaw[0];
   unsigned char bShift = 0;
int iStripe = -1;
                                                               // IStripe = -1 -> search for sentinel
   int iBit = 0:
                                                               // which bit we are working on
   int iRaw;
```

```
// data is LSB first
for (iRaw = 0; iRaw < cbRaw; iRaw++)
      unsigned char b = abRaw[iRaw];
      // Look for Falling Clock Edge
if (((bLast&bClock)!=0) && ((b&bClock)==0))
          // there is a clock edge.
// Determine the bit (reader signal is active low)
unsigned char bit = ((b&bData)?0:bWeight);
         // shift the register and or in the new bit bShift = ( (bShift>>1) | bit);
          iBit++:
          // process the new bit
          if (iStripe < 0)
              // iByte < 0 means we have not seen a start sentinel yet. 
// Check if this bit now reveals the sentinel.
              if (bShift == bSentinel)
                  // fprintf(stderr, "Start Sentinel found\n");
                 // start recording characters .
                 iStripe = 0;
abTrack[iStripe++] = bShift;
                 iBit = 0
             // we've seen a start sentinel, so mark off each cBits into a
byte
              if (iBit == cBits)
                 // we've picked up a new byte
abTrack[iStripe++] = bShift;
                 iBit = 0:
                 // if the byte before this one was the end sentinel, 
// then this byte is the LCC and we are done with the string 
if (iStripe >= 2 && abTrack[iStripe-2] == bTerminal)
                     // fprintf(stderr, "End Sentinel found\n");
                     return iStripe;
                 // will we run out of room? if (iStripe >= cbTrack)
                     break:
                 // end of look for falling edge
      // remember this byte for the next iteration
     bLast=b;
// end of for loop
  // we did not find an end sentinel or ran out of room
// Convert the Stripe Bytes to a character string
void DumpRaw(int cb, unsigned char *abRaw)
 FILE *file = fopen("magcard.txt", "wt");
 if (file == NULL)
     perror("DumpRaw");
  else
     int i:
     for (i = 0; i < cb; i++)
```

only a few wires. The essential task is making an adapter cable from the MSR's connector to the LPT port connector. Each pin on the MSR is wired to a male DB25 connector that plugs into the LPT port. The pins are called out in Table 1. Connect all the LPT ground leads together, and make some provision for powering the MSR.

If your reader doesn't have Track 1 or Track 2, then you can leave its clock and data pins open. You must supply a connection for CLS_L for the software to recognize a card.

When a card is swiped, CLS_L

goes low (becomes active) and then the clock lines continue to toggle at a reasonably constant rate. Initially both data lines are held high (logic zero), but after a short time, they start changing back and forth. The data should be clocked on the high to low transition of its clock line — the software given handles that.

Getting the Data into the Computer

The connection to the LPT port allows the computer to sample the instantaneous signal values from the MSR. For the con-

nection to be useful, the computer must sample the port often enough to notice all the clock changes before a data line changes. The procedure CaptureRaw reads the port data and records every change. The port data only needs to be saved when the CLS line is active (i.e., when a card is being swiped), so the routine waits for CLS_L to go active, and then records all the data until CLS_L becomes inactive.

To get an idea of how often we must look at the port, an MSR can read cards that are swiped at 4 to 60

inches per second. For Track 1, that implies bit rates of 840 to 12,600 bits per second. In order to catch all the clock changes, it should sample at least four times the data rate — about 50,000 samples per second or every 20 microseconds for a fast swipe.

```
Start Sentinel 1 character
Format code = 'D' 1 character
Name 58 characters
Address 29 characters
City 13 characters
End sentinel 1 character
LRC 1 character
```

Table 3: Track 1 for California Driver's License

```
unsigned char b = abRaw[i];
       fprintf(file, "%02x %d%d%d%d%d%d%d%d%d%n",
                  (b>>7)&1, (b>>6)&1, (b>>5)&1, (b>>4)&1, (b>>3)&1, (b>>2)&1, (b>>3)&1, (b>>2)&1, (b>>1)&1, (b
    fclose(file);
int fOddParity(unsigned char bByte)
 register unsigned char b = bByte;
 b ^= (b>>2);
b ^= (b>>1);
 return (b&0x01);
char cYYY(unsigned int cBits, unsigned int cx)
 if (cBits == 4 || cBits == 5)
     return '0' + (cx&0x0F);
  else if (cBits == 6 || cBits == 7)
    // characters are six bit + parity ...
return ' ' + (cx&0x3F);
    // *** unknown code!
    assert(0);
return **;
void PrintTrack(struct MCode *pmcCode, int cbLength, unsigned char
abTrack)
  int cBits = pmcCode->cBits;
 for (i = 0; i < cbLength; i++)
    fprintf(stderr, "%c", cYYY(cBits, abTrack[i]));
 fprintf(stderr, "\n");
void PrintTrackParity(int cbLength, unsigned char *abTrack)
 int i:
 for (i = 0; i < cbLength; i++)
    fprintf(stderr, "%c", (fOddParity(abTrack[i]))? ' : 'X');
 fprintf(stderr, "\n");
char *szStripeToChar(int cbTrack, unsigned char *abTrack, char
 'acStripe)
 int i:
 for (i = 0; i < cbTrack; i++)
     acStripe[i] = cYYY(7, abTrack[i]);
 //*** should guarantee from for the null byte ... acStripe[cbTrack] = \(^0\);
 return acStripe;
// Process one Track
```

```
// return length of track
int ProcessTrack(struct MTrack *pmtTrack, struct MCode *pmcCode, int cb, unsigned char *abRaw, int cbTrack, unsigned char *abTrack)
  int iReturn = -1;
  // we got stuff ...
int cbLength = ExtractTrack(pmtTrack, pmcCode, cb, abRaw, cbTrack,
abTrack):
 \begin{array}{l} \operatorname{assert}(\operatorname{cYYY}(7, 0x45) = \ \ \%'); \\ \operatorname{assert}(\operatorname{cYYY}(7, 0x3E) = \ \ \%'); \\ \operatorname{assert}(\operatorname{cYYY}(7, 0x5F) = \ \ \%'); \end{array}
  // if cbLength <= 2, then we did not find the sentinels! if (cbLength <= 2)
       fprintf(stderr, ".. no sentinels found\n");
       fprintf(stderr, "Track Raw length %d bytes\n", cbLength);
PrintTrack(pmcCode, cbLength, abTrack);
       // Do error detection
        unsigned char bLCC = 0;
int cBits = pmcCode->cBits;
int fParity = pmcCode->fParity;
unsigned char bMaskP = (0xFFU >> (8-cBits));
unsigned char bMaskD = (fParity)? (bMaskP>>1) : bMaskP;
int cErrors = 0;
int iError = 0;
int i:
         // calculate # of parity errors and LCC for (i = 0; i < cbLength; i++)
              bLCC ^= abTrack[i];
if (!fOddParity(abTrack[i]))
                   cErrors++:
         // do we have a parity error if (fParity && cErrors != 0)
PrintTrackParity(cbLength, abTrack);
fprintf(stderr, "Parity Errors: cErrors = %d, LCC = %02x\n",
cErrors, bLCC);
              if (cErrors == 1)
                  fprintf(stderr, "Correcting single error:\n");
abTrack[iError] ^= bLCC;
                   PrintTrack(pmcCode, cbLength, abTrack);
                   // but say we failed anyway iReturn = -1;
          else if ((bMaskD & bLCC) != 0)
              fprintf(stderr, "LCC Error: LCC = %02x\n", bLCC);
               // no errors found!
              iReturn = cbLength;
   return iReturn;
// Read and Print a Card
unsigned char abRaw[16384]
                 cbRaw = sizeof(abRaw);
int MagReadAndPrint(void)
```

```
int iReturn = 1:
   fprintf(stderr, "Swipe Card - or press a key to quit\n");
     // capture the data and the number of samples int cb = CaptureRaw(cbRaw, abRaw);
     fprintf(stderr, "Capture data return %d bytes\n", cb);
     assert(cb <= cbRaw):
     if (cb < 0)
          fprintf(stderr, "- Problem capturing the data: error = %d\n", cb);
      else if (cb == 0)
          iReturn = 0;
          unsigned char abTrack[256]
                           cbTrack = sizeof(abTrack);
          // dump port data to a file
// DumpRaw(cb, abRaw);
tprintf(stderr, "TRACK1 — 7bit\n");
if (ProcessTrack(&mtTrack1, &mc7Bit, cb, abRaw, cbTrack, abTrack) < 3)
               int cbDriver;
// if 7 bit failed, try 6 bit ...
fprintf(stderr, "TRACK1 — 6bit\n");
cbDriver = ProcessTrack(&mtTrack1, &mc6Bit, cb, abRaw, cbTrack, abTrack);
               if (cbDriver > 2 && cYYY(6, abTrack[1] == 'D'))
                   int cName = 58;
int cAddress = 29;
                   int cCity = 13;
int iName = 2;
int iAddress = iName + cName;
                   int iCity = iAddress + cAddress;
int iEnd = iCity + cCity;
                   fprintf(stderr, "California Driver's License\n");
for (i=iName; i < min(cbDriver, iAddress); i++)
fprintf(stderr, "%c", cYYY(6, abTrack[i]));
fprintf(stderr, "\n");
for (i=iAddress; i < min(cbDriver, iCity ); i++)
fprintf(stderr, "%c", cYYY(6, abTrack[i]));
fprintf(stderr, "\n");
for (i=iCity; i < min(cbDriver, iEnd ); i++)
fprintf(stderr, "%c", cYYY(6, abTrack[i]));
fprintf(stderr, "\n");
           fprintf(stderr, "TRACK2 — 5bit\n");
ProcessTrack(&mtTrack2, &mc5Bit, cb, abRaw, cbTrack, abTrack);
   return iReturn;
// Main
 int main(void)
   assert(fOddParity(1) && !fOddParity(0x71));
   // read and print card until the user hits a character ... while (MagReadAndPrint())
   return 0;
```

Unfortunately, Windows cannot perform such high sample rates, so the program must run in MS/DOS mode. Windows runs in protected mode and installs a virtual device driver (VxD) for the LPT I/O ports. That VxD traps all I/O instructions to the LPT port and then emulates the I/O. Instead of one simple I/O instruction, the computer will execute hundreds of instructions and perform some task switches. Furthermore, Windows may switch to another application and cause large gaps in the sampling.

Instead of fighting Windows or building more exotic hardware, we can run the code in real mode under MS/DOS. The real-time clock will still interrupt the sampling routine, but its effect is minor. To run the program, put Windows into MS/DOS mode by executing Start | Shut Down, and then select "Restart the computer in MS/DOS Mode." Then run MAGCARD.EXE from the MS/DOS command line.

Grouping the Bits into Characters

The procedure CaptureRaw saves the instantaneous values at the data port. The procedure ExtractTrack examines the raw port data for clock transitions, determines the bit value, and assembles the bits into characters. To get the information from two tracks, we call ExtractTrack twice — once for each track.

The basic format of each track is a preamble, a start sentinel character, an arbitrary number of data characters, the end sentinel character, and a longitudinal check character (LCC). The data come from the card in bit serial fashion with the LSB first. A special bit pattern - called the start sentinel marks the end of the preamble and the start of the data. Succeeding bits are grouped into appropriately-sized characters for the track. Another special character - the end sentinel - marks the end of the data and tells us the next character is the LCC.

Testing for Errors

If ExtractTrack finds the sentinels, then the track data will be stored in the array abTrack. Now we need to test that information for errors. In the standard formats, each character has a parity bit, so each character is tested for proper (odd) parity. Any bad parity indicates the track was misread.

All track formats have a longitudinal check character (LCC). When the track was recorded, the LCC was chosen so that a bitwise XOR of all the characters in the track will produce zero. After

Start Sentinel Primary account number Separator Country code (3 characters)

Expiration Date or separator

Other data ... End Sentinel LRC 1 character Up to 19 characters 1 character Only if primary account n

Only if primary account number starts with 59 ... USA is 840

4 characters YYMM or 1 character

1 character 1 character

Table 4: Track 2 Format

A Issuer is BCD unless
O Government, issuer is BCDE
UATP
Airlines
Travel and Entertainment
Bank, issuer is BCDEF
Bank
if B is 1, 2, or 3, then issuer is 1, 2, or 3 digits
if B is 0, 4, 5, 6, 7, 8, then issuer is BCDEF
Retail (Restricted), issuer is BCDE
Petroleum

reading a track, if XORing all of the characters does not produce zero, then there was a read error. The LCC is an even parity check bit across all the track characters. If either the parity test or the LCC test fails, then there is a problem with the data. We must either reread the track or correct the data.

<future>

National Card

The parity and LCC checks are redundant: either test will detect a single bit that went bad. We don't need both tests to detect a single bit error — one test would be enough. With the two tests, we can actually correct a single bit error. We may not want to do this because it lowers our reliability (we may mistakenly "correct" a detected error to the wrong value), but it will improve our ability to read some cards.

If only one character has bad parity, then we can reconstruct the character using the LCC. The bad parity tells us which character has the error, and the LCC tells us which data bits in that character are bad.

For example, assume bit 3 of the 10th character should be a zero, but is misread as a one. The 10th character (as read) now has an extra one bit, so the 10th character's parity is even. That tells us there is a problem with character 10. When we bitwise XOR all the characters in the track, we don't get zero.

The erroneous bit 3 of the 10th character causes bit 3 of the XOR to be nonzero. Putting the two pieces of information together, we know that bit 3 of character 10 is wrong; complementing that bit should fix the data.

Well, maybe not. Although the parity and LCC scheme can fix single bit errors, multiple errors may confuse it. If there were two errors in one character, then the LCC comes out wrong but all the parity calculations are right. We know there's an error, but we don't know which character. Even worse, there may be two errors in one character and one error in a second character.

The parity calculation indicts only the second character, and the correction algorithm mistakenly believes fixing only the second character will fix the track.

Consequently, it may be better not to correct errors and instead to ask the operator to swipe the card again or key the information in by hand. In technical terms, the Hamming distance of the parity and LCC code is 4. That means we can detect all single, double, and triple bit errors, but will miss some four bit errors.

If we use correction, then we can correct all single bit errors and detect double bit errors — but we will turn some triple bit errors into four bit errors. If we don't correct, then we are much more certain that the data we do read is correct.

Interpreting the Data

After the track has been read without errors (or corrected), then we can decode the information in the track. There are several conventions for encoding the data in a track. Track 1 is a high-density track with up to 79 alphanumeric characters. The first character of the track tells us how to decode the remaining data. Track 2 is a low-density track with more rigid encoding.

Track 1 Format

Track 1 encodes alphanumeric information. The first character following the start sentinel describes the remainder of the track. Usually the first character will be an 'A' (signifying that the following format depends on the card issuer) or a 'B' (signifying a standard layout for the initial data fields).

Of course, seeing format code 'A' doesn't help you unless you know what the card is. Seeing format code 'B' means you can figure out some things about the card.

In the next sections, we cover

the character code used by Track 1 and format code 'B.'

Track 1 Character Code

The code is six bits (64 possible characters). The code can be converted to ASCII by adding 0x20 (a space) to the six-bit code, but many of the possible characters are reserved or prohibited. Space, 'A'-'Z', '0'-'9', '#', '\$', '(', ')', '-', '!', and '/' are legitimate characters. The start sentinel is 0x45 ('%'), the end sentinel is 0x1F ('?'), and the separator is 0x3E ('^') and have special purposes.

Track 1 Format Code B

If the character following the start sentinel is a 'B,' then the remainder of the track has an account number, name, and expiration date. The 'B' format code is used by most credit and ATM cards, and is show in Table 2.

The data following the account number is sometimes dependent upon the account number. If the account number starts with "59," then a country code follows the account number separator. More information can be found in ANSI X4.16.

Track 1 for the California Driver's License

The California driver's license has an unusual format (Table 3). In order to pack more data into the track, they forgo parity and record the data at six bits per character. The format code is a 'D' instead of a 'B.'

Track 2 Format

Track 2 is the low-density, numbers-only track that can hold up to 40 characters. The track usually contains an account number, an expiration date, and some additional information.

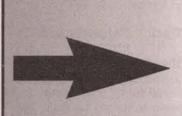
Track 2 Character Code

The Track 2 character code is four bits plus parity, so the track can hold only hexadecimal digits. The hex digits can be converted to ASCII by adding the code for '0.'

The characters 0-9 are used for data, and three characters are designated the start sentinel (B or ';'), the end sentinel (F or '?'), and the separator character (D or '='). The remaining three characters are for hardware control (A or ':' and E or '>') or are reserved (C or '<').

Track 2 Format

Table 4 describes the Track 2 format. The data following the expiration date is determined by the card issuer.



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// Credit Card Checksum Algorithm // ANSI X4.13-1983 #include <assert.h> #include <string.h> #include <ctype.h>

#define digit_weight(x) (assert(isdigit(x)),

// Calculate the value of the check digit ... int iCCCheckCalc(char *szAcct, int n)

assert(n > 0);

for (i = n-2; i >= 0; i-)1// weights alternate 1,2,1,2,... and // the check digit (i=n-1) has weight 1

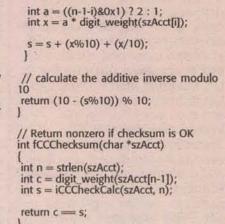
California Drivers License Track 2

Although Track 1 of the California driver's license uses the unusual six-bit character format, Track 2 is conventional. Driver's licenses have expiration dates just like credit cards, so Track 2 dutifully records that information.

The driver's license number is encoded as an account number. Amusingly, the state of California is apparently a retail establishment because its account number string starts with a 6 (see the section on account numbers below). The encoding appears to be

6 + 006460 + <class> + <driver's license number> + <check digit>

where a class C license is coded as 3. The variable information following the expiration date is the driver's birth date encoded as YYMMDD.



Account Numbers

ANSI X4.13-1983 describes the format of account numbers.

Account Number Format

The table below tells how to decode an account number. If the digits of the account number are ABCDEFGH ..., then use the first digit (A) to decode the remaining

Credit Card Checksum

Account numbers also have a checksum algorithm. Retailers and banks want to make sure they got the account number correct, so they include a check digit.

Not only does the checksum algorithm detect a bad digit, but it also detects the common error of swapping two neighboring digits (i.e., turning "37" into "73") The routine fCCChecksum will test the checksum. NV



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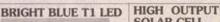
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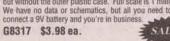
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News Bytes

1999 Trinity College Fire-Fighting Home Robot Contest

over \$4,000.00 in prizes

Fighting Home Robot Contest will be held on the Trinity College campus in Hartford, CT on Sunday, April 18,

This is the largest, public, true Robotics competition held in the US that is open to entrants of any age, ability, or experience from anywhere in the world.

Last April, we had a great contest. People came from all over the US, Canada, and Europe to compete, participate, watch, learn, and enjoy. This April, the contest will be even better.

The goal of the 1999 contest is the same – to build a Robot that can find and extinguish a fire in a house. The challenge is to build a computerized (not radio-controlled) Robotic device that can move through a model of a single floor of a house, detect fire (a lit candle), and then extinguish it. Robots that accomplish this task in the shortest time win.

Other events scheduled on the contest weekend include Robotics seminars and exposition.

This weekend-long international event will culminate months of work and effort by Robotists of all ages. Last year's contest drew interest from people in all 50 states and 14 countries. Participants ranged from college professors and engineers to elementary school students and they came from as far as Switzerland and Argentina.

The 1999 rules are very much like last year's rules, but some slight changes have been made to make the contest more realistic, more fun, and more like the real world. There will be two divisions again this year. A Junior division for those in High School and younger and a Senior division for everyone else. There will be a cash prize of \$1,000.00 awarded to the top winner in each division with additional prizes to other winners in those divisions.

Trinity College is also helping to set up regional contests around North America. Check the Home Page to see if there is a site near you.

Video tapes of the 1998 contest are available for \$25.00 each (includes shipping). Copies of the updated 1999 rules are available for \$3.00. Send cash, check, or money order payable to: Trinity College, Jake Mendelssohn, 190 Mohegan Dr., West Hartford, CT 06117. E-Mail: JMENDEL141@AOL.COM. Or download the information from the contest Home Page at http://www.trincoll.edu/~robot.



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Generator, dual channel option TEK DD501 Digital Delay & Burst Gen.,	
TEK FG502 11 MHz Function Generator	\$300.00 \$250.00 \$225.00
tor function & puse gen's TEK FG501 1 MHz Function Generator, TM500 series TEK FG502 11 MHz Function Generator. TEK FG503 3 MHz Function Generator, TM500 series TEK FG501 Ramp Generator, TM500 series MAVETEK 180 2 MHz Sweep/Function Generator MAVETEK 185 5 MHz Lin/Log Sweep/Function Generator MAVETEK 288 20 MHz Synthesized Function Generator, GPIB	\$200.00 \$300.00 \$750.00
PULSE	3
BERKELEY NUCLEONICS 7085B Digital	\$1,750.00
50 V/50 ohms, counted hurst opt	
HP 8007B 100 MHz Pulse Generator HP 8012B 50 MHz Pulse Generator, variable transition time	
HP 8015A 50 MHz Dual Output Pulse Generator HP 8080A/81A/83A/84A 300 MHz Word Generator HP 8080A/91A/92A/93A 1 GHz Single Channel Pulse Generator	
HP 8111A 20 MHz Pulse / Function Generator HP 8115A 50 MHz Dual Channel	\$1,500.00 \$3,500.00
Pulse Generator, HPIB TEK PG502 250 MHz Pulse Generator, Tr<1nS, TM500 series	
TEK PG505 100 kHz Pulse Generator,	
TEK PG508 50 MHz Pulse Generator, TM500 series WAVETEK 802 50 MHz Pulse Generator	\$500.00

VOLTAGE & CU	NNENI
VOLTMETERS	
FLUKE 845AR High Impedance Voltmeter / Nu HP 3456A 6-1/2 Digit Voltmeter	\$750.00
HP 3478A 5-1/2 digit Multimeter, HPIB KEITHLEY 155 Null Detector/ Microvoltmeter, 1 uV-1000 V f.s.	
KEITHLEY 181 6-1/2 digit Nanovoltmeter, 10 nV sensitivity, GPIB	
SOLARTRON 7081 8-1/2 digit Voltmeter	\$3,900.00

TEK DM501A 4-1/2 digit Multimeter,	\$225.00
CALIBRATION	
FLUKE 510A AC Reference Standard, 10 VRMS, 0-10 mA . FLUKE 515A Portable Calibrator,	\$900.00
DC/AC/Ohms, line & battery power FLUKE 5220A Transconductance Amplifier, DC-5 kHz, 0-20 A	\$3,000.00
FLUKE 720A 7-decade Kelvin-Varley Voltage Divider FLUKE 731B DC Reference Standard	\$1,250.00 \$400.00
FLUKE 732A DC Voltage Standard	\$2,000.00
0.5-1200 V, 20 Hz-30 MHz VALHALLA 2703 AC Volt.Sid.,0-120V/ 10 Hz-100 kHz;120-1200V/10 Hz-1 kHz	\$2,250.00
VOLTAGE SOURCES	
HP 6115A Precision Dual Range Power Supply, 50V 0.8A / 100V 0.4A	\$850.00
KEITHLEY 228 Programmable Voltage/Current Source	\$2,500.00
CURRENT METERS & SOURCES	
HP 4140B Picoammeter / DC Voltage	\$2,000.00
Source, without test fixture HP 6177C DC Current Source, to 50V, 500mA	\$500.00
HP 6181C DC Current Source, to 100 V, 250 mA	\$500.00
HP 6186C DC Current Source, to 300V, 100mA	\$750.00
KEITHLEY 220 Programmable Current Source, 0.5 pA-101 mA, 1-105 V lim	\$2,000.00
KEITHLEY 225 Current Source,	\$500.00
0.1 uA-100 mA, 10-100 V compliance KEITHLEY 227 Current Source, 1 uA-1 A,	
	\$800.00
0-50 V compliance KEITHLEY 261 Plocampere Source	\$375.00
KEITHLEY 642 Electrometer TEK A6303 Current Probe, DC-15 MHz,	\$1,500.00
TEK A6303 Current Probe, DC-15 MHz,	\$1,000.00
100 A max.,for use with AM503 TEK AM503/A6302/TM501 AC/DC	\$1,000,00
Current Prohe System	
TEK CT-5 -opt.05 High Current Transformer for P6021/A6302, to 1000A	\$300.00

IMPEDANCE & COMPONENT	TEST
L.C.R. BOONTON 62AD 1 MHz inductance Meter, 2-2000 uH BOONTON 72BD 1 MHz Capacitance Meter, 3-1/2 digit display	\$550.00 \$650.00
HP 4262A-101 3-1/2 digit LCR Meter,	
HP 4275A-001 5-1/2 digit LCR Meter,	\$5,000.00
UIAITEATIE	6200.00
E.S.I. DB62-11K 6-Decade Resistor,	
E.S.I. SR1010 Resistance Transfer	\$550.00
Standards, 1 Ohm-100 K/step E.S.I. SR1050-1M Resistance Transfer	\$2,000.00
GR 1404-A 1000 pF Reference Standard Capacitor	\$700.00
GR 1406 Standard Air Capacitors,	
GR 1412-BC Decade Capacitor, 50 pF - 1.11115 uF	\$350.00
0-111 10 Ohms 0.01 Ohm resolution	\$125.00
GR 1433-J 4-Decade Resistor,	\$250.00
0-11,110 Ohms, 1 Ohm resolution GR 1433-K 4-Decade Resistor,	\$250.00
0-1,110 Ohms, 0.1 Ohm resolution	4200.00
0-1,110 Ohms, 0.1 Ohm resolution GR 1433-L 4-Decade Resistor,	\$250.00
0-111,100 Ohms, 10 Ohms resolution GR 1433-N 5-Decade Resistor,	\$300 no
0-11.111 Ohms, 0.1 Ohm resolution	\$300.00
0-11,111 Ohms, 0.1 Ohm resolution GR 1433-U 4-Decade Resistor,	\$250.00
0-111.0 Ohms, 0.01 Ohm resolution GR 1433-X 6-Decade Resistor,	\$350.00
to 111.111.0 Ohms, 0.1 Ohm res.	\$350.00
to 111,111.0 Ohms, 0.1 Ohm res. GR 1482-series Standard Inductors	\$275.00
HP 16380A Standard Air Capacitor	The second secon
Set, 1/ 10/ 100/ 1000 pF VALHALLA 2724A Programmable	\$1,675.00
HP 4328A Milliohmeter	\$1,300.00
	\$1,200.00
CURVE TRACERS	4000000
TEK 577D1/177 Storage Curve Tracer,	\$2,250.00
TEK 577D2/177 Curve Tracer, with standard test fixture	\$1,850.00
T.D.R.	
TEK 1502-opt.04 Time Domain	\$1,400.00
Calle stampeters C C CCC foot about an analysis	
TEK 1503-opt.04 Time Domain	\$1,400.00

SINGLE OUTPUT	
HP 6002A-001 0-60 V/ 0-10 A/ 200 Watts max	\$750.00
Autoranging Power Supply	\$200.00
HP 6200B Dual Range Supply. 0-20 V 0-1.5 A/ 0-40 V 0-750 mA CVCC	. \$200.00
HP 6201B 0-20 V 0-1.5 A CV/CC Power Supply	. \$175.00
HP 6207B 0-160 V 0-200 mA CV/CC Power Supply	\$300.00
HP 6260B-027 0-10 V 0-100 A CV/CC	\$675.00
Power Supply; 208 VAC line	
HP 6207B 0-160 V 0-200 mA CV/CC Power Supply HP 6256B 0-10 V 0-20 A CV/CC Power Supply HP 6260B-027 0-10 V 0-100 A CV/CC	\$300.00 \$300.00

POWER SUPPLIES

HP 6261B-027 0-20 V 0-50 A CV/CC	\$675.00
Power Supply; 208 VAC line	****
HP 6263B 0-20 V 0-10 A CV/CC Power Supply	\$400.00
HP 6266B 0-40 V 0-5 A CV/CC Power Supply	\$400.00
HP 6269B-028 0-40 V 0-50 A CV/CC	\$950.00
Power Supply; 230 VAC line	0400.00
HP 6271B 0-60 V 0-3 A CV/CC Power Supply	\$400.00
HP 6274B 0-60 V 0-15 A CV/CC Power Supply	\$900.00
HP 6281A 0-7.5 V 0-5 A CV/CC Power Supply	\$175.00
HP 6284A 0-20 V 0-3 A CV/CC Power Supply	\$225.00
HP 6299A 0-100 V 0-750 mA CV/CC Power Supply	\$225.00
HP 6384A 4.0-5.5 V at 8 A CV/CL Power Supply	
HP 6434B 0-40 V 0-25 A CV/CC Power Supply	\$800.00
HP 6443B 0-120 V 0-2.5 A CV/CC Power Supply	\$450.00
KEPCO ABC-1500M 0-1500 V 10 mA CV/CL Power Supply	\$125.00
KEPCO ATE 36-30M 0-36 V 0-30 A CV/CC Power Supply	\$900.00
KEPCO ATE 36-8M 0-36 V 0-8 A CV/CC Power Supply	\$550.00
SORENSEN DCR 20-25B 0-20 V	\$550.00
0-25 A CV/CC Power Supply SORENSON DCR 600-0.75B 0-600 V	000000
	\$600.00
0-750 mA CV/CC Power Supply	0400 00
SORENSON SRL 20-12 0-20 V	\$400.00
0-12 A CV/CC Power Supply	*****
SORENSON SRL 60-8 0-60 V 0-8 A CV/CC Power Supply	
TEK PS501-1 Power Supply, 0-20 V,	\$175.00
	4. 00
MULTIPLE OUTPUT	
HP 6227B Dual 0-25 V 0-2 A CV/CC Power Supply	\$600.00
HP 6228B Dual 0-50 V 0-1 A CV/CC Power Supply	
HP 6253A Dual 0-20 V 0-3 A CV/CC Power Supply	
HP 6255A Dual 0-40 V 0-1.5 A CV/CC Power Supply	\$500.00
TEK PS5010 Programmable	\$750.00
Triple Power Supply TM5000 series	
TEK PS503A Dual Power Supply, TM500 series	\$200.00
MISCELLANEOUS	
ACME PS2L-500 Programmable Load,	\$400.00
0-75 V / 0-75 A / 500 Watts max.	
ELGAR 1751B/461 AC Power Source,	\$2,000.00
0-135 VAC, 1750 Watts, fixed freq.osc.	
HP 59501B HPIB Isolated DAC/Power Supply Programmer	\$175.00
HP 6825A Bipolar Power Supply/ Amplifier, +/- 20 V 2 A	\$800.00
KEPCO BOP 20-20M Bipolar Op Amp/	\$675.00
Power Supply to 20 V 20 A	
KEPCO BOP 50-2M Bipolar Op Amp/	\$400.00
Power Supply to 50 V 2 A	
TRANSISTOR DEVICES DAL-50-15-100	\$200.00
Programmable Load, 0-50 V, 0-15 A, 100 Watts max.	
THE A PROPERTY	

TIME & FREQUENCY	
UNIVERSAL COUNTERS	
HP 5315A 100 MHz/100 nS Universal Counter	\$450.00
Country botton, nower 1 GHz C-ch	
HP 5315B 100 MHz/ 100 nS Universal Counter HP 5316A 100 MHz/100 nS Universal Counter, HPIB HP 5316A-001,003 100 MHz/ 100 nS Univ	\$500.00
HP 5316A 100 MHz/100 nS Universal Counter, HPIB	\$600.00
HP 5316B 100 MHz/ 100 nS Universal Counter, HPIB	\$1,000.00
HP 5334A 100 MHz Universal Counter, HPIB	\$750.00
OCXO, DVM, 1.3 GHz C-ch., rear in	\$1,000.00
HP 5334B-010,060 100 MHz	\$750.00
Universal Counter, HPIB, OCXO HP 5335A 200 MHz Universal / Statistical Counter	\$1 200 no
PHILIPS PM6665/431 120 MHz/ 100 nS	\$600.00
Universal Counter, 1.3 GHz C-ch., TCXO TEK DC5004 Programmable 100 MHz/100nS	
TEK DC5004 Programmable 100 MHz/100nS Counter/Timer, TM5000 series	\$250.00
TEK DC5009 Programmable 135 MHz Univ.	\$400.00
Counter/Timer TM5000 series	
TEK DC5010 350 MHz / 3.125 nS	\$1,200.00
Universal Counter, TM5000 series	
FREQUENCY COUNTERS	** ***
EIP 575 18 GHz Source Locking Counter, GPIB	\$4,000.00
Locking Counter; nower meas ()(:X()	
HP 5340A 18 GHz Frequency Counter	\$1,000.00
HP 5340A 18 GHz Frequency Counter HP 5342A 18 GHz Frequency Counter HP 5342A-001 18 GHz Frequency	\$2,000.00
Counter, OCXO reference	
HP 5342A-001,011 18 GHz Frequency	\$2,400.00
Counter, OCXO reference & HPIB HP 5342A-003 18 GHz Freq.Counter,	\$2,000,00
122 dBm 20 dBm dynamic range	
HP 5342A-01,04,05 24 GHz Frequency	\$3,250.00
Counter, OCXO, DAC HP 5343A-001 26.5 GHz Frequency	\$4 500 00
Counter OCXO reference	
HP 5345A/5355A/5356B 26.5 GHz	\$4,000.00
CW/Pulse Frequency Counter	6500.00
HP 5384A 225 MHz Frequency Counter, HPIB HP 5385A 1 GHz Frequency Counter, HPIB TEK DP501 1.3 GHz Prescaler,	\$750.00
TEK DP501 1.3 GHz Prescaler,	\$225.00
divide by 16, TM500 series	
STANDARDS	-
HP 105A Quartz Oscillator, 0.1/ 1.0/ 5.0 MHz	\$750.00
HP 105B Quartz Oscillator, 0.1/1.0/5.0 MHz, battery power	\$1,500.00
HP 5087A-4.11.01x8.12x4 Dist. Amp.	\$1,500.00
eight 5 MHz outputs, four 10 MHz outputs HP 5087A-opt.033 Distribution	A4 700 00
HP 5087A-opt.033 Distribution	\$1,750.00
Amplitier; 12 outputs at 10 MH2	

AUDIO & BASEBAND

SPEC	TOUN	ANIA	IVEIC
SPEU	INUIN	MINM	1010

HP 3586C Selective Level Meter, 50 Hz-32.5 MHz, 50 & 75 ohms \$1,500.00



90 DAY WARRANTY PARTS AND LABOR • 10 DAY INSPECTION TEST EQUIPMENT WANTED CALL OR FAX LIST . OPEN ACCOUNTS



TEK 7L5/L3/R7603 Spectrum Analyzer,	\$1,500.00
DISTORTION ANALYZERS	
HP 339A Distortion Analyzer, built-in low distortion osc HP 8903A-001 Audio Analyzer,	\$1,250.00 \$2,000.00
20 Hz-100 kHz; rear panel input HP 8903B-001,013,051 Audio Analyzer,	
TEK DA4084 Programmable Distortion Analyzer	\$1,000.00
RMS VOLTMETERS	
FLUKE 8920A True RMS Voltmeter,	\$450.00
180 uV-700 V, 10 Hz-20 MHz FLUKE 8922A True RMS Voltmeter,	6450.00
180 uV-700 V, 2 Hz-11 MHz	\$450.00
HP 209A Sine/Square Wave Generator,	\$225.00
4 Hz-2 MHz, 5 VRMS max.	
OSCILLATORS	The second
HP 3336C Synthesizer/ Level	
TEK SG5010 Programmable	\$2,750.00
Oscillator 10 Ha 103 0 kHa	
TEK SG502 Sine/Square Osc., 5 Hz-500 kHz, 70 dB step atten.,TM500	\$200.00
MICCELLANEOUS	
HP 3575A-003 Phase-Gain Meter,	\$850.00
1 Hz-13 MHz dual display option	
HP 4437A Step Attenuator, 0-119.9 dB, DC-1 MHz, 600 ohms unbal.	\$175.00
HP 461A Amplifier, 20/40 dB,	\$125.00
1 kHz-150 MHz, 0.5 V/50 Ohms	
KROHN-HITE 3103 High/Low Pass Filter,	\$400.00
KROHN-HITE 3342R Dual HP/LP Filter,	\$1,100.00
0.001 Hz-99.9 kHz, 48 dB/octave KROHN-HITE 3750 LP/HP/BP/BR Filter,	\$700.00
0.02 Hz-20 kHz, 6/12/18/24 dB/oct.	
KROHN-HITE DCA-10R 10 Watt Amplifier,	\$450.00
20 dB gain, DC-1 MHz, 600-1000 Ohms ROCKLAND 852 Dual Highpass/Lowpass	\$1,000,00
Filter 0.1 Hz-111 kHz	The second secon
TEK AF501 Tunable Bandpass Filter /	\$300.00
Amplifier, 3 Hz-35 kHz TEK AM502 Differential Amplifier,	\$475.00
0.1 Hz-1 MHz, TM500 series	=
RF & MICROWAVE	

SPECTRUM ANALYZERS	
HP 11517A/19A/20A Mixer Set,	\$600.00
18.0-40.0 GHz, for HP 8555A/8569A	\$1 100 00
HP 11970K WR42 Harmonic Mixer, 18.0-26.5 GHz	\$1,100.00
HP 11970Q WR22 Harmonic Mixer, 33-50 GHz	\$1,400.00
HP 11970U WR19 Harmonic Mixer, 40-60 GHz	\$1,400.00
0.5-1500 MHz. for 8554.8568.etc.	\$1,250.00
0.5-1500 MHz, for 8554,8568,etc. HP 8445B Preselector, 1.8-18.0 GHz, for HP 8555A HP 8565A-100 Spectrum Analyzer, 10 MHz-22 GHz, 100 Hz min. res. HP 8566B Spectrum An., 100 Hz-22 GHz,	\$650.00
HP 8565A-100 Spectrum Analyzer,	\$4,500.00
HP 8566B Spectrum An., 100 Hz-22 GHz,	\$37,500.00
HP 8569B Spectrum Analyzer,	\$7,500.00
10 MHz-22 GHz, 100 Hz min.res.bw. TEK 7L14-039/7603 Spectrum Analyzer,	\$2,500.00
1 kHz-2.5 GHz, 30 Hz min. res. bw. TEK TH303 Tracking Generator,	*****
TEK TR503 Tracking Generator,	\$850.00
TEK WM782V WR15 Harmonic Mixer, 50-75 GHz	\$1,500.00
NETWORK ANALYZERS HP 85021C Directional Bridge, 0.01-18 GHz, 33 dB dir,for 8755/6/7 HP 8756A Scalar Network Analyzer	\$1,000.00
0.01-18 GHz, 33 dB dir,for 8755/6/7	
SIGNAL GENERATORS FLUKE 6060A Synthesized Signal Gen.,	The same of the
FLUKE 6060A Synthesized Signal Gen.,	\$2,750.00
0.1-1050 MHz, 10 Hz res., GPIB FLUKE 6060A/AN Synthesized Signal	\$1,750.00
Gen.,10 kHz-520 MHz, 10 Hz res.,GPIB FLUKE 6062A Synthesized Signal Gen.,	
FLUKE 6062A Synthesized Signal Gen.,	\$5,000.00
0.1-2100 MHz, 10 Hz res., GPIB GIGATRONICS 600/10-18 Synthesized	\$3,000.00
Source, 10-18 GHz, 1 kHz res., GPIB GIGATRONICS 875/50 Levelled Multiplier,	
GIGATRONICS 875/50 Levelled Multiplier,	\$2,500.00
x4, 50.0-75.0 GHz output, -3 dBm GIGATRONICS 875/86 Levelled Multiplier,	\$3,750.00
26.5-40.0 & 50.0-75.0 GHz outputs	
GIGATRONICS 900/2-8 Synthesized	\$3,000.00
Signal/Sweep Gen., 2-8 GHz, 1 kHz res.,GPl8 HP 11720A Pulse Modulator, 2-18 GHz, 80 dB on/off ratio . HP 85100V Frequency Mult,	\$750.00
HP 85100V Frequency Mult.,	\$3,750.00
10-15 GHz in / 50-75 GHz out >0 dBm HP 8640B-001,002 Signal Gen.,	\$1 750 00
HP 8656A Synthesized Signal Gen.,	\$2,500.00
U.1-990 MHz, 100 Hz res., HPIB HP 86574-002 Signal Generator	\$3 250 00
0.5-1024 MHZ, AM, FM, Var. audio osc. HP 8656A Synthesized Signal Gen. 0.1-990 MHz, 100 Hz res., HPIB HP 8657A-002 Signal Generator, 0.1-1040 MHz, 10 Hz res., HPIB HP 8660C/86602B-002 Synth Sig. Gen.	40,200.00
HP 8660C/86602B-002 Synth. Sig. Gen.,	\$3,250.00
1-1300 MHz, FM / Phase mod. w/86635A HP 8660C/86603A-002 Synthesizer,	e4 500 00
1-2600 MHz. FM / Phase Mod., w/86635A	\$4,500.00
1-2600 MHz, FM / Phase Mod., w/86635A HP 8683B Signal Generator,	\$3,500.00
2.3-6.5 GHz, AM, WBFM, Pulse HP 8684B Signal Generator,	\$3 500 00
5.4-12.5 GHz, AM, WBFM, Pulse	40,000.00
CWEED CENEDATORS	
Oscillator, 5.9-12.4 GHz, 70 dB step attenuator HP 8350B/83592B-002 Sweep HP 8350B/83592B-002 Sweep	\$4,000.00
Oscillator, 5.9-12.4 GHz, 70 dB step attenuator	
HP 8350B/83592B-002 Sweep	\$14,500.00
Generator, 10 MHz-20 GHz, 70 dB step attenuator HP 83545A RF Plug-in,	\$1,750.00
5.9-12.4 GHz, +17 dBm levelled HP 8601A Generator/Sweeper,	A
HP 8601A Generator/Sweeper,	\$400.00
HP 8601A Generator/Sweeper, 0.1-110 MHz, +20 dBm levelled	\$400.00

HP 8620C Sweep Oscillator Frame	\$550.00
HP 86222B-002 RF Plug-in,	1,500.00
HP 86230B RF Plug-in, 1.8-4.2 GHz, +10 dBm unlevelled HP 86235A-001,002 RF Plug-in,	\$500.00
1.7-4.3 GHz, +14 dBm levelled, 70 dB atten,	\$600.00
1.7-4.3 GHz, +14 dBm levelled, 70 dB atten, HP 86240C RF Plug-in, 3.6-8.6 GHz, +16 dBm levelled HP 86241A-001 RF Plug-in,	\$700.00
HP 86241A-001 RF Plug-in,	\$300.00
3.2-6.5 GHz, +8 dBm levelled HP 86242D-004,008 RF Plug-In,	\$300.00
5.9-9.0 GHz, +10 dBm levelled HP 86250D RF Plug-in,	\$500.00
8.0-12.4 GHz, +10 dBm levelled HP 86260A RF Plug-in, 12.0-18.0 GHz,	
+10 dBm unlevelled HP 86260A-H04 RF Plug-in, 10.0-15.0 GHz,	
40 dD-s to thank	
HP 86290A RF Plug-in, 2.0-18.0 GHz, +7 dBm levelled HP 88290B RF Plug-in, 2.0-18.6 GHz, +10 dBm levelled WAVETEK 962 Sweep Generator,	\$2,000.00
1.0-4.0 GHz, markers, +12 dBm univid.	\$1,500.00
1.0-4.0 GHz, markers, +12 dBm unlvld. WILTRON 6619A Sweep Generator, 2-8 GHz, +10 dBm levelled	\$1,500.00
POWER METERS	
ANRITSU MA72B Power Sensor,	\$300.00
-20 to +20 dBm, 0.01-18 GHz ANRITSU MP-81B/ML-83A Power	\$2,500.00
ANRITSU MP-81B/ML-83A Power Meter, 75-110 GHz (WR10), -20 to +20 dBm BIRD 4410A/4410-1 Wattmeter,	\$350.00
with 200-535 kHz 10 W-10 kW element BOONTON 4200-01A,03/8-4A x2 Dual Channel Microwattmeter, w/(2) 1 MHz-7 GHz sensors BOONTON 42B/41-4B Analog Power	\$1 500 00
Dual Channel Microwattmeter, w/(2) 1 MHz-7 GHz sensors	\$1,000.00 \$275.00
BOONTON 42B/41-4E Analog Power Meter, with 1 MHz-18 GHz sensor	
GENERAL MICROWAVE 476/4240A	\$300.00
HP 4354/H4R1 & Power Meter	59000000
10 MHz-18 GHz, -30 to +20 dBm HP 435A/8482H Power Meter, 0.1-4200 MHz, -10 to +34 dBm HP 435B/8482B Power Meter, 0 to +43 dBm, 100 kHz-4.2 GHz	\$950.00
0.1-4200 MHz, -10 to +34 dBm	\$1,800.00
0 to +43 dBm, 100 kHz-4.2 GHz	8500.00
HP 8477A Power Meter Calibrator, for HP 432 series	\$350.00
18.0-26.5 GHz, for 432 series HP Q8486A Power Sensor,	\$1,500.00
33.0-50.0 GHz, WR22, for 435/6/7/8	\$350.00
Mount, 26.5-40 GHz, for 432 series	9000.00
RF MILLIVOLTMETERS	6500.00
BOONTON 92B-opt.05 RF Millivoltmeter, 10 kHz-1.2 GHz, 75 Ohms scale RACAL 9303 TRMS Level Meter,	
10 kHz 2 CHz -77 to 122 dBm CDIR	
AMPLIFIEDS MISCELL ANEOUS	
AMPLIFIERS, MISCELLANEOUS AMPLIFIER RESEARCH 1W1000	\$650.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt 01A Modulation	\$900.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AW/EM Test Source	\$900.00 \$1,600.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AW/EM Test Source	\$900.00 \$1,600.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms	\$900.00 \$1,600.00 \$300.00 \$125.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms	\$900.00 \$1,600.00 \$300.00 \$125.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0,1-400 MHz, 5 dB NF, +6 dBm output HP 8447E Amplifier, 22 dB, 0.1-1300 MHz,	\$900.00 \$1,600.00 \$300.00 \$125.00 \$375.00 \$750.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0,1-400 MHz, 5 dB NF, +6 dBm output HP 8447E Amplifier, 22 dB, 0.1-1300 MHz,	\$900.00 \$1,600.00 \$300.00 \$125.00 \$375.00 \$750.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0,1-400 MHz, 5 dB NF, +6 dBm output HP 8447E Amplifier, 22 dB, 0.1-1300 MHz,	\$900.00 \$1,600.00 \$300.00 \$125.00 \$375.00 \$750.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0,1-400 MHz, 5 dB NF, +6 dBm output HP 8447E Amplifier, 22 dB, 0.1-1300 MHz,	\$900.00 \$1,600.00 \$300.00 \$125.00 \$375.00 \$750.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447E Amplifier, 20 dB, 13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz, HP 8901A Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1,2,3 Modulation An, 0.15-1300 MHz, rear input, OCXO, ext.LO HP 8970A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier,	\$900.00 \$1,600.00 \$300.00 \$125.00 \$375.00 \$750.00 \$1,200.00 \$4,000.00 \$5,000.00 \$1,500.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447E Amplifier, 20 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901A Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1,2,3 Modulation An, 0.15-1300 MHz, rear input, OCXO, ext.LO HP 8970A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4.0-8.0 GHz, 10 Watts output MICROWAVE SEMUL CORP MC5112 Noise Source.	\$900.00 \$1,600.00 \$300.00 \$125.00 \$375.00 \$1,200.00 \$3,000.00 \$4,000.00 \$5,000.00 \$1,500.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447F Amplifier, 22 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901B-1, 2,3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1, 2,3 Modulation Analyzer, 150 kHz-1300 MHz HP 8970A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4,0-8,0 GHz, 10 Watts output MICROWAVE SEMI.CORP. MCS112 Noise Source, 25.5 dB ENR, 1,0-12.4 GHz, N(m), +28 VDC ROHDE & SCHWARTZ ESH2 Test	\$900.00 \$1,600.00 \$300.00 \$125.00 \$375.00 \$1,200.00 \$3,000.00 \$4,000.00 \$5,000.00 \$1,500.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447E Amplifier, 20 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901A Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1,2,3 Modulation An, 0.15-1300 MHz, rear input, OCXO, ext.LO HP 8970A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4.0-8.0 GHz, 10 Watts output MICROWAVE SEMUL CORP MC5112 Noise Source.	\$900.00 \$1,600.00 \$300.00 \$125.00 \$375.00 \$1,200.00 \$3,000.00 \$4,000.00 \$5,000.00 \$1,500.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447F Amplifier, 22 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901B-1, 2,3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1, 2,3 Modulation Analyzer, 150 kHz-1300 MHz HP 8970A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4,0-8,0 GHz, 10 Watts output MICROWAVE SEMI.CORP. MCS112 Noise Source, 25.5 dB ENR, 1,0-12.4 GHz, N(m), +28 VDC ROHDE & SCHWARTZ ESH2 Test	\$900.00 \$1,600.00 \$300.00 \$125.00 \$375.00 \$1,200.00 \$3,000.00 \$4,000.00 \$1,500.00 \$5,000.00 \$5,000.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447F Amplifier, 22 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901B-1 2.3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1 2.3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1 2.3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1 (2.3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1 (2.3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1 (2.3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1 (2.4 MHz) MHz, 150 kHz-1300 MHz HP 8901B-1 (2.5 MHz) MHz, 150 kHz-1300 MHz HP 8901B-1 (2.5 MHz) MHz Hz-1300 MHz HP 8901B-1 (2.5 MHz) MHz Hz-1300 MHz HP 8901B-1 (2.5 MHz) MHz Hz-1300 MHz HP 8901B-1 (2.5 MHz) MHz Hz-130 MHz HP 8901B-1 (2.5 MHz) MHZ Hz-130 MHz HP 8901B-1 (2.5 MHz) MHZ Hz-130 MHz COAXIAL & WAVEGUIDE	\$900.00 \$1,600.00 \$300.00 \$125.00 \$750.00 \$1,200.00 \$4,000.00 \$5,000.00 \$1,500.00 \$5,000.00 \$5,000.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447F Amplifier, 22 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901B-1, 2,3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1, 2,3 Modulation Analyzer, 150 kHz-1300 MHz HP 8970A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4.0-8.0 GHz, 10 Watts output MICROWAVE SEMI, CORP, MCS112 Noise Source, 25.5 dB ENR, 1.0-12.4 GHz, N(m), +28 VDC ROHDE & SCHWARTZ ESH2 Test Receiver, 9 kHz-30 MHz COAXIAL & WAVEGUIDE AMERICAN NUCLEONICS AM-432 Cauthy Backed Soiral Antenna LHC, 2-18 GHz TNC/ft, TNEW	\$900.00 \$1,600.00 \$300.00 \$125.00 \$750.00 \$1,200.00 \$3,000.00 \$4,000.00 \$5,000.00 \$5,000.00 \$5,000.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447F Amplifier, 22 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901B-1, 2,3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1, 2,3 Modulation Analyzer, 150 kHz-1300 MHz HP 8970A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4.0-8.0 GHz, 10 Watts output MICROWAVE SEMI, CORP, MCS112 Noise Source, 25.5 dB ENR, 1.0-12.4 GHz, N(m), +28 VDC ROHDE & SCHWARTZ ESH2 Test Receiver, 9 kHz-30 MHz COAXIAL & WAVEGUIDE AMERICAN NUCLEONICS AM-432 Cauthy Backed Soiral Antenna LHC, 2-18 GHz TNC/ft, TNEW	\$900.00 \$1,600.00 \$300.00 \$125.00 \$750.00 \$1,200.00 \$3,000.00 \$4,000.00 \$5,000.00 \$5,000.00 \$5,000.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20'40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447F Amplifier, 20 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901A Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1.2,3 Modulation An, 0.15-1300 MHz, rear input, OCXO, ext.LO HP 8970A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4.0-8.0 GHz, 10 Watts output MICROWAVE SEMI, CORP, MC5112 Noise Source, 25.5 dB ENR, 1.0-12.4 GHz, N(m), +28 VDC ROHDE & SCHWARTZ ESH2 Test Receiver, 9 kHz-30 MHz COAXIAL & WAVEGUIDE AMERICAN NUCLEONICS AM-432 Cavity Backed Spiral Antenna, LHC, 2-18 GHz, TNC(f) "NEV FXR/MICROLAB S3-02N Triple Stub Tuner, 200-1000 MHz, 100 Watts max., N(m/f) GR 874-LTL Constant Impedance	\$900.00 \$1,600.00 \$300.00 \$125.00 \$175.00 \$1,200.00 \$3,000.00 \$4,000.00 \$1,500.00 \$5,000.00 \$5,000.00 \$5,000.00 \$1,500.00 \$1,500.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20'40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447F Amplifier, 20 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901A Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1.2,3 Modulation An, 0.15-1300 MHz, rear input, OCXO, ext.LO HP 8970A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4.0-8.0 GHz, 10 Watts output MICROWAVE SEMI, CORP, MC5112 Noise Source, 25.5 dB ENR, 1.0-12.4 GHz, N(m), +28 VDC ROHDE & SCHWARTZ ESH2 Test Receiver, 9 kHz-30 MHz COAXIAL & WAVEGUIDE AMERICAN NUCLEONICS AM-432 Cavity Backed Spiral Antenna, LHC, 2-18 GHz, TNC(f) "NEV FXR/MICROLAB S3-02N Triple Stub Tuner, 200-1000 MHz, 100 Watts max., N(m/f) GR 874-LTL Constant Impedance	\$900.00 \$1,600.00 \$300.00 \$125.00 \$175.00 \$1,200.00 \$3,000.00 \$4,000.00 \$1,500.00 \$5,000.00 \$5,000.00 \$5,000.00 \$1,500.00 \$1,500.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20'40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447F Amplifier, 20 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901A Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1.2,3 Modulation An, 0.15-1300 MHz, rear input, OCXO, ext.LO HP 8970A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4.0-8.0 GHz, 10 Watts output MICROWAVE SEMI, CORP, MC5112 Noise Source, 25.5 dB ENR, 1.0-12.4 GHz, N(m), +28 VDC ROHDE & SCHWARTZ ESH2 Test Receiver, 9 kHz-30 MHz COAXIAL & WAVEGUIDE AMERICAN NUCLEONICS AM-432 Cavity Backed Spiral Antenna, LHC, 2-18 GHz, TNC(f) "NEV FXR/MICROLAB S3-02N Triple Stub Tuner, 200-1000 MHz, 100 Watts max., N(m/f) GR 874-LTL Constant Impedance	\$900.00 \$1,600.00 \$300.00 \$125.00 \$175.00 \$1,200.00 \$3,000.00 \$4,000.00 \$1,500.00 \$5,000.00 \$5,000.00 \$5,000.00 \$1,500.00 \$1,500.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20'40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447F Amplifier, 20 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901A Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1.2,3 Modulation An, 0.15-1300 MHz, rear input, OCXO, ext.LO HP 8970A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4.0-8.0 GHz, 10 Watts output MICROWAVE SEMI, CORP, MC5112 Noise Source, 25.5 dB ENR, 1.0-12.4 GHz, N(m), +28 VDC ROHDE & SCHWARTZ ESH2 Test Receiver, 9 kHz-30 MHz COAXIAL & WAVEGUIDE AMERICAN NUCLEONICS AM-432 Cavity Backed Spiral Antenna, LHC, 2-18 GHz, TNC(f) "NEV FXR/MICROLAB S3-02N Triple Stub Tuner, 200-1000 MHz, 100 Watts max., N(m/f) GR 874-LTL Constant Impedance	\$900.00 \$1,600.00 \$300.00 \$125.00 \$1750.00 \$1,200.00 \$3,000.00 \$4,000.00 \$1,500.00 \$5,000.00 \$5,000.00 \$5,000.00 \$1,500.00 \$1,500.00 \$1,500.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20'40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447F Amplifier, 20 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901A Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1.2,3 Modulation An, 0.15-1300 MHz, rear input, OCXO, ext.LO HP 8970A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4.0-8.0 GHz, 10 Watts output MICROWAVE SEMI, CORP, MC5112 Noise Source, 25.5 dB ENR, 1.0-12.4 GHz, N(m), +28 VDC ROHDE & SCHWARTZ ESH2 Test Receiver, 9 kHz-30 MHz COAXIAL & WAVEGUIDE AMERICAN NUCLEONICS AM-432 Cavity Backed Spiral Antenna, LHC, 2-18 GHz, TNC(f) "NEV FXR/MICROLAB S3-02N Triple Stub Tuner, 200-1000 MHz, 100 Watts max., N(m/f) GR 874-LTL Constant Impedance	\$900.00 \$1,600.00 \$300.00 \$125.00 \$1750.00 \$1,200.00 \$3,000.00 \$4,000.00 \$1,500.00 \$5,000.00 \$5,000.00 \$5,000.00 \$1,500.00 \$1,500.00 \$1,500.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447A Amplifier, 22 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901A Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1,2,3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1,2,3 Modulation An. 0.15-1300 MHz, rear input, OCXO, ext.LO HP 8970A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4.0-8.0 GHz, 10 Watts output MICROWAVE SEMILCORP, MC5112 Noise Source, 25.5 dB ENR, 1.0-12.4 GHz, N(m), +28 VDC ROHDE & SCHWARTZ ESH2 Test Receiver, 9 kHz-30 MHz COAXIAL & WAVEGUIDE AMERICAN NUCLEONICS AM-432 Cavity Backed Spiral Antenna,LHC, 2-18 GHz,TNC(f) *NEV FXFVMICROLAB S3-02N Triple Stub Tuner, 200-1000 MHz, 100 Watts max., N(m/f) GR 874-LTL Constant Impedance Trombone Line, 0-44 cm, DC-2 GHz GR 900-Q GR900 14mm Interseries Adapters HP 11590A-001 Bias Network, 1.0-18.0 GHz, APC7 HP 11612A Bias Network, 45 MHz-26.5 GHz, APC3.5 HP 11691D Directional Coupler, 20 dB, 2-18 GHz HP 777D Dual Directional Coupler, 20 dB, 1.9-4.1 GHz HP 778D-011 Dual Dir. Coupler,	\$900.00 \$1,600.00 \$300.00 \$125.00 \$375.00 \$1,200.00 \$3,000.00 \$4,000.00 \$5,000.00 \$5,000.00 \$5,000.00 \$1,500.00 \$1,500.00 \$1,500.00 \$275.00 \$400.00 \$450.00 \$450.00 \$450.00 \$275.00 \$275.00 \$275.00 \$275.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447A Amplifier, 22 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901A Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1,2,3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1,2,3 Modulation An. 0.15-1300 MHz, rear input, OCXO, ext.LO HP 8970A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4.0-8.0 GHz, 10 Watts output MICROWAVE SEMILCORP, MC5112 Noise Source, 25.5 dB ENR, 1.0-12.4 GHz, N(m), +28 VDC ROHDE & SCHWARTZ ESH2 Test Receiver, 9 kHz-30 MHz COAXIAL & WAVEGUIDE AMERICAN NUCLEONICS AM-432 Cavity Backed Spiral Antenna,LHC, 2-18 GHz,TNC(f) *NEV FXFVMICROLAB S3-02N Triple Stub Tuner, 200-1000 MHz, 100 Watts max., N(m/f) GR 874-LTL Constant Impedance Trombone Line, 0-44 cm, DC-2 GHz GR 900-Q GR900 14mm Interseries Adapters HP 11590A-001 Bias Network, 1.0-18.0 GHz, APC7 HP 11612A Bias Network, 45 MHz-26.5 GHz, APC3.5 HP 11691D Directional Coupler, 20 dB, 2-18 GHz HP 777D Dual Directional Coupler, 20 dB, 1.9-4.1 GHz HP 778D-011 Dual Dir. Coupler,	\$900.00 \$1,600.00 \$300.00 \$125.00 \$375.00 \$1,200.00 \$3,000.00 \$4,000.00 \$5,000.00 \$5,000.00 \$5,000.00 \$1,500.00 \$1,500.00 \$1,500.00 \$275.00 \$400.00 \$450.00 \$450.00 \$450.00 \$275.00 \$275.00 \$275.00 \$275.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447A Amplifier, 22 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901A Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1,2,3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1,2,3 Modulation An. 0.15-1300 MHz, rear input, OCXO, ext.LO HP 8970A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4.0-8.0 GHz, 10 Watts output MICROWAVE SEMILCORP, MC5112 Noise Source, 25.5 dB ENR, 1.0-12.4 GHz, N(m), +28 VDC ROHDE & SCHWARTZ ESH2 Test Receiver, 9 kHz-30 MHz COAXIAL & WAVEGUIDE AMERICAN NUCLEONICS AM-432 Cavity Backed Spiral Antenna,LHC, 2-18 GHz,TNC(f) *NEV FXFVMICROLAB S3-02N Triple Stub Tuner, 200-1000 MHz, 100 Watts max., N(m/f) GR 874-LTL Constant Impedance Trombone Line, 0-44 cm, DC-2 GHz GR 900-Q GR900 14mm Interseries Adapters HP 11590A-001 Bias Network, 1.0-18.0 GHz, APC7 HP 11612A Bias Network, 45 MHz-26.5 GHz, APC3.5 HP 11691D Directional Coupler, 20 dB, 2-18 GHz HP 777D Dual Directional Coupler, 20 dB, 1.9-4.1 GHz HP 778D-011 Dual Dir. Coupler,	\$900.00 \$1,600.00 \$300.00 \$125.00 \$375.00 \$1,200.00 \$3,000.00 \$4,000.00 \$5,000.00 \$5,000.00 \$5,000.00 \$1,500.00 \$1,500.00 \$1,500.00 \$275.00 \$400.00 \$450.00 \$450.00 \$450.00 \$275.00 \$275.00 \$275.00 \$275.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447A Amplifier, 22 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901A Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1,2,3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1,2,3 Modulation An. 0.15-1300 MHz, rear input, OCXO, ext.LO HP 8970A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4.0-8.0 GHz, 10 Watts output MICROWAVE SEMILCORP, MC5112 Noise Source, 25.5 dB ENR, 1.0-12.4 GHz, N(m), +28 VDC ROHDE & SCHWARTZ ESH2 Test Receiver, 9 kHz-30 MHz COAXIAL & WAVEGUIDE AMERICAN NUCLEONICS AM-432 Cavity Backed Spiral Antenna,LHC, 2-18 GHz,TNC(f) *NEV FXFVMICROLAB S3-02N Triple Stub Tuner, 200-1000 MHz, 100 Watts max., N(m/f) GR 874-LTL Constant Impedance Trombone Line, 0-44 cm, DC-2 GHz GR 900-Q GR900 14mm Interseries Adapters HP 11590A-001 Bias Network, 1.0-18.0 GHz, APC7 HP 11612A Bias Network, 45 MHz-26.5 GHz, APC3.5 HP 11691D Directional Coupler, 20 dB, 2-18 GHz HP 777D Dual Directional Coupler, 20 dB, 1.9-4.1 GHz HP 778D-011 Dual Dir. Coupler,	\$900.00 \$1,600.00 \$300.00 \$125.00 \$375.00 \$1,200.00 \$3,000.00 \$4,000.00 \$5,000.00 \$5,000.00 \$5,000.00 \$1,500.00 \$1,500.00 \$1,500.00 \$275.00 \$400.00 \$450.00 \$450.00 \$450.00 \$275.00 \$275.00 \$275.00 \$275.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447F Amplifier, 22 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901A Modulation Analyzer, 150 kHz-1300 MHz HP 8901A Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-12.3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-12.3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-12.3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-12.4 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-12.4 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-12.4 Modulation Analyzer, 150 kHz-1800 MHz HP 8970A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4.0-8.0 GHz, 10 Watts output MICROWAVE SEMI.CORP. MC5112 Noise Source, 25.5 dB ENR, 1.0-12.4 GHz, N(m), +28 VDC ROHDE & SCHWARTZ ESHZ Test Receiver, 9 kHz-30 MHz COAXIAL & WAVEGUIDE AMERICAN NUCLEONICS AM-432 Cavity Backed Spiral Antenna,LHC, 2-18 GHz,TNC(f) *NEV FXF/MICROLAB S3-02N Triple Stub Tuner, 200-1000 MHz, 100 Watts max., N(m/f) GR 874-LTL Constant Impedance Trombone Line, 0-44 cm, DC-2 GHz GR 900-Q GR900 14mm Interseries Adapters HP 11590A-001 Bias Network, 10-18.0 GHz, APC7 HP 11612A Bias Network, 45 MHz-26.5 GHz, APC3.5 HP 1169D Directional Coupler, 20 dB, 215-450 MHz HP 774D Dual Directional Coupler, 20 dB, 215-450 MHz HP 778D-011 Dual Directional Coupler, 20 dB, 19-4.1 GHz HP 778D Dual Directional Coupler, 20 dB, 19-4.1 GHz HP 778D-011 Dual Directional Coupler, 20 dB, 19-4.1 GHz HP 778D-011 Dual Directional Coupler, 20 dB, 19-4.1 GHz HP 778D-011 Dual Directional Coupler, 20 dB, 19-4.1 GHz HP 778D-011 Dual Directional Coupler, 20 dB, 19-4.1 GHz HP 778D-011 Dual Directional Coupler, 20 dB, 19-4.1 GHz H	\$900.00 \$1,600.00 \$1,600.00 \$1,25.00 \$750.00 \$1,200.00 \$3,000.00 \$4,000.00 \$5,000.00 \$5,000.00 \$5,000.00 \$1,500.00 \$275.00 \$450.00 \$450.00 \$275.00 \$450.00 \$275.00 \$450.00 \$275.00 \$300.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447F Amplifier, 22 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901A Modulation Analyzer, 150 kHz-1300 MHz HP 8901A Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-12.3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-12.3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-12.3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-12.4 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-12.4 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-12.4 Modulation Analyzer, 150 kHz-1800 MHz HP 8970A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4.0-8.0 GHz, 10 Watts output MICROWAVE SEMI.CORP. MC5112 Noise Source, 25.5 dB ENR, 1.0-12.4 GHz, N(m), +28 VDC ROHDE & SCHWARTZ ESHZ Test Receiver, 9 kHz-30 MHz COAXIAL & WAVEGUIDE AMERICAN NUCLEONICS AM-432 Cavity Backed Spiral Antenna,LHC, 2-18 GHz,TNC(f) *NEV FXF/MICROLAB S3-02N Triple Stub Tuner, 200-1000 MHz, 100 Watts max., N(m/f) GR 874-LTL Constant Impedance Trombone Line, 0-44 cm, DC-2 GHz GR 900-Q GR900 14mm Interseries Adapters HP 11590A-001 Bias Network, 10-18.0 GHz, APC7 HP 11612A Bias Network, 45 MHz-26.5 GHz, APC3.5 HP 1169D Directional Coupler, 20 dB, 215-450 MHz HP 774D Dual Directional Coupler, 20 dB, 215-450 MHz HP 778D-011 Dual Directional Coupler, 20 dB, 19-4.1 GHz HP 778D Dual Directional Coupler, 20 dB, 19-4.1 GHz HP 778D-011 Dual Directional Coupler, 20 dB, 19-4.1 GHz HP 778D-011 Dual Directional Coupler, 20 dB, 19-4.1 GHz HP 778D-011 Dual Directional Coupler, 20 dB, 19-4.1 GHz HP 778D-011 Dual Directional Coupler, 20 dB, 19-4.1 GHz HP 778D-011 Dual Directional Coupler, 20 dB, 19-4.1 GHz H	\$900.00 \$1,600.00 \$1,600.00 \$1,25.00 \$750.00 \$1,200.00 \$3,000.00 \$4,000.00 \$5,000.00 \$5,000.00 \$5,000.00 \$1,500.00 \$275.00 \$450.00 \$450.00 \$275.00 \$450.00 \$275.00 \$450.00 \$275.00 \$300.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447F Amplifier, 22 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901A Modulation Analyzer, 150 kHz-1300 MHz HP 8901A Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-12.3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-12.3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-12.3 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-12.4 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-12.4 Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-12.4 Modulation Analyzer, 150 kHz-1800 MHz HP 8970A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4.0-8.0 GHz, 10 Watts output MICROWAVE SEMI.CORP. MC5112 Noise Source, 25.5 dB ENR, 1.0-12.4 GHz, N(m), +28 VDC ROHDE & SCHWARTZ ESHZ Test Receiver, 9 kHz-30 MHz COAXIAL & WAVEGUIDE AMERICAN NUCLEONICS AM-432 Cavity Backed Spiral Antenna,LHC, 2-18 GHz,TNC(f) *NEV FXF/MICROLAB S3-02N Triple Stub Tuner, 200-1000 MHz, 100 Watts max., N(m/f) GR 874-LTL Constant Impedance Trombone Line, 0-44 cm, DC-2 GHz GR 900-Q GR900 14mm Interseries Adapters HP 11590A-001 Bias Network, 10-18.0 GHz, APC7 HP 11612A Bias Network, 45 MHz-26.5 GHz, APC3.5 HP 1169D Directional Coupler, 20 dB, 215-450 MHz HP 774D Dual Directional Coupler, 20 dB, 215-450 MHz HP 778D-011 Dual Directional Coupler, 20 dB, 19-4.1 GHz HP 778D Dual Directional Coupler, 20 dB, 19-4.1 GHz HP 778D-011 Dual Directional Coupler, 20 dB, 19-4.1 GHz HP 778D-011 Dual Directional Coupler, 20 dB, 19-4.1 GHz HP 778D-011 Dual Directional Coupler, 20 dB, 19-4.1 GHz HP 778D-011 Dual Directional Coupler, 20 dB, 19-4.1 GHz HP 778D-011 Dual Directional Coupler, 20 dB, 19-4.1 GHz H	\$900.00 \$1,600.00 \$1,600.00 \$1,25.00 \$750.00 \$1,200.00 \$3,000.00 \$4,000.00 \$5,000.00 \$5,000.00 \$5,000.00 \$1,500.00 \$275.00 \$450.00 \$450.00 \$275.00 \$450.00 \$275.00 \$450.00 \$275.00 \$300.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447E Amplifier, 22 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901A Modulation Analyzer, 150 KHz-1300 MHz HP 8901B-1, 2, 3 Modulation Analyzer, 150 KHz-1300 MHz HP 8901B-1, 2, 3 Modulation Analyzer, 150 KHz-1300 MHz HP 8907A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4.0-8.0 GHz, 10 Watts output MICROWAVE SEMI. CORP. MC5112 Noise Source, 25.5 dB ENR, 1.0-12.4 GHz, N(m), +28 VDC ROHDE & SCHWARTZ ESH2 Test Receiver, 9 kHz-30 MHz COAXIAL & WAVEGUIDE AMERICAN NUCLEONICS AM-432 Cavity Backed Spiral Antenna, LHC, 2-18 GHz, TNC(f) "NEV FXY/MICROLAB S3-02N Triple Stub Tuner, 200-1000 MHz, 100 Watts max., N(m/f) GR 874-LTL Constant Impedance Trombone Line, 0-44 cm, DC-2 GHz GR 900-Q GR900 14mm Interseries Adapters HP 11590A-001 Bias Network, 1.0-18.0 GHz, APC7 HP 11612A Bias Network, 1.0-18.0 GHz, APC7 HP 177D Dual Directional Coupler, 20 dB, 1.9-4.1 GHz HP 777D Dual Directional Coupler, 20 dB, 1.9-4.1 GHz HP 778D-011 Dual Dir. Coupler, 20 dB, 1.9-4.1 GHz HP 778D-011 Dual Dir. Coupler, 20 dB, 1.9-4.1 GHz HP 8470B Crystal Detector, 10 MHz-18 GHz, neg, pol., SMA HP 8495G-002 Programmable Step Attenuator, 0-70 dB, DC-4 GHz, SMA HP 8495G-002 Programmable Step Attenuator, 0-70 dB, DC-4 GHz, SMA HP 8495G-002 Programmable Step Attenuator, 0-70 dB, DC-4 GHz, SMA HP 8497K-004 Programmable Step	\$900.00 \$1,600.00 \$300.00 \$125.00 \$375.00 \$1,25.00 \$1,500.00 \$1,500.00 \$5,000.00 \$5,000.00 \$1,500.00 \$1,500.00 \$275.00 \$400.00 \$125.00 \$450.00 \$450.00 \$275.00 \$450.00 \$275.00 \$350.00 \$450.00 \$450.00 \$275.00 \$450.00 \$275.00 \$450.00 \$275.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447E Amplifier, 22 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901A Modulation Analyzer, 150 KHz-1300 MHz HP 8901B-1, 2, 3 Modulation Analyzer, 150 KHz-1300 MHz HP 8901B-1, 2, 3 Modulation Analyzer, 150 KHz-1300 MHz HP 8907A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4.0-8.0 GHz, 10 Watts output MICROWAVE SEMI.CORP. MC5112 Noise Source, 25.5 dB ENR, 1.0-12.4 GHz, N(m), +28 VDC ROHDE & SCHWARTZ ESH2 Test Receiver, 9 kHz-30 MHz COAXIAL & WAVEGUIDE AMERICAN NUCLEONICS AM-432 Cavity Backed Spiral Antenna,LHC, 2-18 GHz,TNC(f) *NEV FXV/MICROLAB S3-02N Triple Stub Tuner, 200-1000 MHz, 100 Watts max., N(m/f) GR 874-LTL Constant Impedance Trombone Line, 0-44 cm, DC-2 GHz GR 900-Q GR900 14mm Interseries Adapters HP 11590A-001 Bias Network, 1.0-18.0 GHz, APC7 HP 11612A Bias Network, 1.0-18.0 GHz, APC7 HP 1167D Dual Directional Coupler, 20 dB, 215-450 MHz HP 777D Dual Directional Coupler, 20 dB, 215-450 MHz HP 778D-011 Dual Dir. Coupler, 20 dB, 1.9-4.1 GHz HP 778D-011 Dual Dir. Coupler, 20 dB, 1.9-4.1 GHz HP 778D-011 Dual Dir. Coupler, 20 dB, 1.9-4.1 GHz HP 8470B Crystal Detector, 10 MHz-18 GHz, neg, pol., SMA HP 8496-002 Programmable Step Attenuator, 0-70 dB, DC-4 GHz, SMA HP 8498-002 Programmable Step Attenuator, 0-70 dB, DC-4 GHz, SMA HP 8497-002 Programmable Step Attenuator, 0-70 dB, DC-4 GHz, SMA HP 8497-002 Programmable Step Attenuator, 0-70 dB, DC-6 GHz HP K422A WR42 Flat	\$900.00 \$1,600.00 \$300.00 \$125.00 \$375.00 \$1,250.00 \$1,500.00 \$1,500.00 \$5,000.00 \$5,000.00 \$1,500.00 \$275.00 \$400.00 \$125.00 \$450.00 \$450.00 \$275.00 \$450.00 \$275.00 \$450.00 \$275.00 \$350.00 \$275.00 \$350.00 \$275.00 \$350.00 \$275.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447E Amplifier, 22 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901A Modulation Analyzer, 150 KHz-1300 MHz HP 8901B-1, 2, 3 Modulation Analyzer, 150 KHz-1300 MHz HP 8901B-1, 2, 3 Modulation Analyzer, 150 KHz-1300 MHz HP 8907A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4.0-8.0 GHz, 10 Watts output MICROWAVE SEMI.CORP. MC5112 Noise Source, 25.5 dB ENR, 1.0-12.4 GHz, N(m), +28 VDC ROHDE & SCHWARTZ ESH2 Test Receiver, 9 kHz-30 MHz COAXIAL & WAVEGUIDE AMERICAN NUCLEONICS AM-432 Cavity Backed Spiral Antenna,LHC, 2-18 GHz,TNC(f) *NEV FXV/MICROLAB S3-02N Triple Stub Tuner, 200-1000 MHz, 100 Watts max., N(m/f) GR 874-LTL Constant Impedance Trombone Line, 0-44 cm, DC-2 GHz GR 900-Q GR900 14mm Interseries Adapters HP 11590A-001 Bias Network, 1.0-18.0 GHz, APC7 HP 11612A Bias Network, 1.0-18.0 GHz, APC7 HP 1167D Dual Directional Coupler, 20 dB, 215-450 MHz HP 777D Dual Directional Coupler, 20 dB, 215-450 MHz HP 778D-011 Dual Dir. Coupler, 20 dB, 1.9-4.1 GHz HP 778D-011 Dual Dir. Coupler, 20 dB, 1.9-4.1 GHz HP 778D-011 Dual Dir. Coupler, 20 dB, 1.9-4.1 GHz HP 8470B Crystal Detector, 10 MHz-18 GHz, neg, pol., SMA HP 8496-002 Programmable Step Attenuator, 0-70 dB, DC-4 GHz, SMA HP 8498-002 Programmable Step Attenuator, 0-70 dB, DC-4 GHz, SMA HP 8497-002 Programmable Step Attenuator, 0-70 dB, DC-4 GHz, SMA HP 8497-002 Programmable Step Attenuator, 0-70 dB, DC-6 GHz HP K422A WR42 Flat	\$900.00 \$1,600.00 \$300.00 \$125.00 \$375.00 \$1,250.00 \$1,500.00 \$1,500.00 \$5,000.00 \$5,000.00 \$1,500.00 \$275.00 \$400.00 \$125.00 \$450.00 \$450.00 \$275.00 \$450.00 \$275.00 \$450.00 \$275.00 \$350.00 \$275.00 \$350.00 \$275.00 \$350.00 \$275.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447E Amplifier, 22 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901A Modulation Analyzer, 150 KHz-1300 MHz HP 8901B-1, 2, 3 Modulation Analyzer, 150 KHz-1300 MHz HP 8901B-1, 2, 3 Modulation Analyzer, 150 KHz-1300 MHz HP 8907A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4.0-8.0 GHz, 10 Watts output MICROWAVE SEMI.CORP. MC5112 Noise Source, 25.5 dB ENR, 1.0-12.4 GHz, N(m), +28 VDC ROHDE & SCHWARTZ ESH2 Test Receiver, 9 kHz-30 MHz COAXIAL & WAVEGUIDE AMERICAN NUCLEONICS AM-432 Cavity Backed Spiral Antenna,LHC, 2-18 GHz,TNC(f) *NEV FXV/MICROLAB S3-02N Triple Stub Tuner, 200-1000 MHz, 100 Watts max., N(m/f) GR 874-LTL Constant Impedance Trombone Line, 0-44 cm, DC-2 GHz GR 900-Q GR900 14mm Interseries Adapters HP 11590A-001 Bias Network, 1.0-18.0 GHz, APC7 HP 11612A Bias Network, 1.0-18.0 GHz, APC7 HP 1167D Dual Directional Coupler, 20 dB, 215-450 MHz HP 777D Dual Directional Coupler, 20 dB, 215-450 MHz HP 778D-011 Dual Dir. Coupler, 20 dB, 1.9-4.1 GHz HP 778D-011 Dual Dir. Coupler, 20 dB, 1.9-4.1 GHz HP 778D-011 Dual Dir. Coupler, 20 dB, 1.9-4.1 GHz HP 8470B Crystal Detector, 10 MHz-18 GHz, neg, pol., SMA HP 8496-002 Programmable Step Attenuator, 0-70 dB, DC-4 GHz, SMA HP 8498-002 Programmable Step Attenuator, 0-70 dB, DC-4 GHz, SMA HP 8497-002 Programmable Step Attenuator, 0-70 dB, DC-4 GHz, SMA HP 8497-002 Programmable Step Attenuator, 0-70 dB, DC-6 GHz HP K422A WR42 Flat	\$900.00 \$1,600.00 \$300.00 \$125.00 \$375.00 \$1,250.00 \$1,500.00 \$1,500.00 \$5,000.00 \$5,000.00 \$1,500.00 \$275.00 \$400.00 \$125.00 \$450.00 \$450.00 \$275.00 \$450.00 \$275.00 \$450.00 \$275.00 \$350.00 \$275.00 \$350.00 \$275.00 \$350.00 \$275.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00
Amplifier, 30 dB gain, 1-1000 MHz, 1 Watt output BOONTON 82AD-opt.01A Modulation Meter, AM, FM, 10-1200 MHz, GPIB HP 11715A AM/FM Test Source HP 415E SWR Meter HP 465A Amplifier, 20/40 dB, 5 Hz-1 MHz, 1/2 Watt/50 Ohms HP 8447A Amplifier, 20 dB, 0.1-400 MHz, 5 dB NF, +6 dBm output HP 8447A Amplifier, 22 dB, 0.1-1300 MHz, +13 dBm output HP 8447F Preamplifier / Power Amplifier, 0.1-1300 MHz HP 8901A Modulation Analyzer, 150 kHz-1300 MHz HP 8901A Modulation Analyzer, 150 kHz-1300 MHz HP 8901B-1, 2, 3 Modulation Ana, 0.15-1300 MHz, rear input, OCXO, ext.LO HP 8970A Noise Figure Meter HUGHES 1177H02F000 TWT Amplifier, 4.0-8.0 GHz, 10 Watts output MICROWAVE SEMI.CORP. MC5112 Noise Source, 25.5 dB ENR, 1.0-12.4 GHz, N(m), +28 VDC ROHDE & SCHWARTZ ESHZ Test Receiver, 9 kHz-30 MHz COAXIAL & WAVEGUIDE AMERICAN NUCLEONICS AM-432 Cavity Backed Spiral Antenna,LHC, 2-18 GHz,TNC(f) *NEW FXP/MICROLAB S3-02N Triple Stub Tuner, 200-1000 MHz, 100 Watts max., N(m/f) GR 874-LTL Constant Impedance Trombone Line, 0-44 cm, DC-2 GHz GR 900-Q GR900 14mm Interseries Adapters HP 11590A-001 Bias Network, 10-18.0 GHz, APC7 HP 11612A Bias Network, 45 MHz-26.5 GHz, APC3.5 HP 11612B Bias Network, 45 MHz-26.5 GHz, APC3.5 HP 11612B Bias Network, 45 MHz-26.5 GHz, APC3.5 HP 177D Dual Directional Coupler, 20 dB, 215-450 MHz HP 777D Dual Directional Coupler, 20 dB, 215-450 MHz HP 777D Dual Directional Coupler, 20 dB, 215-450 MHz HP 778D Out Directional Coupler, 20 dB, 19-4.1 GHz HP 778D Out Directional Coupler, 20 dB, 19-4.1 GHz HP 778D Out Directional Coupler, 20 dB, 19-4.1 GHz HP 778D Out Directional Coupler, 20 dB, 19-4.1 GHz HP 778D Out Directional Coupler, 20 dB, 19-4.1 GHz HP 778D Out Directional Coupler, 20 dB, 215-450 MHz HP 778D-011 Dual Directional Coupler, 20 dB, 215-450 MHz HP 778D-011 Dual Directional Coupler, 20 dB, 215-450 MHz HP 778D-011 Dual Directional Coupler, 20 dB, 215-450 MHz HP 84964-002 Programmable Step Attenuator, 0-70 dB, DC-4 GHz, SMA HP 8495G-002 Programmable Step Attenuator, 0-70 dB, DC-4 GHz, SMA HP 8497K-004 Programm	\$900.00 \$1,600.00 \$300.00 \$125.00 \$375.00 \$1,250.00 \$1,500.00 \$1,500.00 \$5,000.00 \$5,000.00 \$1,500.00 \$275.00 \$400.00 \$450.00 \$450.00 \$275.00 \$450.00 \$275.00 \$450.00 \$275.00 \$350.00 \$275.00 \$350.00 \$275.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00 \$350.00

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HP R532A WR28 Frequency Meter, 26.5-40 GHz	\$500.00
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In this column, I answer questions about all aspects of electronics, including computer hardware and software. This column doesn't replace the Tech Forum that you've grown to love and support. Instead, it will supplement it, so feel free to participate as always with your questions and answers. You can send your questions to me by E-Mail at q&a@nutsvolts.com, or by snail mail at Nuts & Volts Magazine, 430 Princeland Ct., Corona, CA 91719.

What's Up:

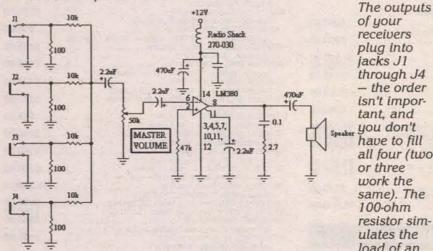
One man's trash is another man's treasure: two types of metal detectors. Transistor basics for want-to-be engineers. Maxim's new family of tunable low-pass filters and an audio mixer. Two Q & A answer updates (space-age stepper motor controller and well-depth gauge), and hard disk hardware fixes.

Mix And Match Audio

Q. I have a simple problem for which I hope you can give me a simple solution. Between scanners, ham radios, and broadcast band, I have more than a couple receivers in my truck. Is there a simple circuit that would combine the audio outputs together via the external speaker (earphone) jack on each rig and run them through one quality speaker? I don't want the output of one rig to feed back into another and cause damage.

John Chaput via Internet

A. Yes, there's a simple solution called an audio mixer. This circuit is used extensively in the recording industry to combine different sound sources - basically, the way the two channels of a stereo recording are created by combining sounds from 16 or more separate sources. Here's a four-input mixer.

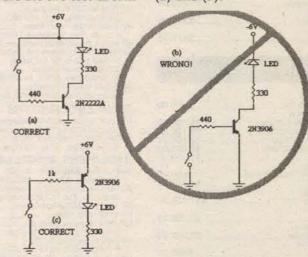


of your receivers plug into iacks J1 through J4 - the order isn't important, and you don't have to fill all four (two or three work the same). The 100-ohm resistor simulates the load of an

earphone, and the 10K resistor prevents the output from feeding back into the other inputs (receivers). The combined inputs now go to an LM380 power amplifier, which gives you enough sound to be heard over the noise of your truck. Make sure to use the Radio Shack hash filter shown, otherwise you'll get more engine noise than you will radio. To use the mixer, turn the Master Volume up full, plug the receiver into the desired jack, and adjust its volume control for the desired loudness. Turn off that receiver and proceed to the next, then the next, etc. After that, use the Master Volume to adjust the sound level. While only four inputs are shown, you can add as many as you wish - well, up to a point. After about a dozen, you may want to consider an intermediate amplifier (an op amp between the 10K resistors and Master Volume control) to make up for the losses. If you want to have some fun, turn on two receivers at the same time and use their respective volume controls to fade from one source to the other, just like the sound engineers do.

Transistor Basics

Q. I know this may be very basic for most of your readers, but I'm trying to do some simple tests with transistors before assembling a more complex design and I cannot get the PNP transistors (2N3906) to work. Here are the two test circuits - (a) and (b).



Closing the switch in circuit (a) turns on the LED; when I do the same in circuit (b) it doesn't work. What am I doing wrong?

Gregory M. Kiyoi via Internet

A. Well you've done a lot of things right. For example, you reversed both the LED diode and the polarity of the power supply. That's smart. Your

mistake is that you don't have a current path through the base of the transistor. Basically, a transistor is two back-to-back diodes with the base as common. For a transistor to work, you need to have current flowing from the base to the emitter. This current causes current to flow from the collector to the emitter; the amount of current flow is determined by the gain (hfe) of the transistor. If the transistor has an hfe of 100, 1 mA through the base-emitter will produce a flow of 100 mA through the collector-emitter. In circuit (b), there is no current path through the base-emitter. Since you're mixing NPN and PNP transistors in a more complex circuit, the correct way to handle the situation

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P.O. Box 14156 Fremont CA 94539 Fax 510-651-8454 Write in 29 on Reader Service Card. is to invert the 2N3906 transistor (c) so that you can run off a singlepolarity power source. In this configuration, current will flow from the emitter (+6V) through the base via the 1K resistor when the switch is closed. This causes the LED to glow. Good luck with your project!

Hard Disk Fixes

Q. My 2GB (nearly full) hard disk went from being fully operational to being "not detected" by the computer's BIOS. A spare hard disk works just fine in the computer. Because the BIOS doesn't recognize the drive, I'm thinking that the failure is with the drive's electronics and not a mechanical crash. Some questions: Is my assumption likely to be correct? Are there any fuses on a typical drive? Can the drive be repaired or the data retrieved? If so, can you provide a repair/restoration vendor's contact or name two?

Derek Neely via Internet

A. Been there many times, most recently a couple of weeks ago. Yes, you have a hard disk problem. There are many reasons why a hard disk fails. Let me list them in the order of failure rate.

1) The disk gets "stickism" where the bearing freezes or the read/write head "glues" itself to the platter, preventing the disk from rotating. If you don't hear the drive rev up when power is applied, it may be stuck. To fix it, hold the drive horizontally in your hand and give it a quick twist. This often frees the stick and gets the disk up and running, but not for long. Remove the data immediately. Some data may be lost, but probably nothing important.

2) Heat and vibration inside the PC cabinet has caused the solder

joints on the controller board, mounted directly under the drive itself, to loosen and lose electrical contact. This most frequently happens with the milk-white power connector. VERY carefully apply soldering iron heat to these four pads on the controller board. Also push down -don't remove - any socketed ICs on the controller board to reseat them.

3) The controller board has died. Unfortunately, there are no fuses to replace. However, this problem is fixable if you can find a used drive of the same make, model, and relatively-close serial number. Simply remove the board from the used drive and drop it into your drive. The controller board is coupled to the drive via a couple of flexible printed circuit cables. These are fragile, as are the connectors that attaches them, so be careful. I've repaired several drives this way.

4) The drive is dead and you've exhausted all the hardware options. If the drive contains valuable data it's probably worth having a professional retrieve them for you. Expect to pay about \$500.00. You'll find a list of data recovery services at

http://www.btinternet.com/-gfd/links.htm. Although I've never used a data recovery service, the following two companies sound like they know what they're doing: ECO Data Recovery (1-800-339-3412; http://www.eco-datarecov.com/index.html) and Data Recovery Labs (416-510-6990; http://www.datarec.com/index5.html).

Well-Depth Gauge Revisited

Q. In a previous column (Aug. '98), you published a schematic of a well-depth alarm using thermistors. I thought of using this circuit for a cistern, but how would you get the thermistors down the well and be watertight too? Phone wire?

> Stephanie Drake via Internet

A. Yes, I'd use phone wire – but not the kind you buy from Radio Shack. Instead, contact your local phone company and ask for a hank of direct burial cable. It has about six twisted pairs and is encased in silicon-filled rubber. However, the last time I asked for a "slice" of this cable (I needed about 36 feet) they gave me a full spool, so be careful what you ask for. You may get more than you want! If you can corner a repair tech, he/she will probably have some remnants on hand. My local phone company hands this stuff out for free, but others may charge. Alternatives? Of course. Coax, ribbon, and just about any wire that's designed to work in wind, rain, sleet, and snow you know, the kind you see on power poles and the outside of a building. What's more important is the thermistor splices, which could compromise the integrity of the sensor. I suggest covering the splices with RTV (silicon) then covering that with shrink warp after it's cured, as illustrated below. Whatever you do, don't insulate the thermistor. It's already waterproof and trying to further protect it will only hinder its performance. Just make sure the leads are covered.

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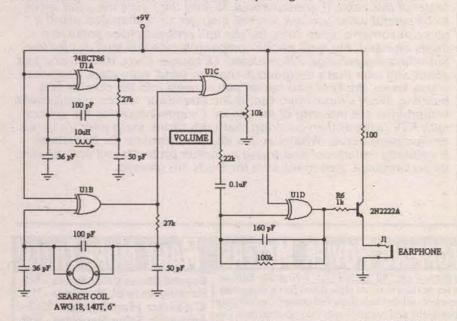
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Let The Treasure Hunt Begin

Q. I'm trying to find plans for a transmit/receive type metal locator. I understand the concept and the principles of the system, but that's a long way from actually building one. I was referred to a book by Charles Rakes on building metal locators but haven't been to find it.

Karl Klein via Internet

A. Like all technologies, today's metal detector doesn't look anything like the ones Mr. Rakes describes in his 1986 book (which is long out of print). Back in those days, the BFO (beat frequency oscillator) detector was all the rage. Today, it's pulse induction and VLF (very low frequency), with magnetometers playing a small part. Here's how they compare. Pulse induction is the least sensitive and the least expensive. It can't discriminate between gold or tin – but it's great at finding beer cans and watches. Magnetometers, often called flux gates or gradiometers, are mainly sensitive to iron objects. The unique thing about VLF metal detectors is that they can tell the difference between a gold coin and a bottle cap - well, most of the time. Unfortunately, it's not an easy trick because it requires a microprocessor. Radio Shack sells an entry-level VLF metal detector (63-3005) for just \$49.99, but the serious units run about \$400.00. While I don't have the space to show you how to build a VLF metal detector, you can have fun with this medium low-frequency BFO metal detector.



This metal detector uses four exclusive-OR gates, two of which (U1A and U1B) are wired as twin oscillators. The search coil is the inductance element of one oscillator (U1B). One oscillator is tuned to 161 KHz and the other is tuned to 160 KHz. U1C serves as a mixer, which outputs difference and sum frequencies of 1 KHz and 321 KHz, the latter of which is filtered out by the 10 kHz filter at U1D. When the loop coil is brought near metal, the metal changes the inductance of the

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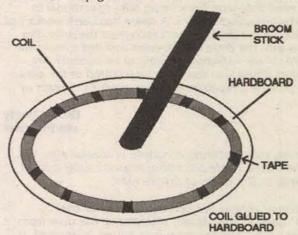
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inductor which changes the oscillator's frequency and the pitch of the audio. While not as sensitive as a VLF, the sensitivity is enough to detect a coin buried under a foot of sand. The coil is 140 turns of scramble-wound 18-gauge enamelled wire on a six-inch, round form that you make by pounding eight 6-penny nails into a board (a kitchen pot works, too). The coil is then taped and glued to a piece of hardboard or plywood. An old broom stick serves as a handle.



To use the detector, tune the variable inductor until you hear a tone in the headphones - then have fun!

Gradiometer Sees Through Rock

Q. As a treasure hunter for many years, I've used a wide variety of metal detectors, including a long boom proton differential magnetometer, dualloop deep range metal detectors by White, and the more common coin detectors by Fisher and others. Now that I'm fully retired, I need to hold down the cost of owning such gadgetry, plus I'd enjoy building or modifying my own. The objects I search for are made of old iron, weighing between 20 and 200 pounds, and are buried at depths ranging between 5 to 20 feet in mud or rock-filled pits. Given these parameters, relatively minor anomalies in the earth's magnetic field is probably the only way to find them. Do you know anything about the sensitivity of the FGM-3 flux gate sensors or have any other circuit recommendations for sensitive differential detectors that balance out the earth's field?

WO Enderle W7IZR via Internet

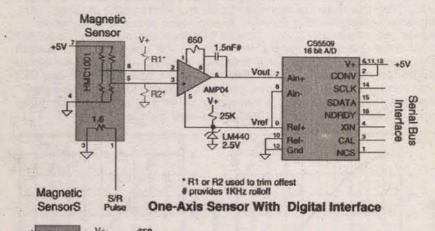
A. Honeywell (612-954-2093; http://www.ssec.honeywell.com/pro ducts/magsensor_index.html#a) claims to have the most sensitive magnetic field detectors for low-cost commercial applications, and are well-suited for your need. Honeywell's magnetic sensing elements are Anisotropic magnetoresistors (AMR) made of nickel-ferrite (NiFe) thin films deposited on silicon to form a balanced Wheatstone bridge, where the resistance of the four resistors is the same. This material has the unique property of changing resistance when a magnetic field is applied perpendicular to the current flow in the AMR material. In the Wheatstone configuration, the magnetic field causes one pair of resistors to decrease in value and the opposing pair to increase in resistance. The result is a differential output voltage with a sensitivity of just 27 microgauss (uG). The output is linear over a range of -2G to +2G. (By comparison, the earth's magnetic field is 300 milligauss (mG)). Because of the fine resolution and wide range, these sensors are used in compasses, traffic detection, navigation systems - and gradiometers. Here are two simple designs using the HMC1001 one-

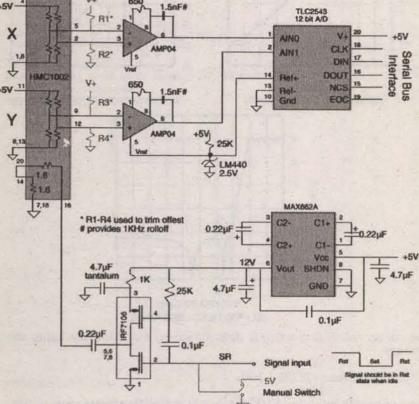
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\$275.00	TEK CG5001 PROG.O-SCOPE CAL.GEN	\$2000.00
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\$900.00	TEK 485 350MHZ OSCILLOSCOPE	\$650.00
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\$1200.00	TEK 11402 IGHZ DIG PROG. O-SCOPE FRAME	\$1000.00
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Electronics Q & A

axis detector and HMC1002 two-axis detector.



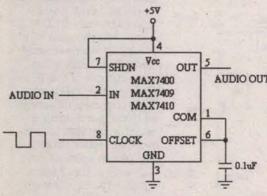


Two-Axis Sensor With Set/Reset Circuit and Digital Interface

You can buy the HMC1001 and HMC1002 from Newark Electronics (1-800-639-2759; http://www.newark.com) for \$18.00 and \$31.00, respectively. For a complete schematic of a gradiometer, download document AN204 from the Honeywell Web site.

Tunable Low-Pass Filters

Q. I've made a home-grown infrared gas analyzer using two DACs (digitalto-analog converter) on an instrumentation card. The DAC signals are carried through a 20-foot cable with other signals and DC power to a terminal strip for connection. What I need is a filter to smooth out the stairsteps of the outputs. The required response is DC to 10 Hz, and the sampling rate is 50 Hz. Currently, I'm using a simple two-pole Sallen-Key Bessel filter with unity gain - and less than stunning performance. Would you suggest cascading two of these filters and if so how should I distribute the cut-off frequencies?



Steve Roberts via Internet

A. This is a very timely AUDIO OUT question because Maxim Integrated Products (408-737-7600; http://www. maxim-ic.com) just announced a family of switched-capacitor filter ICs specifically designed for ADC anti-aliasing and DAC postfiltering. The MAX7409 is a fifth-order,

low-pass, Bessel, switched-capacitor filter; the MAX7410 is a fifthorder, low-pass, Butterworth, switched-capacitor filter; and the MAX7400 is an eighth-order, low-pass, Elliptic, switched-capacitor filSource Code:810NV

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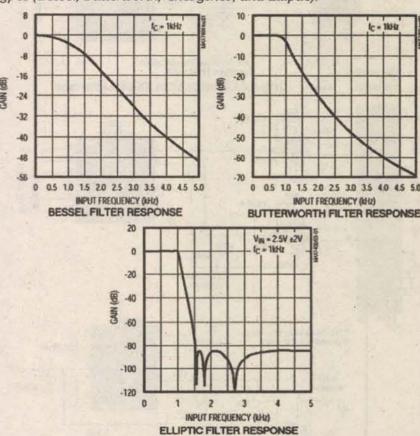
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Electronics Q & A

Low-pass Bessel filters delay all frequency components equally, preserving the shape of step inputs. Bessel filters settle quickly — an important characteristic for ADC applications that use multiplexed inputs. An anti-aliasing filter placed between the multiplexer and ADC must settle quickly as the inputs are switched. Low-pass Butterworth filters provide a flat passband response, making them ideal for instrumentation applications that require minimum deviation from the DC gain throughout the passband. Low-pass Elliptic filters provide the steepest possible rolloff with frequency of the four most popular filter types (Bessel, Butterworth, Chebyshev, and Elliptic).



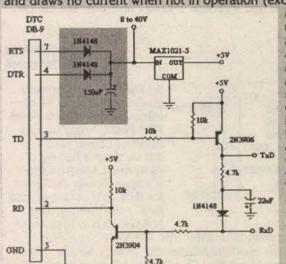
The corner rolloff frequency is determined by the clock rate using the formula

clock rate = fCLK / 100

For a corner frequency of 100 Hz, apply a 10-KHz squarewave to pin 8. When using the filter for anti-aliasing or DAC postfiltering, you have to synchronize the DAC and filter clocks. If the clocks aren't synchro-

Reader's Tip

Several simple RS-232 interfaces built around bipolar transistors have appeared in *NEV* articles, but most have shortcomings. The following circuit is small, simple, inexpensive, compatible with the RS-232 standard, and works in full-duplex operation, something most simplified interfaces can't do. The circuit is based on the one used for the BASIC Stamp II microprocessor. The modification is the addition of diode D1 and capacitor C1 to the Parallax circuit. When RxD is active, C1 charges to -12 volts and holds it during positive transitions, which effectively isolates the TxD and RxD lines and allows full-duplex operation. Q1 is the receive inverter, and Q2 the transmit inverter. TxD and RxD go to the host TD and RD go to the local CPU. The circuit "steals" its power from the host serial port, and draws no current when not in operation (except for transistor leak-



age currents), making it useful for low-power applications. It costs approximately \$1.00, about 1/3 the cost of a MAX232 interface, and saves the 5 mA quiescent current of the IC. Further, the TxD and RxD channels of several of these ports can be wired in parallel for networking applications. We use this circuit consistently at baud rates up to 115,200 through 12-foot cables.

Dan Michaels Oricom Technologies oricom@sni.net

Electronics Q & A

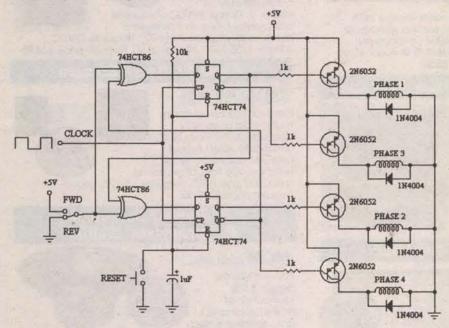
nized, beat frequencies will alias into the passband. I can't find the ICs at any of the local watering holes yet, but you can order the part directly from Maxim at 408-737-7600, extension 3468. However, I'm sure their regular distributors, like Digi-Key (1-800-344-4539; http://www.digikey.com), will have them in stock anytime soon. They cost about \$3.00.

Space-age Stepper Motor Controller Update

Q. In the Feb. '98 issue, you published a schematic of a "Space-Age Stepper Motor Controller." In a later issue, you published a correction reversing the TIP120 transistors. I have tried this circuit and cannot get it to work. Can you explain the logic for this circuit? I'm having trouble understanding how bipolar current flow can be achieved with fewer than eight transistors.

J. D. Mather Johnson City, TN

A. Actually, there were two mistakes in that schematic, which I copied from a supposed "NASA" source in my sleep and didn't check for errors. Here's the same circuit from EDN's "Ideas For Design" submitted by a JPL engineer that I know works — I tried it!



How does it work? Sit tight and buckle up because this will be fast. Different magnetic polarity sequences are needed to drive a stepper motor. For forward motion, Phase 1 leads Phase 2 by 90 degrees; for reverse motion, Phase 2 leads Phase 1 by 90 degrees — just the opposite. Using XOR gates and flip-flops, it's easy enough to make this happen because flipping the switch flips the phase shift from lead to lag — just what's needed. As always, the speed of the motor is proportional to the clock pulse; the higher the clock speed, the faster the motor spins.

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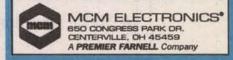
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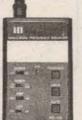
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The Ims and Outs of **Optimizing Compilers**

f you're not writing computer programs in hand-coded assembly, chances are you're using a compiler. If you're using a compiler, chances are the compiler is performing optimizations on your code, possibly unbe-knownst to you. Compilers are where text touches silicon; your abstract source code becomes a concrete program that runs on an actual machine. Being aware of compiler optimization techniques can save you a measured amount of frustration, especially when debugging your

Fundamental Compiler Technology

Compilers are usually broken up into two parts: a front end and back end. The front end takes care of scanning and parsing the source code, and the back end takes care of generating and optimizing code. Figure 1 illustrates the basic components of a compiler.

As the source code enters the compiler, the front end reads the characters in the input stream and separates them into tokens, as shown in Figure 2. This is the part of the compilation process that's called lexical analysis. Tokens are symbols that cannot be reduced any further. Tokens are not restricted to single characters. For example, if you have a variable named MyVar in your source program, MyVar cannot be reduced any further, therefore, MyVar is a token. In some compiler literature, tokens are occasionally called atoms.

As the tokens are scanned, their type is determined and the token and its type are placed in a data construct called a symbol table. The symbol table is a convenient storage device that allows other components to access expressions, variables, and types. Symbol tables are usually implemented as linked lists.

The next component in the compiler's front end is the parser. The parser does essentially two things. First, it determines whether the input represents a legal construct of the language. Second, it puts the input expression into an intermediate form that makes it easier for the code generator to process. The parser tries to

mach the sequence of tokens to a set of rules called productions. The set of productions that make up the rules for a language is called a

Code

If you look in Appendix A, Section A13 of Kerninghan and Richie's book The C Programming Language, the grammar for C is listed. Productions or grammar rules are usually expressed in Backus-Normal Form, or BNF. BNF

Want to write better code? Consider understanding compiler optimizations.

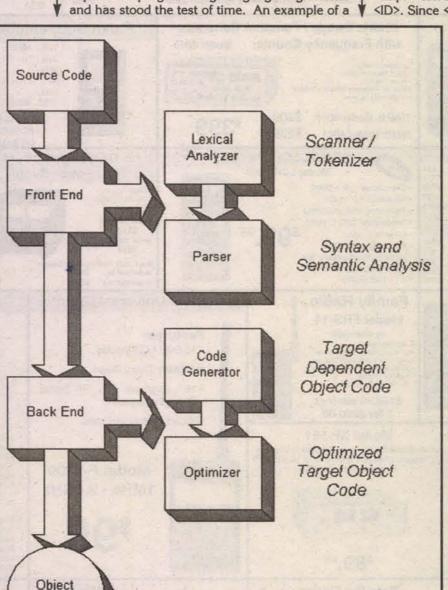
was invented and used to express the grammar A for the first implementation of FORTRAN. BNF is an adaptation of the way linguists express natural language. John Backus is credited for creating FORTRAN and for first developing BNF, so BNF is named after him. BNF is a convenient way to express a programming language's grammar

code can be generated for this expression, and the resulting computation can be stored in the variable i.

Here's the derivation:

First, we can consider j + k * z to be an expression <Expr>. From the grammar rules, <Expr> can be rewritten as <Expr> ::= <Expr> ' <ID>. Since <ID> can be rewritten as a letter or a

digit, this derivation resolves to <Expr> * z. Next we need to figureure i + k into the derivation. We do this by rewriting <Expr>* z with <Expr> + <ID> * z. We can substitute the token k for <ID>, resulting in $\langle Expr \rangle + k * z$. Lastly, we can rewrite $\langle Expr \rangle$ as $\langle ID \rangle$, yielding <ID> + k * z. We can substitute the token j for <ID>, resulting in j + k * z. Since we were able to match the expression to the grammar rules, the input expression is indeed legal and can be correctly compiled. Figure 4 shows the complete derivation sequence.



Code Generation

After parsing is complete, the grammar rules are matched, and the symbol tables filled, code generation can begin. Code generation may take the form of assembly language, or the compiler may skip assembly code generation and directly produce code for the target machine. This is called native code generation. Most C compilers for embedded systems produce assembly code, which is then optimized before any object code is produced.

Low-Tech Optimization

There's a lot you can do before your source code is ever compiled. Careful programming can make the compiler's job easier. By using a few hand-optimization techniques, your code will run tighter and faster when it's compiled. Hand optimization is a lowtech approach, but it pays off. For

example, look at the following C code fragment:

Simply removing the assignment x = 10 rad-

grammar for simple arithmetic expressions is shown in Figure 3.

FIGURE 1

Suppose the parser encounters the input expression i = j + k * z. In order to determine if this is indeed a legal expression, the parser needs to match it to the grammar rules given in Figure 3. Is i = j + k * z a legal expression? First, the parser must determine whether j + k * z can be derived from the grammar rules. If it can, then ically increases the efficiency of this code fragment. This type of source level optimization is fairly obvious, and even beginning programmers recognize this. More subtle methods include using pointers instead of using array indices as the following example illustrates:

/*
* Non-pointer method of access buffer elements using an index variable

printf("\nBuffer access using index variable\n"); for(I = 0; i < 10; i++)printf("%c",Buffer[i]);

Performance of this code is increased by using a

* Set pointer to start of Buffer and print values printf("\nBuffer access using pointer\n"); ptr = Buffer; while(*ptr)
printf("%c",*ptr++); printf("\n");

These are simple optimizations that a careful programmer can accomplish on his or her own.

Profiling

Another useful procedure is to profile a program without any compiler optimizations turned on. Profilers are important, but sometimes little used tools. Profilers or performance analyzers - find run-time bottlenecks in your program while it executes. You compile and link your program, then execute it under the profiler's control. When the program terminates, the profiler generates program performance statistics.

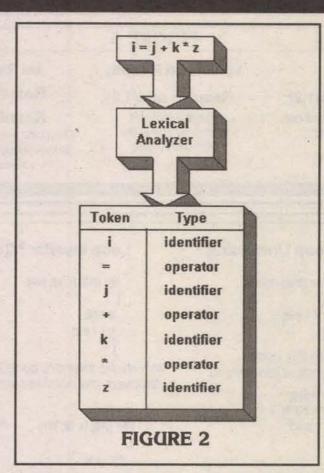
You can discover where your program spends most of its time, how many times certain routines were called, how much CPU time was consumed, and how many interrupts occurred, among other things. Profilers are extremely powerful tools that are sometimes bundled for free with some compilers.

Common Optimization Techniques

A compiler doesn't necessarily produce object code or an executable program exactly the way your program intended it to. All a compiler is expected to do is to reproduce the way the program was intended to behave.

From a compiler's perspective, as long as the program produced works the same way as your program text intended, what happens algorithmically within the program doesn't matter. This is surprising, but true. Knowing that the optimized program a compiler produces may not be exactly what you programmed is a good thing to bear in mind when you're debugging your code.

Some of the compiler optimization methods have strange sounding names that, on the surface, don't seem to make a lot of sense, such as loop induction, peephole optimization, or constant folding. It's worth the time to understand optimization terminology so you can make informed decisions about what optimizations to allow when compiling your code.



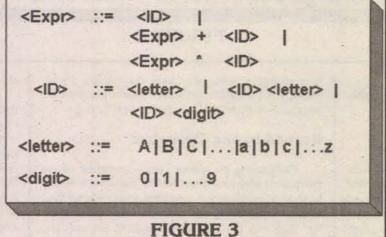


FIGURE 4

Rule Matching for j+k*z <Expr> ::= <Expr> * <ID> <Expr> ::= <Expr> * z <Expr> ::= <Expr> + <ID> * z <Expr> ::= <Expr> + k * z <Expr> ::= <ID> + k * z <Expr> ::= <ID> + k * z <Expr> ::= j + k * z

Register Allocation

Register allocation is probably the simplest and most ubiquitous of all optimizations. When a variable is accessed, the compiler first looks if it can use a CPU register to store the variable instead of storing it in external memory. This is a speed-oriented optimization, since no memory address bus cycles are used. Register allocation must be done in the back end of the compiler during code generation, since the front end of the compiler does not know how many registers the target machine contains.

Dead Code Elimination

If a value is computed but never used, it's dead code. An optimizing compiler will recognize this and eliminate it in the code generation phase. This can be distracting if code stubs are placed in a program to be filled in later. For example, if you have the following lines in your program:

int Result; Result = add(1,2);

and your program never used the variable Result again, the code may be completely optimized out of your program. If this was a program stub that you were going to build upon later, you'd be in trouble. A way to place stubs into the code without having them optimized out and without turning off compiler optimizations is to add the following assignment immediately after the call to add(1,2):

Result = Result;

This uses the variable Result without really doing anything. This simple trick costs nothing and allows the stub to avoid the optimizer's axe. You could also declare Result as volatile. Declaring a variable as volatile forces the compiler to use the variable under all circumstances, since the keyword volatile suppresses any compiler optimizations. Be careful using the keyword volatile, since all of the variables of this type will never be optimized. See Figure 5 for a simple side-by-side comparison of this code.

Loops

Loops are obvious candidates for optimization. Most programs spend most of their CPU cycles within loops. Here are some common loop optimizations.

Loop Unwinding

Loop unwinding is a classic example of the code-size, code-speed tradeoff. When loop unwinding occurs, the loop is decomposed into linear code. The linear code is copied the number of times the code iterates. This produces more code, but it runs faster. An example of loop unwinding is shown in Figure 6.

Loop-Invariant Code

If code exists in a loop that doesn't change, then there is no reason for the code to be executed over and over again within the loop. It wastes CPU and bus cycles, which wastes time. Optimizing compilers that are sensitive to loopinvariance recognize this type of code and extract it from the loop. The loop-invariant code is placed above the loop, yielding more efficient code. We saw this example before, in the LowTech Optimization section. An example of loop-invariant code elimination is show in Figure

Loop induction

Pointers are more efficient than indexes, and addition is more efficient than multiplication. With loop induction opti-

mization, the compiler attempts to replace array index multiplications with pointer additions, again yielding more efficient code. We saw a simple form of this in the Low-Tech Optimization section where we substituted pointers for array indexes in the for loop code example.

Constant Folding

This is a somewhat strange name for performing calculations at compile-time instead of run-time. When a compiler encounters expressions that can be evaluated at compile time, the compiler does the actual calculation and then stores the result. For example, a code fragment such as:

#define MAX_TEMPERATURE 100 y = 25: x + y + 2 * MAX_TEMPERATURE;

is optimized to x + 225 by the compiler by utilizing constant folding.

Peephole Optimization

The last technique we'll examine is peephole optimization. This is also sometimes called linear optimization. Peephole optimization is common throughout almost all compilers, since it is one of the easier techniques to implement. A peephole optimizer scans through the code examining only a small fragment at a time, like it's examining the code through a little peephole (hence the name).

The peephole optimizer then tries to improve the current fragment, possibly reducing redundant instructions or placing memory references

FIGURE 5

int Result:

Result = add(1,2);

This code is optimized out by the compiler

volatile int Result:

Result = add(1,2);

Result is NEVER optimized due to the keyword volatile

int Result;

Result = add(1,2):

Result = Result:

This code is not optimized out due to the simple benign assignment Result = Result;

integer function that added two numbers together:

int add(int x, int y);

The actual call to the function in the body of the code was:

Result = add(1,2);

It was hard to think of a simpler function to start experimenting with. We compiled, linked, downloaded, and ran the code through the debugger on the target system. The debugger stepped right over the function call as if it didn't exist in the code! We checked the code, recompiled, downloaded, and ran again with the same result.

Everything appeared to be completely legal. We tried it on a PC with another compiler, and the line containing the function call was executed. We returned to the target environment, recompiled, and ran again. The debugger still stubbornly refused to execute the function

To add to our confusion, we could set a breakpoint within the function body, but could not set a breakpoint at the function invocation. Meanwhile, several hours had

elapsed.

We decided to call the development environment vendor, thinking that we had encountered a bug in the compiler or debugger. After talking to a couple of support engineers, we finally happened upon one who had previously encountered a similar problem. His response was "Welcome to the world of optimizing compilers!" It turned out that our result value was never used in the program, so via dead code elimination, the compiler decided to optimize out the code.

The moral of this story is, however valuable compiler optimizations may be, TURN THEM OFF when you are initially developing code for a new system using new tools. Incrementally turn on optimizations as your code development progresses. If you don't, you may get burned when you're debugging. **NV**

Loop Unwinding Loop Invariant Code for (i=0;i<3;i++) for (i=0; i< 10; i++) K = K44; x =10; y= i+x; When this code When the invariant code is unwinds, it resolves to: removed, the code resolves to: x = x+0; x=x+1; x = 10: x = x + 2; for (i=0; i< 10; i++)

FIGURE 6

y=i+x;

into registers. After it's done optimizing a segment, the peephole optimizer examines another segment of code and continues optimizing.

Burned by the Optimizer

Optimizing compilers can sometimes cause confusion and cost time, which translates directly to money. Here's a personal experience I had with an optimizing compiler for a 32 bit processor that was used in an embedded system. We compiled and loaded a small test program that was supplied with the operating system code.

Since this was our first experience with this particular processor and operating system, we figured it was a good place to start. The program ran correctly on the target system, so we decided to add a new function. We declared a simple

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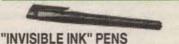
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Questions & Answers

TECH FORUM

This is a READER TO READER Column. All questions AND answers will be provided by Nuts & Volts readers and are intended to promote the exchange of ideas and provide assistance for solving problems of a technical nature. All questions submitted are subject to editing and will be published on a space available basis if deemed suitable to the publisher. All answers are submitted by readers and NO GUARANTEES WHATSOEVER are made by the publisher. The implementation of any answer printed in this column may require varying degrees of technical experience and should only be attempted by qualified individuals. Always use common sense and good judgement!

QUESTIONS

How can I interface and set the switches of a HP PaintJet printer to work with a IBM-compatible PC? I do not have a manual. The printer appears to be a RS232 serial port. The printer does a self-test okay. There are two DIP switches to be set. 11981 Cliff

Canyonville, OR

I recently bought a used comput-

The sound does not work and before it boots up, it gives me the following message: "!!Warning!! The Primary Wave Device does not appear at I/O address 534. The sound card will not be fully functional without this device. Check the hardware settings, and then check the hardware configuration panel associated with this program. The "Waveport" parameter must match port address selected by the hardware jumpers. Press any button to continue.

After this, my Windows95 runs just fine although with no sound

11982

John Rehm via Internet

How do underground wire locators work? Do you have a simple circuit for building such a device?

11983

Richard Haendel via Internet

I have prepared a cassette tape for teaching purposes. Is there any way to prevent the duplication of this tape by others?

I need an electronic piece to go with the tape to prevent direct and easy duplication.

11984

via Internet

I have several new surplus 3UP1 CRTs that have been in my junk box for over 20 years. I cannot bring myself to toss them out, especially since I just completed a homebrew spectrum analyzer and one of them would be a great fit for it. They are a natural to dress up any new PIC pro-

My difficulty is not the 2 KV of HV required for the anode or focus electrodes since the new laser kit power supplies will adapt neatly there. I need help on part selection/design for the deflection circuits. I want to Send all material to Nuts & Volts Magazine, 430 Princeland Court, Corona, CA 91719, OR fax to [909] 371-3052, OR E-Mail to forum@nutsvolts.com

be able to drive the CRT with a O to 5V output from a DAC.

The only specs for the 3UP1 show that I will need about -300 to +300V drive into a 20 pF load. By driving it with DAC output from a PIC, I could even generate simple text if it had about 3 MHz of bandwidth. For the spectrum analyzer, I only need 50 KHz or so, of bandwidth.

Is there a simple way to create a deflection circuit for this project [perhaps with an op-amp and MOSFET]? Ron L. Sparks

Katy, TX

I have a RadioShack multimeter, a Micronta 22-168, which includes the capacity to communicate via the serial port. It works fine with the supplied software, but I have been unable to access it with the suggested (GW Basic) basic code. Here's the QB version of the code to read the data in the multimeter once:

OPEN "COM1: 1200,N,7,2,RS,CS,DS,CD" FOR RAN-DOM AS #2

A\$ = "D" PRINT #2, A\$ INS = INPUTS[14, #2] PRINT INS CLOSE #2

The program does not get past the IN\$ line. IN\$ is always empty if I print it from outside the program. Does anyone have Quick Basic code which will access this meter?

11986

Grant Fair Ontario, Canada

I am able to buy a surplus generator that puts out 400 Hz. Can you help me with a way to convert it to 60 Hz? Articles or projects?

11987

Gary Stiffler via Internet

I have a Tystar VGA monitor I am running on my older 486 PC. When I run America Online, It tells me I don't have 256 colors selected as AOL requires to run properly. I tried to change the VGA drivers in Windows Setup, but all it did was cause the monitor to be completely out of sync. I have two questions:

1. How does one know how many colors a given monitor will support, assuming you have no documentation?

2. Which VGA driver should I use for this application?

11988

Lonnie W. Sutton Dugway, UT

I tried to modify the SA8500-321, cut a jumper W310, and install a .01 uF disk cap, and the resistor connect to pin 21 in IC305.

The problem is, it only works for a short time and turns the screen black. If the channel is changed, it will work again, but for a short time. Maybe I am doing something wrong. 11989 Alfredo Gonzalez

Presidio, TX

I replaced a HP C1599A SCSI DAT tape drive after it failed. But after checking out the failed drive, all the motors run and the tape tries to stat against the VCR type heads. The tape lowers itself twice then the vellow LED comes on blinking silently and failing. Can someone point me to a repair path?

119810

George Clute Mercer Island, WA

I'm looking for a simple circuit to detect randomly inverting video. Ideally, the circuit would light an LED when this happens.

119811

Anonymous

ANSWERS

ANSWER TO #89810 - AUG. 1998

Make sure you are disabling the touchpad in the laptop's BIOS, not just removing it from Windows. Also, your touchpad probably uses DOS drivers, because you are using Win 3.1. Make sure any mousy looking lines in AUTOEXEC.BAT and CON-FIG.SYS are "rem"ed out (type REM in front of the offending line, (i.e., REM C:\ DOS\ TOUCHPAD.COM) instead of C:\DOS\TOUCHPAD.COM). This temporarily disables the drivers.

You will then have to add lines pertaining to your mouse drivers [MOUSE.COM] if the automatic setup do it (i.e., doesn't C:\ MOUSE\ MOUSE.COM, copied your drivers to C:\ MOUSE\].

Then reboot and see if your mouse works. If it doesn't, poke around for any other touchpad dri-

ANSWER INFO

 Include the question number that appears directly below the question you are responding to.
• Payment of \$25.00 will be sent if

your answer is printed.
• In most cases, only one answer per question will be printed.

Your name, city, state, and E-Mail address, (if submitted by E-Mail), will be printed in the magazine, unless you notify us otherwise with your submission.

• Due to space limitations, we can not reprint the original questions with the answer. The question number and the issue it appeared in are printed above the answer

 Unanswered questions from a past issue may still be responded to.

Comments regarding answers printed in this column may be printed in the Reader Feedback section if space allows.

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All questions should relate to one or more of the following:

1) Circuit Design 3) Problem Solving

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Questions may be subject to editing.

HELPFUL HINTS

· Be brief but include all pertinent information. If no one knows what you're asking, you won't get any response (and we probably won't print it either).

Write legibly (or type). If we can't read

it, we'll throw it away.

Include your Name, Address and Phone Number. Only your name will be published with the question, but we may need to contact you.

vers. Also, try running your mouse as COMS

To do this, you will have to add a command line switch to the MOUSE.COM line in AUTOEXEC.BAT. At the DOS prompt, switch to the directory containing your new mouse drivers and type MOUSE /? [ENTER].

This will tell you about the options available. One last thing to try is to disable all power saving related to the serial ports. You will have to do that through your laptop's BIOS, too.

Evan Weaver Hockessin, DE

ECH FORUM

ANSWER TO #109811 - OCT. 1998

The LM3914, LM3915, and LM3916 are designed to do just that. They require a minimum of parts to operate and most come with diagrams on how to hook them up as

ANSWER TO #7984 - JULY 1998

A "Roger Beep" or End of Transmission (EOT) beep circuit is fairly easy and inexpensive to build as the schematic diagram shows.

The circuit can be assembled on a small section of perfboard using pointto-point wiring and installed inside most any transceiver.

The circuit is designed around an LM1458 dual op-amp IC, but any similar IC such as the LM358, etc., will also work. The circuit operates as follows:

When push button switch S2 [microphone PTT switch] is pressed, the relay coil is energized which causes the transceiver to transmit. When the microphone PTT button is released, the transceiver remains in transmit for approximately .27 seconds during which time, the beep tone is transmitted.

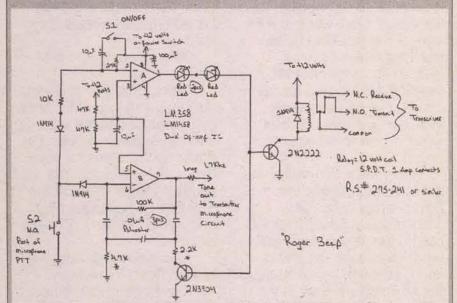
After the .27 second delay time has passed, the relay coil is de-energized which places the transceiver back into receive.

When switch S1 (normally a mini toggle, etc.) is open, the EOT beep tone is not transmitted. The frequency of the beep tone [currently 1700 Hz] can be changed somewhat by altering the component values of either one or both of the resistors marked with "'

Increasing their values will lower the frequency while decreasing their values will raise the frequency.

A different value resistor may need to be substituted in place of the one megohm output resistor at pin 7 of the IC in order to avoid over-modulating the transmitter. Increasing the resistance value will lower the modulation level.

Brian Pliler Baxter Springs, KS



either a VU meter or a power meter.

Two or more of these units can be cascaded together to drive 20 or more LEDs, LCDs, or vacuum fluorescent displays. A single pin changes the mode of operation from a "moving dot" to the "bar graph"

The LM3914 senses an analog voltage and divides into 10 segments which drive 10 separate outputs. These outputs are regulated and fully programmable which means that you can program it for low-power usage, as well as high-power amps.

The LM3915 is a logarithmic version of the LM3914 with a 3 dB interval between segments.

The LM3916 has all of the same features as the LM3914 and LM3915, but is designed specifically for use as a "VU" meter.

Several cross reference numbers are:

National Semiconductor part # LM3914

ECG part #1508 NTE part #1508

National Semiconductor part # LM3915

> ECG part #1509 NTE part #1509

National Semiconductor part # LM3916

NTE part #1549

Chris Bieber, CA

ANSWER TO #109815 - OCT. 1998

Do not use port I/O to control your soundcard - use the waveln dri-

Windows puts a lot of overhead on I/O port instructions, and soundcards require double-buffered DMA transfers and other sophisticated programming methods. device

Application software should talk to the hardware through the system device drivers.

There are many benefits. Not only do you avoid fiddling with lowlevel programming, but your program will also work with soundcards that are not SoundBlaster compati-

The proper driver is the waveln multimedia device. I know how to access it in C, but not VB. You should be able to find the details about PCMWAVEFORMAT and the equivalents of wavelnOpen, waveInPrepareHeader, MM_WIM_DATA, and friends.

There are also calls to control the mixer settings, but I recommend working on the decoding algorithm before tackling the soundcard and mixer programming.

The quick fix is to use the Sound Recorder [Start | Accessories | Multimedia Sound Recorder) to record a .WAV file with your weather satellite image, and writing a VB program to process the .WAV file.

Using the soundcard directly implies processing the image on the fly, and it may take a while before your program can do it on the fly. Using a .WAV file will give you consistent data and let you focus on the algorithms without worrying about processing speed.

Record the image in mono at 8 KHz with 8 or 16 bit samples. The .WAV file has some header information and then the data. The eight-bit samples are offset 128 numbers and the 16-bit samples are two's complement.

Several people have used soundcards to process weather satellite information. The August '97 QST has an article about a freeware satellite decoder, but I don't know if it does

Continued on page 74

0

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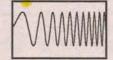
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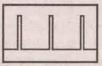
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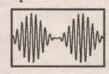
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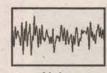
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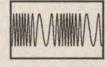
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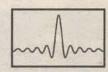
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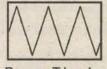
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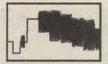
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Scott Edwards Electronics

Graphics LCD Module with Serial Interface



The new G12864 makes it easy to display text and graphics on a 128-by-64-pixel LCD. It interfaces with a computer through a 2400 or 9600-baud RS-232 serial hookup.

Text Features

The G12864 works like a serial-receive terminal. It displays text in a 4-line by 16-character format. Text is displayed in a large 8- by 16-pixel font, which can be edited to include custom symbols.

Graphics Features

The display lets you plot points, draw lines, and display full-screen graphics using easy instructions. Its flash memory stores the text font plus 14 screens. You can create fonts and graphics on your PC, then download them to the G12864 using the included software.

Convenience Features

A power supply and DB9 serial-port connector are built in. Connect the display to the (included) AC adapter; plug the (included) serial cable into your PC or other computer, and you're ready to go. Current draw ranges from 15mA (typical, backlight off) to 100mA (max, backlight on). For complete specifications, see our web site: www.seetron.com.

Display, with starter pack: \$199

Display alone (OEM qty 1): \$179

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Resistance is Futille!

by E. Z. Camp

ooking for a new career? I've got a great one, if you don't mind when or IF you eat or sleep! The money's good, you get to travel, and you meet lots of interesting people. In your spare time, you're parked in front of a computer screen, when you're not on the phone doing your investigations.

Me, I'm a technical writer. Free-lance to be specific. Yep, it's a 24/7 work week, but I love it! You wouldn't believe the things I've seen and places I've visited, not to mention getting paid for my efforts. I've met extremely intelligent people, beautiful women, and some real nut cases!

Every once in a while, you get to verbally abuse the Editor, when "editorial license" is stretched. This job can be fun, if you don't get fired! Like I said, the pay is good, although never on time, but that's how it goes in the publishing business.

Fringe benefits? You bet! Some of the technical stuff you pick up is like money in the bank. The sharp tech writer can develop some ideas legally from this material, and really cash in.

You've got to be super careful here, as you don't want to get black-listed for piracy. Your job could disappear overnight!

This job can get dull and boring, but within a couple of days you're on something new – just like the weather, it's always changing. Sometimes, it even gets risky, or should I say, downright dangerous? Take for instance, the Metalloid Affair ...

The phone was buzzing at me again, damn! Getting really tough to concentrate on editing.
"Hello?"

"Skip? It's Fred. You busy?

"Always, Fred! What's up

with you?'

"I'm working on a new project farmed out to me from DIGI-LOG and I ran out of acrylic spray - got any?'

"Yeah, I think I've got about half a can left. DIGI-LOG, huh? That's the outfit I'm editing data sheets for right now."

'Oh, anything interest-

'Sure looks like it! Seems our dead-and-gone Ms. Anna Log developed some very interesting linear circuits. I'm doing up the specs for what they call the 741 op-amp, and another gadget they call the 555 timer. They expect big sales! And I think they might be right."

You've been getting a lot of work from them lately."

"No kidding! Ever since that article I did for them before they pulled out of digital manufacturing and changed their name. How'd you hook up with them?"

'They saw a letter I sent into a hobbyist electronic magazine a while back. I was looking for information on temperature coefficients of certain metal and non-metal

alloys."

"I guess they saw something they liked?"

"Sure did. They contacted as the mag hit the me as soon as the mag hit the newsstands! Wanted some independent research conducted on attempting to come up with a zero-tempco metal alloy. They offered me a juicy contract, and I took it!" "Good for you! Well, I'm

ready for a little break. How about if I bring you over the acrylic spray and we rap for a

"Great! Bring those specs you're working on - I want to see them."

"Right! See you in 15!"

Fred's a scrawny little guy with those rough, good looks that women can't seem to resist. He's got himself a centerfold wife, and both of them have those upper-stratosphere type IQs. His 'workshop' is something to behold, money being no object. "Hi, Fred! Where's the

wife?"

"Out nailing down another software contract. I'm free for the afternoon. How's yours?"

"Great! She's really getting heavy into this anti-fraud stuff now that New Jersey has the highest auto insurance rates on the planet. There seems to be an abundance of "dirty" doctors and patients in the

"Tell me about it! Hand me that acrylic spray, huh?'

He began to gingerly spray a coat of the crystal clear plastic onto a beautifully labeled aluminum panel. "Has she had any luck yet nailing any dirty lawyers?"

Walking over to open a window for ventilation, I replied, "No luck yet. They're pretty well protected. Looks like lots of cash changing hands up top. Boy, that spray

stinks!"

Yeah, but not as bad as

those lawyers!"

"Agreed, but not all of them are dirty. We still need them, like it or not. What's

that panel for?"

Oh, I had a little accident with the chart recorder DIGI-LOG loaned me for this job. I kind of destroyed their front panel, so I made a new one," offered Fred.

Fred is always having 'little accidents.' For such a sharp guy, it always amazes me how he does it! "How many coats are you putting on there? I'm getting a buzz!

Fred grumbled, "Relax Skip, I'm done. Want to see the test rig?"

"Sure, is this it?" I replied, pointing to his bench.

On the bench was a neatly made fixture holding a shiny, metallic rod about the size of a lead pencil. Several sets of wires led off to the chart recorder.

A pair of triple-ought cables almost a 1/2" in diameter were connected to the jig and hung off the bench. These went down to the floor and tied in to three seriesconnected graphite rods about the size of flashlights. The cables disappeared through a wall grommet.

Fred saw my puzzled look, "Those are my homemade variable resistors - see the sliders on the rods? I needed some kind of current limiting on this set-up. I'm using my door stop for the power sup-

Said 'door stop' is a huge, 75-pound transformer rated at five volts at 1 KVA. That's a 200-amp supply, folks! I asked sarcastically, "Think you've got enough current, Fred?'

A straight-faced Fred: 'Just about enough, maybe! I've been running conductivity tests on different alloys supplied to my specs from another outfit. Their standard sample size is 1/4" by 5", so I needed something hefty to get a measurement.

I asked, "So you said DIGI-LOG wants you to investigate alloys for zero-tempco;

what's the point?"

Fred laughed. "The zerotempco they're interested in is not dimensionally related, but electrically related. They apparently have a use for conductors that exhibit no conductivity change over wide temperature variations. This was not my original intent, but if they wanted to pay me, why not bag two birds with one stone?

So what are you looking

Fred explained, "My original theory was that it should be possible to form an alloy from two or more metals or non-metals that would have

very high and constant conductivity at any temperature. By combining a metal, whose conductivity decreases as temperature increases, I hoped to get something that worked."

Bloody hell, you say! Did

you do it?

He looked upset. "Yeah, I fulfilled their contract. Would you believe I found two workable alloys?

I was intrigued to say the least, "How'd you do it?

Fred pondered. "Did you know that aluminum is NOT a metal? Not many people do. It's a metalloid; its conductivity varies directly with temperature, as opposed to real metals. This was the key to my experiments, as aluminum already has a high conductivity, like gold and silver and copper. The trick was to alloy one or more real metals with aluminum in the right proportions. Two of the dozen alloys I dreamed up show the zerotempco effect, and I've still got three more to test."

"So, why the long face?" "I'm still not seeing what I

expected to see!"

'Let's see how your rig

works, okay Fred?

He brightened up. "Sure! This thing's really pretty simple, just set up for high power. I apply power to the sample rod from the door stop through the variable resistors using those monster cables, starting out at about 10 amps and ending up at 50-100 amps. At those currents, the sample 'self-heats' which saves me using a separate heater."

"And you print out the run on the chart recorder."

"Right! The three upper recorder pens trace out the sample temperature, current through the sample, and the voltage drop across it. The fourth pen gives the calculated resistance of the sample. What you want to see is a flat line on that trace."

I was impressed. "Nice chart recorder they loaned you."

"Yeah, I was lucky I was able to fix it! Want to watch a



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Write in 188 on Reader Service Card



HO! HO! HO! Just in time for the holidays ... Check out our special gift subscription offer on page 96. run or two or three?" He was already in the middle of sample #10's first run.

I checked my watch, 'Can't, gotta get on home and toss a couple of Cornish hens in the oven before the wife gets home."

"Come to think of it, I'm getting hungry myself. Well, I've got time for another run - I'll let you know how it

"Okay, take it easy. I'll give you a call tomorrow." I beat a hasty retreat out to my

And then, all of a sudden WHAM!!!

I woke up with my face flat on his concrete sidewalk, with people milling all around me, and a meat wagon up on the curb! Lying next to me was the plastic spray can lid.

Said I, "What the hell?" and finally managed to sit up.

"Are you okay?" asked the ambulance driver.

"I think I'm in one piece, but my ears are ringing."

Right then Fred came staggering out what used to be his front door, one arm dangling uselessly, obviously broken. In his other, he was clutching a piece of chart recorder paper and waving it at me with a big grin! "I did

"You certainly did," I said, looking at his demolished house front, "but what the heck did you do?"

"Look at all of these flat lines!" he said, pushing the recorder paper in my face, "Notice anything unusual? I pushed the current from 10 amps to 200 amps: ambient temperature, flat line! Zero voltage drop, flat line! Zero resistance, flat line! What's that tell you?"

I was starting to hurt. "You blew up your house, and your Old Lady's gonna be a little miffed?"

Fred was unperturbed, "I'll buy her a few more! Come on, read the chart, will you?" I finally got it: "A room

temperature superconductor! You're now fabulously wealthy - so THAT was your original theory! What about DIGI-LOG? Don't they own

Now Fred was miffed! "Don't you remember, I already fulfilled their contract! They're getting two working alloys. This one's all mine. Although, they'll probably charge me for a new chart recorder; theirs didn't survive the blast.

"And I'm going to write your story up for a mere 10 times my usual fee! What caused the explosion anyway, Fred?

Oh, I had a little accident dropped the acrylic spray can right on the resistor assembly. Which promptly vaporized when a slider shorted and put full current right through that big steel bench - shrapnel was flying all over the place. Pretty much missed everything except my wing."

Well, they loaded us into the meat-wagon, assuring us that our injuries weren't anything life-threatening. I finally had a chance to reflect, "You know, Fred, I never did like those ceramic superconductors."

"Me neither, Skip. They don't bend." Go Figure!!! NV

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CA - LIVERMORE - Hamfest, Livermore ARK, Cliff Kibbe KF6Ell, 209-835-6715. E-Mail: larkswap@hotmail.com

IA - DES MOINES - Hamfest. Tikva Tracers ARC,

Randall Lees NOLMS, 515-279-4241.

IL - MACOMB - Hamfest, National Guard Armory, 8am-1pm. VE Exams. Talk-in: 147.060/147.660, 444,300/449,300, Lamoine Emergency ARC, Don. Johnson KA9SQB, 309-833-4626. E-Mail: Don

Johnson@ccmail.wiu.edu
NY - FARMINGVILLE - Hamfest. Radio Central ARC, JoAnn Colletti N2IME, 516-399-1877. E-

OH - MASSILLON - Hamfest. Stark County Fairgrounds, 305 Wertz Ave. N.W. Talk-in: 147.18+ repeater. MARC, Don Wade W8DEA, 330-497-7232; Terry Russ, 330-837-3091 before 10pm. E-Mail: MARC.HAMCLUB@JUNO.COM

NOVEMBER 7

CA - SANTEE - ARC of El Cajon Ham, Computer & Electronic Swapmeet. Santee Drive-in. 619-561-0052

FL - MIAMI - Hamfest: Flamingo Net/University of Miami ARC, Walt Dixon W4DWN, 305-895-0398 FL - SORRENTO - Hamfest. Lake ARA, Chuck Crittendon KA4EXM, 352-669-2075

KY - HAZARD - Swapfest. Hazard High School, south end of Rt. 15, Hazard Bypass. 8am-2pm, VEC Exams. Talk-in: 146.07/.67, KY Mountains ARC, John Farler K4AVX, 606-436-5354. E-Mail: jfarler@mis.net Web: http://www.geo

cities.com/SiliconValley/2564/hf.html
NH - LONDONDERRY - Ham Radio Flea Market. Lions Club, Mammoth Rd. (Rt. 128). 8am-1pm. The Interstate Repeater Society ARC, Paul Gifford, -1538. E-Mail: k1llx@juno.com

NM - SOCORRO - Hamfest. SARA, TARA, & City of Socorro, Al Braun AC5BX, 505-835-3456 days

or 505-835-1061 eves. E-Mail: AC5BX@juno.com Web: http://www.ees.nmt.edu/sara/ OK - ENID - Hamfest. Garfield County Fairgrounds, Hoover Bldg., Oxford & 4th Sts. 8am-5pm. VE Exams. Talk-in: 147.15+ 444.400+. Tom Worth N5LWT, 580-233-8473, E-Mail: N5LWT@HOTMAIL.COM. Fred Selfridge N5QJX, 580-242-3551, E-Mail: FREDNNEL@IONET.NET SC - MYRTLE BEACH - Beachfest '98. Myrtle

Beach High School, 38th Ave. N. VE Exams. Talk-in: 147.12. GSARC, Jim Wood KF4CJE, 843-238-0800. E-Mail: kf4cje@juno.com Web: www.w4gs.org

http://www.qsl.net/kf4hav/hamfest.htm

TX - AZLE - Hamfest. Tri-County ARC, David Johnson KB5YLG, 817-922-1081 days, 817-444-2369 eves, E-Mail: kb5ylg@gte.net Web: http://www.qsl.net/tcarc-ntxl WI - WACKESHA - Hamfest. Milwaukee Repeater

Club, Mike KB9PHA, 414-258-4435. Web: http://execpc.com/-mrc/friendlyfest.htm

NOVEMBER 7-8

GA - LAWRENCEVILLE - Hamfest. Gwinnett County Fairgrounds. Sat: 9am-5pm, Sun: 9am-3pm. VE Exams. Talk-in: 145.45, PL 107.2 if nec-Alford Memorial RC, Randy Bassett KR4NQ, 770-410-3989. E-Mail:

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Phone 909-371-8497 - Fax 909-371-3052

E-mail events@nutsvolts.com

Hamfest@totr.radio.org

TX - ODESSA - Hamfest, Ector County Coliseum, Exhibit Bldg, D., 42nd & Andrews Hwy. Sat: 8am-5pm, Sun: 9am-1pm. VE Exams. Talk-in: 145.470. West TX ARC, Robert Jordan N5RKN, 915-335-7980. E-Mail: n5rkn@apex2000.net Web; http://www.apex2000 .net/personal/wd5cwj/main2.htm

NOVEMBER 8

WI - KAUKAUNA - Hamfest. Starlite Club, Corners of Hwy. 55 & CR JJ. VE Exams. Talk-in: 146.52 simplex. Fox Cities ARC, Chad Pennings N9PRC 920-993-0485 Web: http://www.w9zl.ampr.org

NOVEMBER 14

AL - MONTGOMERY - Hamfest & Computer Show. Garrett Coliseum, S. AL State Fairgrounds. 9am-3pm. Phil 334-272-7980 after 5pm CST. E-Mail: wb4ozn@worldnet.att.net

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FL - PORT ST. LUCIE - Hamfest. St. Andrew Luthern Church, 295 N. Prima Vista Blvd. 8am-2pm. Talk-in: 146.955. Port St. Lucie ARA, Roy J. Cox KT4PA, 561-340-4319. Paul Harrison Kl4MG, 561-878-2475. E-Mail: julian@ecqual.net Web: www.geocities.com/CapeCanaveral/Hangar/4533 FL - TITUSVILLE - Hamfest. Titusville ARC, Bud

Hughes K4CW6, 407-267-3450. E-Mail: bud@expedient.com

LA - WEST MONROE - Hamfest. Twin City Ham Club, Mark Ketchell N5MYH, 318-323-6621. E-Mail: TCHC@iAmerica.net E-Mail: n5mvh@iamerica.net Web: http://cust.iamerica.net/TCHC

NOVEMBER 14-15

IN - FT. WAYNE - Hamfest & Computer Expo. Allen County War Memorial Coliseum-Expo Center. Sat: 9am-4pm, Sun: 9am-3pm. VE Exams. Talk-in: 146.88(-). Doug Jones N9NNT, 219-484-3317. E-Mail: djones2233@aol.com Web: http://www.pipeline.com/~dagagnon/

NOVEMBER 15

MA - PLYMOUTH - Hamfest. Mayflower ARC, Jack Kenealy K1BFJ, 508-830-3452. http://members.aol.com/wa1vkd/flyer.htm NC - BENSON - Jarsfest, American Legion Complex, Hwy. 301, N. 8am-4pm. Talk-in: 147.270 + 600. VE Exams. Johnston ARS, Paul Dunn KD4BJD, 919-894-3100 Web: http://www.jars.net

NOVEMBER 18

FL - ST. PETERSBURG - Hamfest. Pelican Chapter #128 QCWA, Jay Strom K9BSL, 813-822-9107

NOVEMBER 20-21

MS - OCEAN SPRINGS - Hamfest/Swapfest. MS - OCEAN SPRINGS - Hamlest/Swaptest. Latimer Community Center, N. of I-10, Exit 50. Fri: 5-9pm, Sat: 8am-2pm. Talk-in: 145.110 N5OS (-600). West Jackson County ARC, Phil Hunsberger W9NZ, 228-872-1499; Harry McLemore KD4AK, 228-872-0732

NOVEMBER 21

CA - SANTEE - ARC of El Cajon Ham, Computer & Electronic Swapmeet. Santee Drive-in. 619-561-0052

IL - LITCHFIELD - Hamfest. Central IL/St. Louis Area ATV Club, Scott Millick K9SM, 217-532-3837

NOVEMBER 21-22

FL - TAMPA - Suncoast Amateur Radio & Computer Convention. State Fairgrounds, Expo Hall. Ed Pellenz N4HRN, 813-685-7115 or 813-272-7021 xt. 3320. E-Mail: epellenz@cftnet.com Web: http://www.fgcarc.org

NOVEMBER 22

IL - WHEATON - Radio Fest, Electronics Flea Market. DuPage County Fairgrounds, Manchester Rd. GMRS of Illinois, Inc., 815-756-3933 or 630-

NY - POUGHKEEPSIE - Hamfest. Mt. Beacon ARC, Ken Akasofu KL7JCQ, 914-485-9617

NOVEMBER 28

IN - EVANSVILLE - Winter Hamfest, Vanderburgh County Fairgrounds, Exposition Center. 8am-2pm. 145.150- Evansville, 146.925- & 443.925+ Vincennes. EARS, Neil WB9VPQ 812-479-5741.

Continued on page 72

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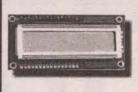


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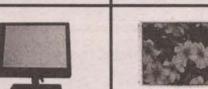
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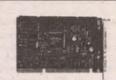
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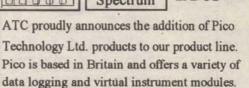


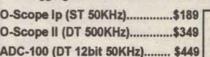












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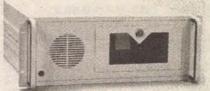
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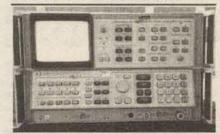
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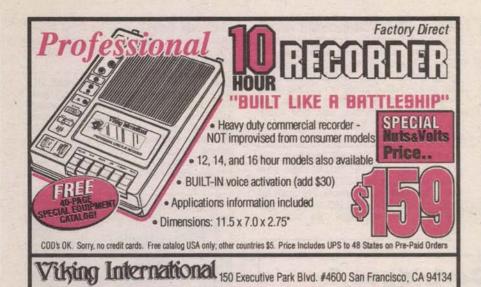
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HP 432A, Power Meter w/Cable/8478, 01-18GHz Sensor. \$350 HP 432A, Power Meter w/o Cable/Sensor. \$150 HP 435A, Power Meter w/o Sensor/Cable \$175 HP 651B, Test Oscillator, 10Hz-10MHz \$150 HP 652B, Test Oscillator, 10Hz-10MHz \$150 HP 654A, Coscillator, 10Hz-10MHz \$150 HP 1980B, Scope Measurement System w/1965A Gated Universal Timer (like new) \$550 HP 3312A, Function Generator, 1Hz-13MHz \$400 HP 3325A, Programmable Frequency Synthesizer 1Hz-32MHz \$1100 HP 3330B, Automatic Synthesizer, 20Hz-13MHz \$425 Sassar Synthesizer (2Hz-13MHz \$425 Sassar	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$675 Tek TM506, Plug-in (225MHz), Single Trace Amp. \$100 Tek TA16A, Plug-in (225MHz), Dual Trace Amp. \$75 Tek 7A19, Plug-in (800MHz), Single Trace Amp. \$150 Tek 7A26, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 7863A, Plug-in (100MHz), Time Base. \$100 Tek 78670, Plug-in (200MHz), Time Base. \$125 Tek 7870, Plug-in (200MHz), Dual Trace Base. \$75 Tek 7880, Plug-in (400MHz), Dual Trace Base. \$150
HP 432A, Power Meter wi Cable/8478, .01-18GHz Sensor. \$350 HP 432A, Power Meter wio Cable/Sensor. \$150 HP 435A, Power Meter wio Sensor/Cable \$175 HP 651B, Test Oscillator, 10Hz-10MHz \$150 HP 652B, Test Oscillator, 10Hz-10MHz \$150 HP 654A, Coscillator, 10Hz-10MHz \$150 HP 654A, Coscillator, 10Hz-10MHz \$150 HP 1830D, Logic Analyzer wipods \$550 HP 1990B, Scope Measurement System wi1965A Gated Universal Timer (like new) \$550 HP 3312A, Function Generator, 1Hz-13MHz \$490 HP 33325A, Programmable Frequency Synthesizer 1Hz-32MHz \$1,100 HP 3330B, Automatic Synthesizer, 20Hz-13MHz \$325 HP 3400A, True RMS Voltmeter, 10Hz-10MHz, 1mW-300V \$175	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot \$200 Tek TM506, Power Module, 6 Slot \$200 Tek TM506, Power Module, 6 Slot \$675 Tek 7A16A, Plug-in (225MHz), Single Trace Amp \$100 Tek 7A18, Plug-in (200MHz), Single Trace Amp \$150 Tek 7A26, Plug-in (600MHz), Dual Trace Amp \$150 Tek 7B50A, Plug-in (150MHz), Dual Trace Amp \$150 Tek 7B50A, Plug-in (100MHz), Time Base \$100 Tek 7B70, Plug-in (200MHz), Time Base \$75 Tek 7B80, Plug-in (400MHz), Delayed Time Base \$150 Tek 7892, Plug-in (300MHz), Dual Time Base \$150 Tek 7892, Plug-in (400MHz), Dual Time Base \$200
HP 432A, Power Meter wiCable/8478, 01-18GHz Sensor. \$350 HP 432A, Power Meter wio Cable/Sensor. \$150 HP 435A, Power Meter wio Sensor/Cable \$175 HP 651B, Test Oscillator, 10Hz-10MHz \$150 HP 652B, Test Oscillator, 10Hz-10MHz \$150 HP 652A, Oscillator, 10Hz-10MHz \$150 HP 653A, Oscillator, 10Hz-10MHz \$150 HP 653D, Logic Analyzer wipods \$550 HP 1980B, Soope Measurement System wi1965A Gated Universal Timer (like new) \$550 HP 3312A, Function Generator, 1Hz-13MHz \$490 HP 3330B, Automatic Synthesizer, 20Hz-13MHz \$325 HP 3400A, True RMS Meter, 10Hz-10MHz, 1mV-300V \$175 HP 3400A, True RMS Meter, AC/DIC/BB 100MHz, 1mV-300V \$175 HP 3400A, True RMS Meter, AC/DIC/BB 100MHz, 1mV-300V \$175 HP 3403C, True RMS Meter, AC/DIC/BB 100MHz, 1mV-300V \$175 HP 3403C, True RMS Meter, AC/DIC/BB 100MHz, 1mV-300V \$175 HP 3403C, True RMS Meter, AC/DIC/BB 100MHz, 1mV-300V \$175 HP 3403C, True RMS Meter, AC/DIC/BB 100MHz, 1mV-300V \$175 HP 3403C, True RMS Meter, AC/DIC/BB 100MHz, 1mV-300V \$175 HP 3403C, True RMS Meter, AC/DIC/BB 100MHz, 1mV-300V \$175 HP 3403C, True RMS Meter, AC/DIC/BB 100MHz, 1mV-300V \$175 HP 3403C, True RMS Meter, AC/DIC/BB 100MHz, 1mV-300V \$175 HP 3403C, True RMS Meter, AC/DIC/BB 100MHz, 1mV-300V \$175 HP 3403C, True RMS Meter, AC/DIC/BB 100MHz, 1mV-300V \$175 HP 3403C, True RMS Meter, AC/DIC/BB 100MHz, 1mV-300V \$175 HP 3403C, True RMS Meter, AC/DIC/BB 100MHz, 1mV-300V \$175 HP 3403C, True RMS Meter, AC/DIC/BB 100MHz, 1mV-300V \$175 HP 3403C, True RMS Meter, AC/DIC/BB 100MHz, 1mV-300V \$175 HP 3403C, True RMS Meter, AC/DIC/BB 100MHz, 1mV-30V \$175 HP 3403C, True RMS Meter, AC/DIC/BB 100MHz, 1mV-30V \$175 HP 3403C, True RMS Meter, AC/DIC/BB 100MHz, 1mV-30V \$175 HP 3403C, True RMS Meter, AC/DIC/BB 100MHz, 1mV-30V \$175 HP 3403C, True RMS Meter, AC/DIC/BB 100MHz, 1mV-30V \$175 HP 3403C, True RMS Meter, AC/DIC/BB 100MHz, 1mV-30V \$175 HP 3403C, True RMS Meter, AC/DIC/BB 100MHz, 1mV-30V \$175 HP 3403C	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot \$200 Tek TM506, Power Module, 6 Slot \$200 Tek TM506, Digitizer \$675 Tek 7A16A, Plug-in (225MHz), Single Trace Amp. \$100 Tek 7A18, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 7A19, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 7850A, Plug-in (150MHz), Time Base. \$100 Tek 7850A, Plug-in (200MHz), Time Base. \$152 Tek 7880, Plug-in (200MHz), Delay Time Base. \$150 Tek 7880, Plug-in (300MHz), Delay Time Base. \$150 Tek 7891, Plug-in (500MHz), Dual Time Base. \$200 Tek 7911, Plug-in (500MHz), Dual Time Base. \$200 Tek 7911, Plug-in (500MHz), Dual Time Base. \$200
HP 432A, Power Meter w/Cable/8478, 01-18GHz Sensor. \$350 HP 432A, Power Meter w/Cable/Sensor. \$150 HP 435A, Power Meter w/S Sensor/Cable \$175 HP 651B, Test Oscillator, 10Hz-10MHz \$150 HP 652B, Test Oscillator, 10Hz-10MHz \$150 HP 654D, Coscillator, 10Hz-10MHz \$150 HP 654D, Coscillator, 10Hz-10MHz \$150 HP 654D, Coscillator, 10Hz-10MHz \$150 HP 1830D, Logic Analyzer w/pods \$550 HP 1980B, Soope Measurement System w/1965A Gated Universal Timer (like new) \$550 HP 3312A, Function Generator, 1Hz-13MHz \$490 HP 33325A, Programmable Frequency Synthesizer Htz-32MHz \$100 HP 3330B, Automatic Synthesizer, 20Hz-13MHz \$100 HP 3430B, Automatic Synthesizer, 20Hz-13MHz \$125 HP 3403C, True RMS Meter, AC/DC/08 100MHz \$250 HP 3403C, True RMS Meter, AC/DC/08 100MHz \$250 HP 3406B, FF Voltmeter, 50LW3V 1, 26Hz \$250 Sent Sent Sent Sent Sent Sent Sent Sent	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot \$200 Tek TM506, Power Module, 6 Slot \$200 Tek TM506, Power Module, 6 Slot \$675 Tek 7A16A, Plug-in (225MHz), Single Trace Amp \$100 Tek 7A18, Plug-in (200MHz), Single Trace Amp \$150 Tek 7A26, Plug-in (200MHz), Dual Trace Amp \$150 Tek 7826, Plug-in (200MHz), Dual Trace Amp \$150 Tek 7826, Plug-in (200MHz), Dual Trace Amp \$150 Tek 7870, Plug-in (200MHz), Time Base \$150 Tek 7882A, Plug-in (500MHz), Delayed Time Base \$150 Tek 7892A, Plug-in (500MHz), Dual Time Base \$150 Tek 7011, Plug-in Digital Delay \$175
HP 432A, Power Meter wiCable/B478, 01-18GHz Sensor. \$350 HP 432A, Power Meter wio Cable/Sensor. \$150 HP 435A, Power Meter wio Sensor/Cable \$175 HP 655B, Test Oscillator, 10Hz-10MHz \$150 HP 654B, Test Oscillator, 10Hz-10MHz \$150 HP 654A, Oscillator, 10Hz-10MHz \$150 HP 654A, Oscillator, 10Hz-10MHz \$150 HP 1990B, Soope Measurement System wi1965A Gated Universal Timer (like new) \$550 HP 3312A, Function Generator, 1Hz-13MHz \$490 HP 3330B, Automatic Synthesizer, 20Hz-13MHz \$490 HP 3340B, Automatic Synthesizer, 20Hz-13MHz \$175 HP 3400A, True RMS Voltmeter, 10Hz-10MHz, 1mV-300V \$175 HP 3405A, True RMS Voltmeter, 10Hz-10MHz, 1mV-30V \$175 HP 3405A, True RMS Voltmeter, 10Hz-10MHz, 1mV-30V \$275 HP 3405A, True RMS Meter, ACD/CIB 100MHz \$250 HP 3455A, DMM 5-1/Z Diola \$250 HP 345B, DMM 5-1/Z Diola \$250 HP	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot \$200 Tek TM506, Power Module, 6 Slot \$200 Tek TM506, Power Module, 6 Slot \$675 Tek 7A16A, Plug-in (225MHz), Single Trace Amp \$100 Tek 7A18, Plug-in (200MHz), Single Trace Amp \$150 Tek 7A26, Plug-in (200MHz), Dual Trace Amp \$150 Tek 7826, Plug-in (200MHz), Dual Trace Amp \$150 Tek 7826, Plug-in (200MHz), Dual Trace Amp \$150 Tek 7870, Plug-in (200MHz), Time Base \$150 Tek 7882A, Plug-in (500MHz), Delayed Time Base \$150 Tek 7892A, Plug-in (500MHz), Dual Time Base \$150 Tek 7011, Plug-in Digital Delay \$175
HP 432A, Power Meter wiCable/8478, 01-18GHz Sensor. \$350 HP 432A, Power Meter wio Cable/Sensor. \$150 HP 435A, Power Meter wio Sensor/Cable \$175 HP 651B, Test Oscillator, 10Hz-10MHz \$150 HP 652B, Test Oscillator, 10Hz-10MHz \$150 HP 654A, Oscillator, 10Hz-10MHz \$150 HP 654A, Oscillator, 10Hz-10MHz \$150 HP 654A, Oscillator, 10Hz-10MHz \$150 HP 1980B, Soope Measurement System wi1965A Gated Universal Timer (like new) \$550 HP 3312A, Function Generator, Hz-13MHz \$490 HP 3335A, Programmable Frequency Synthesizer Hz-32MHz \$1,100 HP 3330B, Automatic Synthesizer, 20Hz-13MHz \$325 HP 3400A, True RIMS Meters A, C/DC/BB 100MHz \$275 HP 3406A, RF Voltmeter, 50uV-3V, 12GHz \$250 HP 3456A, DMM 5-1/2 Digit \$255 HP 3456A, DMM 6-1/2 Digit \$255	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$675 Tek 7A18, Plug-in (225MHz), Single Trace Amp. \$100 Tek 7A18, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 7A26, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 780A, Plug-in (100MHz), Dual Trace Amp. \$150 Tek 7850, Plug-in (100MHz), Dual Trace Amp. \$150 Tek 7870, Plug-in (200MHz), Trace Base. \$125 Tek 780A, Plug-in (500MHz), Dual Trace Base. \$150 Tek 789A, Plug-in (500MHz), Dual Trace Base. \$150 Tek 789A, Plug-in (500MHz), Dual Trace Base. \$150 Tek 7011, Plug-in Digital Delay. \$175 Tek 7015, Plug-in Counter/Timer, DC-225MHz. \$225 Tek 7118, Plug-in Samping Urit \$170 Tek 7319, Plug-in Samping Urit \$170
HP 432A, Power Meter w/Cable/8478, 01-18GHz Sensor. \$350	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$875 Tek 7A18, Plug-in (225MHz), Single Trace Amp. \$150 Tek 7A19, Plug-in (900MHz), Single Trace Amp. \$150 Tek 7A28, Plug-in (900MHz), Dual Trace Amp. \$150 Tek 7B50A, Plug-in (150MHz), Dual Trace Amp. \$100 Tek 7B50A, Plug-in (100MHz), Time Base. \$105 Tek 7B80, Plug-in (200MHz), Time Base. \$125 Tek 7B80, Plug-in (200MHz), Delayred Time Base. \$150 Tek 7B90, Plug-in (200MHz), Delayred Time Base. \$150 Tek 7B90, Plug-in (200MHz), Delayred Time Base. \$150 Tek 7B17, Plug-in Digital Delay. \$175 Tek 7D13, Plug-in CounterTimer, CDC-225MHz. \$225 Tek 7D14, Plug-in CounterTimer, CDC-225MHz. \$170 Tek 134, Current Probe Amp. \$100
HP 432A, Power Meter wiCable/8478, 01-18GHz Sensor. \$350	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$675 Tek TA16A, Plug-in (225MHz), Single Trace Amp. \$100 Tek TA19, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 7A26, Plug-in (200MHz), Single Trace Amp. \$150 Tek 7863A, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 7863A, Plug-in (100MHz), Dual Trace Amp. \$100 Tek 7863A, Plug-in (100MHz), Dual Trace Base. \$125 Tek 7892A, Plug-in (500MHz), Dual Trace Base. \$150 Tek 7892A, Plug-in (500MHz), Dual Trace Base. \$200 Tek 7701, Plug-in Digital Delay. \$175 Tek 7701, Plug-in Digital Delay. \$175 Tek 77015, Plug-in Counter/Timer, Dc 225MHz. \$225 Tek 7711, Plug-in Sampling Unit. \$175 Tek 435, Soope (60MHz), Dual Trace. \$175 Tek 435, Soope (60MHz), Dual Trace. \$175
HP 432A, Power Meter w/Cable/8478, 01-18GHz Sensor. \$350	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$675 Tek 7A18, Plug-in (225MHz), Single Trace Amp. \$100 Tek 7A18, Plug-in (600MHz), Disal Trace Amp. \$150 Tek 7A26, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 7826, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 7850, Plug-in (100MHz), Dual Trace Amp. \$150 Tek 7870, Plug-in (200MHz), Dual Trace Base. \$175 Tek 7880, Plug-in (500MHz), Dual Trace Base. \$150 Tek 7819, Plug-in (500MHz), Dual Trace Base. \$200 Tek 7011, Plug-in Digital Delay. \$175 Tek 7015, Plug-in Counter/Timer, DC-225MHz. \$225 Tek 7015, Plug-in Sampling Unit \$170 Tek 334, Current Probe Amp. \$100 Tek 455, Scope (100MHz), Dual Trace \$425
HP 432A, Power Meter wiCable/8478, 01-18GHz Sensor. \$350 HP 432A, Power Meter wio Cable/Sensor. \$150 HP 435A, Power Meter wio Sensor/Cable \$175 HP 655B, Test Oscillator, 10Hz-10MHz \$150 HP 652B, Test Oscillator, 10Hz-10MHz \$150 HP 1990B, Soope Measurement System wi1965A Gated Universal Timer (like new) \$550 HP 3912A, Function Generator, 1Hz-13MHz \$490 HP 3335B, Automatic Symthesizer, 20Hz-13MHz \$490 HP 3335B, Automatic Symthesizer, 20Hz-13MHz \$325 HP 340A, True RMS Voltmeter, 10Hz-10MHz, 1mV-300V \$175 HP 3406A, RF Voltmeter, 50U/-3V, 12GHz \$250 HP 3455A, DMM 6-1/2 Digit \$250 HP 3456A, DMM 6-1/2 Digit \$250 HP 3456A, DMM 6-1/2 Digit ACBattery, 5 Function \$225 HP 3456A, DMM 6-1/2 Digit ACBattery, 5 Function \$255 HP 3576A, Vigital Phase Gain Meter \$650 HP 3580A, Spectrum Analyzer, 5Hz-50KHz, LED Readout \$860 HP 3581A, Wave Analyzer, 15Hz-50KHz, LED Readout \$350 HP 3770A, Amplitude/Delay Distortion Analyzer \$425 HP 3770A, Amplitude/Delay Distortion Analyzer \$425	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TM16, Plug-in (25MHz), Single Trace Amp. \$150 Tek 7A18, Plug-in (25MHz), Dual Trace Amp. \$75 Tek 7A28, Plug-in (800MHz), Dual Trace Amp. \$150 Tek 7B50A, Plug-in (150MHz), Dual Trace Amp. \$150 Tek 7B50A, Plug-in (150MHz), Time Base. \$125 Tek 7B70, Plug-in (200MHz), Time Base. \$125 Tek 7B80, Plug-in (400MHz), Delayed Time Base. \$150 Tek 7B70, Plug-in (300MHz), Dual Time Base. \$150 Tek 7B70, Plug-in (300MHz), Dual Time Base. \$150 Tek 7B70, Plug-in (300MHz), Dual Time Base. \$150 Tek 7B71, Plug-in Digital Delay. \$175 Tek 7D13, Plug-in Counterfürer, DC-225MHz. \$225 Tek 7D15, Plug-in Counterfürer, DC-225MHz. \$25 Tek 314, Current Probe Amp. \$100 Tek 4855, Scope (60MHz), Dual Trace. \$175 Tek 4855, Scope (60MHz), Dual Trace. \$475 Tek 4865, Scope (60MHz), Dual Trace. \$475
HP 432A, Power Meter wiCable/8478, 01-18GHz Sensor. \$350	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$675 Tek TM18, Plug-in (1925MHz), Single Trace Amp. \$100 Tek TM18, Plug-in (190MHz), Dual Trace Amp. \$150 Tek TA26, Plug-in (200MHz), Single Trace Amp. \$150 Tek T863A, Plug-in (100MHz), Dial Trace Amp. \$150 Tek T863A, Plug-in (100MHz), Dial Trace Base. \$125 Tek T8970, Plug-in (200MHz), Time Base. \$155 Tek 7892A, Plug-in (500MHz), Dual Time Base. \$200 Tek 7791, Plug-in Digital Delay. \$175 Tek 7791, Plug-in Digital Delay. \$175 Tek 77915, Plug-in Counter/Timer, DC-225MHz. \$225 Tek 711, Plug-in Sampling Unit. \$175 Tek 455, Scope (60MHz), Dual Trace. \$175 Tek 465, Scope (100MHz), Dual Trace. \$425 Tek 466, Scope (100MHz), Dual Trace. \$475 Tek 468, Scope (100MHz), Dual Trace. \$475 Tek 466, Scope (100MHz), Dual Trace. \$475 Tek 468, Scope (100MHz), Scope, Scope, Scope, Scope, Scope, Scope, Scope, Scope, Scope, Sco
HP 432A, Power Meter w/Cable/8478, 01-18GHz Sensor. \$350	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TA16A, Plug-in (225MHz), Single Trace Amp. \$100 Tek TA18, Plug-in (225MHz), Single Trace Amp. \$75 Tek TA18, Plug-in (600MHz), Single Trace Amp. \$150 Tek TA26, Plug-in (200MHz), Dual Trace Amp. \$150 Tek T820, Plug-in (100MHz), Dual Trace Amp. \$150 Tek T850, Plug-in (100MHz), Dual Trace Amp. \$150 Tek T870, Plug-in (200MHz), Dual Trace Base. \$175 Tek T880, Plug-in (500MHz), Dual Trace Base. \$150 Tek 7819, Plug-in (500MHz), Dual Trace Base. \$200 Tek 7011, Plug-in Digital Delay. \$175 Tek 7015, Plug-in Counter/Timer, DC-225MHz. \$225 Tek 7015, Plug-in Samping Unit \$175 Tek 33, Scope (60MHz), Dual Trace. \$170 Tek 465, Scope (100MHz), Dual Trace. \$425 Tek 465, Scope (100MHz), Dual Trace. \$475 Tek 476, Scope (200MHz), Dual Trace. \$475 Tek 476, Scope (200MHz), Dual Trace. \$475 Tek 475, Scope (200MHz), Dual Trace. \$475
HP 432A, Power Meter wCable/8478, 01-18GHz Sensor. \$350 HP 432A, Power Meter wCable/Sensor. \$150 HP 432A, Power Meter wCable/Sensor. \$150 HP 432A, Power Meter wCable \$175 HP 651B, Test Oscillator. 10Hz-10MHz. \$150 HP 652B, Test Oscillator. 10Hz-10MHz. \$150 HP 652B, Cest Oscillator. 10Hz-10MHz. \$150 HP 653C, Oscillator. 10Hz-10MHz. \$150 HP 653C, Oscillator. 10Hz-10MHz. \$150 HP 1980B, Scope Measurement System w1965A Gated Universal Timer (like new) \$550 HP 3812A, Function Generator, HTx-13MHz \$490 HP 3325A, Programmable Frequency Synthesizer Htx-32MHz \$11,00 HP 3325A, Programmable Frequency Synthesizer Htx-32MHz \$1,100 HP 3330B, Autometic Synthesizer, 20Hz-13MHz \$325 HP 3400A, True RMS Voltmeter, 10Hz-10MHz, 1mW-300V \$175 HP 3403C, True RMS Meter, AC/DC/dB 100MHz \$275 HP 3456A, DMM 6-1/2 Digit \$250 HP 3456A, DMM 6-1/2 Digit \$250 HP 3456A, DMM 6-1/2 Digit \$250 HP 3581A, Mave Analyzer 5Hz-50KHz, LED Readout \$860 HP 3881A, Wave Analyzer 5Hz-50KHz, LED Readout \$360 HP 3770A, Amplitude/Delay Distortion Analyzer \$425 HP 3770B, Primary MPX Analyzer \$625 HP 3781B, Pattern Generator \$300 HP 3332A, LCR Meter \$450 HP 3931B, Crumer 100MHz HDIB \$475 \$450 HP 3931B, LCR Meter \$	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TA16A, Plug-in (225MHz), Single Trace Amp. \$100 Tek 7A18, Plug-in (225MHz), Single Trace Amp. \$75 Tek 7A18, Plug-in (800MHz), Single Trace Amp. \$150 Tek 7A28, Plug-in (800MHz), Dual Trace Amp. \$150 Tek 7B30A, Plug-in (100MHz), Dual Trace Amp. \$150 Tek 7B30A, Plug-in (100MHz), Time Base. \$100 Tek 7B30, Plug-in (200MHz), Time Base. \$125 Tek 7B30, Plug-in (200MHz), Dial Time Base. \$175 Tek 7B30, Plug-in (900MHz), Dual Time Base. \$200 Tek 7D11, Plug-in Digital Delay. \$175 Tek 7D13, Plug-in Counter/Timer, DC-225MHz. \$225 Tek 7L18, 1.5-60GHz Spectrum Analyzer \$175 Tek 453, Scope (80MHz), Dual Trace. \$175 Tek 465, Scope (100MHz), Dual Trace. \$425 Tek 4665, Scope (100MHz), Dual Trace. \$475 Tek 466, Scope (100MHz), Dual Trace. \$475 Tek 466, Scope (200MHz), Dual Trace. \$475 Tek 475, Scope (200MHz), Dual Trace. \$475 </td
HP 432A, Power Meter wCable/8478, 01-18GHz Sensor. \$350 HP 432A, Power Meter wCable/Sensor. \$150 HP 432A, Power Meter wCable/Sensor. \$150 HP 432A, Power Meter wCable \$175 HP 651B, Test Oscillator. 10Hz-10MHz. \$150 HP 652B, Test Oscillator. 10Hz-10MHz. \$150 HP 652B, Cest Oscillator. 10Hz-10MHz. \$150 HP 653C, Oscillator. 10Hz-10MHz. \$150 HP 653C, Oscillator. 10Hz-10MHz. \$150 HP 1980B, Scope Measurement System w1965A Gated Universal Timer (like new) \$550 HP 3812A, Function Generator, HTx-13MHz \$490 HP 3325A, Programmable Frequency Synthesizer Htx-32MHz \$11,00 HP 3325A, Programmable Frequency Synthesizer Htx-32MHz \$1,100 HP 3330B, Autometic Synthesizer, 20Hz-13MHz \$325 HP 3400A, True RMS Voltmeter, 10Hz-10MHz, 1mW-300V \$175 HP 3403C, True RMS Meter, AC/DC/dB 100MHz \$275 HP 3456A, DMM 6-1/2 Digit \$250 HP 3456A, DMM 6-1/2 Digit \$250 HP 3456A, DMM 6-1/2 Digit \$250 HP 3581A, Mave Analyzer 5Hz-50KHz, LED Readout \$860 HP 3881A, Wave Analyzer 5Hz-50KHz, LED Readout \$360 HP 3770A, Amplitude/Delay Distortion Analyzer \$425 HP 3770B, Primary MPX Analyzer \$625 HP 3781B, Pattern Generator \$300 HP 3332A, LCR Meter \$450 HP 3931B, Crumer 100MHz HDIB \$475 \$450 HP 3931B, LCR Meter \$	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TA16A, Plug-in (225MHz), Single Trace Amp. \$100 Tek 7A18, Plug-in (225MHz), Dual Trace Amp. \$75 Tek 7A28, Plug-in (200MHz), Single Trace Amp. \$150 Tek 7A28, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 7B3A, Plug-in (100MHz), Dual Trace Amp. \$150 Tek 7B3A, Plug-in (100MHz), Dual Trace Amp. \$150 Tek 7B3A, Plug-in (100MHz), Dual Trace Base. \$150 Tek 7B3A, Plug-in (100MHz), Dial Trace Base. \$150 Tek 7B3A, Plug-in (500MHz), Dual Trace Base. \$200 Tek 7B3A, Plug-in (500MHz), Dual Trace Base. \$200 Tek 7D11, Plug-in Digital Delay. \$175 Tek 7D11, Plug-in Digital Delay. \$175 Tek 7D15, Plug-in Counter/Timer, DC-225MHz. \$225 Tek 7D15, Plug-in Sampling Unit \$175 Tek 405, Soope (100MHz), Dual Trace. \$175 Tek 465, Soope (100MHz), Dual Trace. \$475 Tek 475, Soope (200MHz), Dual Trace. \$475 Tek 475, Soope (200MHz), Dual Trace. \$475
HP 432A, Power Meter wiCable/8478, 01-18GHz Sensor. \$350	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TA16A, Plug-in (225MHz), Single Trace Amp. \$100 Tek 7A18, Plug-in (225MHz), Single Trace Amp. \$75 Tek 7A18, Plug-in (800MHz), Single Trace Amp. \$150 Tek 7A28, Plug-in (800MHz), Dual Trace Amp. \$150 Tek 7B50A, Plug-in (100MHz), Dual Trace Amp. \$150 Tek 7B50A, Plug-in (100MHz), Dual Trace Base. \$150 Tek 7B80, Plug-in (200MHz), Time Base. \$125 Tek 7B80, Plug-in (200MHz), Dial Time Base. \$200 Tek 7B90, Plug-in (900MHz), Dial Time Base. \$200 Tek 7D11, Plug-in Digital Delay. \$175 Tek 7D13, Plug-in Counter/Timer, DC-225MHz. \$225 Tek 7D13, Plug-in Sampling Unit \$125 Tek 7S11, Plug-in Sampling Unit \$175 Tek 465, Scope (100MHz), Dual Trace. \$175 Tek 465, Scope (100MHz), Dual Trace. \$475 Tek 466, Scope (100MHz), Dual Trace. \$475 Tek 475, Scope (200MHz), Dual Trace. \$475 Tek 475, Scope (200MHz), Dual Trace. \$475
HP 432A, Power Meter wiCable/8478, 01-18GHz Sensor. \$350 HP 432A, Power Meter wio Cable/Sensor. \$150 HP 435A, Power Meter wio Sensor/Cable \$175 HP 651B, Test Oscillator, 10Hz-10MHz \$150 HP 652B, Test Oscillator, 10Hz-10MHz \$150 HP 654D, Oscillator, 10Hz-10MHz \$150 HP 654D, Oscillator, 10Hz-10MHz \$150 HP 654D, Oscillator, 10Hz-10MHz \$150 HP 1803D, Logic Analyzer w/pods \$550 HP 1803D, Logic Analyzer w/pods \$550 HP 1804B, Scope Measurement System w/1965A Gated Universal Timer (like new) \$550 HP 3312A, Function Generator, Hz-13MHz \$490 HP 3325A, Programmable Frequency Synthesizer Hz-32MHz \$1,100 HP 3330B, Autometic Synthesizer, 20Hz-13MHz \$325 HP 3400A, True RMS Voltmeter, 10Hz-10MHz, 1mV-300V \$175 HP 3456A, DMM 5-1/2 Digit \$255 HP 3456A, DMM 5-1/2 Digit \$250 HP 3456A, DMM 6-1/2 Digit \$252 HP 3456A, Poetrum Analyzer, 514z-50KHz, LED Readout \$860 HP 3581A, Wave Analyzer, 154z-50KHz, LED Readout \$360 HP 3570A, Amplitude/Delay Distortion Analyzer \$425 HP 3770B, Primary MPX Analyzer \$425 HP 3771B, Primary MPX Analyzer \$425 HP 3781B, Pattern Generator \$300 HP 4328A, Counter, 100MHz, WIDVM/Opt. 021 \$250 HP 3588A, Counter, 100MHz, WIDVM/Opt. 021 \$350 HP 3580A, Counter, 100MHz, WIDVM/Opt. 020 \$350	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TA16A, Plug-in (225MHz), Single Trace Amp. \$100 Tek TA16A, Plug-in (225MHz), Dual Trace Amp. \$75 Tek TA19, Plug-in (600MHz), Single Trace Amp. \$150 Tek TA26, Plug-in (200MHz), Dual Trace Amp. \$150 Tek TS6D, Plug-in (300MHz), Dual Trace Amp. \$150 Tek TS6D, Plug-in (200MHz), Dual Trace Amp. \$150 Tek TS6D, Plug-in (200MHz), Dual Trace Base. \$125 Tek TS7D, Plug-in (200MHz), Dual Trace Base. \$75 Tek TS8D, Plug-in (500MHz), Dual Trace Base. \$200 Tek T701, Plug-in Digital Delay. \$175 Tek T701, Plug-in Digital Delay. \$175 Tek T701, Plug-in Digital Delay. \$125 Tek T701, Plug-in Digital Delay. \$125 Tek T701, Plug-in Digital Delay. \$175 Tek T819, Plug-in Sampling Unit \$125 Tek 718, 15-60GHz Spectrum Analyzer \$1,700 Tek 436, Scope (60MHz), Dual Trace. \$175 Tek 466, Scope (100MHz), Dual Trace. \$175
HP 432A, Power Meter wiCable/8478, 01-18GHz Sensor. \$350	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TA16A, Plug-in (225MHz), Single Trace Amp. \$100 Tek 7A18, Plug-in (75MHz), Dual Trace Amp. \$75 Tek 7A18, Plug-in (600MHz), Single Trace Amp. \$150 Tek 7A28, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 7820, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 7850, Plug-in (100MHz), Dual Trace Amp. \$150 Tek 7860, Plug-in (200MHz), Dual Trace Base. \$150 Tek 7870, Plug-in (200MHz), Dual Trace Base. \$75 Tek 7802, Plug-in (500MHz), Dual Trace Base. \$200 Tek 7819, Plug-in (500MHz), Dual Trace Base. \$200 Tek 7011, Plug-in Digital Delay. \$175 Tek 7015, Plug-in Counter/Timer, DC 225MHz. \$225 Tek 7015, Plug-in Sampling Unit \$175 Tek 33, Scope (60MHz), Dual Trace. \$175 Tek 465, Scope (60MHz), Dual Trace. \$425 Tek 468, Scope (100MHz), Dual Trace. \$475 Tek 475, Scope (200MHz), Dual Trace. \$475 Tek 475, Scope (200MHz), Dual Trace. \$475
HP 432A, Power Meter wiCable/8478, 01-18GHz Sensor. \$350	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$675 Tek TM16, Plug-in (225MHz), Single Trace Amp. \$100 Tek TM18, Plug-in (190MHz), Dual Trace Amp. \$150 Tek TA19, Plug-in (800MHz), Single Trace Amp. \$150 Tek TR50A, Plug-in (200MHz), Single Trace Amp. \$150 Tek T863A, Plug-in (100MHz), Dual Trace Amp. \$150 Tek T863A, Plug-in (100MHz), Dual Trace Base. \$125 Tek T892A, Plug-in (500MHz), Dual Trace Base. \$150 Tek 7892A, Plug-in (500MHz), Dual Trace Base. \$200 Tek 7701, Plug-in Digital Delay. \$175 Tek 7701, Plug-in Digital Delay. \$175 Tek 77015, Plug-in Counter/Timer, Dc 225MHz. \$225 Tek 7711, Plug-in Sampling Unit. \$175 Tek 473, Scope (60MHz), Dual Trace. \$175 Tek 465, Scope (100MHz), Dual Trace. \$175 Tek 465, Scope (100MHz), Dual Trace. \$475 Tek 475, Scope (200MHz), Dual Trace. \$375 Tek 475, Scope (200MHz), Dual Trace. \$375
HP 432A, Power Meter wCable/8478, 01-18GHz Sensor. \$350 HP 432A, Power Meter wCable/Sensor. \$150 HP 435A, Power Meter wCable/Sensor. \$150 HP 435A, Power Meter wCosensor/Cable \$175 HP 651B, Test Oscillator, 10Hz-10MHz \$150 HP 652B, Test Oscillator, 10Hz-10MHz \$150 HP 652B, Cest Oscillator, 10Hz-10MHz \$150 HP 6530D, Logic Analyzer w/pods \$550 HP 1980B, Scope Measurement System w/1965A Gated Universal Timer (like new) \$550 HP 3812A, Function Generator, 1Hz-13MHz \$490 HP 3325A, Programmable Frequency Synthesizer Htz-32MHz \$1,100 HP 3325A, Programmable Frequency Synthesizer Htz-32MHz \$1,100 HP 3325A, Programmable Frequency Synthesizer Htz-32MHz \$1,100 HP 3330B, Autometic Synthesizer, 20Hz-13MHz \$325 HP 3400A, True RMS Voltmeter, 10Hz-10MHz, 1mt/-300V \$175 HP 3405A, DMM 5412 Digit \$252 HP 3455A, DMM 5412 Digit \$252 HP 3456A, DMM 6412 Digit \$252 HP 3456A, Downter, 100MHz, HP1B \$452 HP 3770A, Amplitude/Delay Distortion Analyzer \$425 HP 3771B, Primary MPX Analyzer \$252 HP 3781B, Pattern Generator \$300 HP 5346A, Counter, 100MHz, MP1B \$457 HP 34545, Counter, 500MHz \$450 HP 34545, Counter, 500MHz \$450 HP 34545, Counter, 500MHz \$450 HP 3454, Counter, 500MHz \$450 HP 3454, Counter, 500MHz \$450 HP 34545, Counter, 500MHz \$450 HP 3454, Counte	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TM16, Plug-in (225MHz), Single Trace Amp. \$150 Tek 7A16A, Plug-in (225MHz), Single Trace Amp. \$150 Tek 7A19, Plug-in (600MHz), Single Trace Amp. \$150 Tek 7A26, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 780A, Plug-in (100MHz), Dual Trace Amp. \$150 Tek 780A, Plug-in (100MHz), Dual Trace Amp. \$150 Tek 780A, Plug-in (100MHz), Dual Trace Base. \$175 Tek 780A, Plug-in (500MHz), Dual Trace Base. \$175 Tek 7011, Plug-in Digital Delay \$175 Tek 7015, Plug-in Counter/Timer, DC-225MHz. \$225 Tek 718, Plug-in Sampling Unit \$175 Tek 436, Scope (50MHz), Dual Trace \$175 Tek 486, Scope (100MHz), Dual Trace \$175 Tek 466, Scope (100MHz), Dual Trace \$175 Tek 475, Scope (200MHz), Dual Trace \$375
HP 432A, Power Meter wiCable/9478, 01-18GHz Sensor. \$350	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TM18, Plugher (FSMHz), Single Trace Amp. \$150 Tek 7A18, Plugher (FSMHz), Dual Trace Amp. \$150 Tek 7A28, Plugher (600MHz), Dual Trace Amp. \$150 Tek 780A, Plugher (100MHz), Dual Trace Base. \$175 Tek 780A, Plugher (500MHz), Dual Trace Base. \$250 Tek 781B, Plugher (500MHz), Dual Trace Base. \$200 Tek 7011, Plugher (500MHz), Dual Trace Base. \$200 Tek 7015, Plugher (500MHz), Dual Trace Base. \$175 Tek 7015, Plugher (500MHz), Dual Trace. \$175 Tek 731, Plugher (600MHz), Dual Trace. \$175 Tek 435, Scope (600MHz), Dual Trace. \$425 Tek 468, Scope (100MHz), Dual Trace. \$475 Tek 475, Scope (200MHz), Dual Trace. \$375 Tek 475, Scope (300MHz), Dual Trace. <t< td=""></t<>
HP 432A, Power Meter wiCable/9478, 01-18GHz Sensor. \$350	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TM16, Plug-in (225MHz), Single Trace Amp. \$150 Tek 7A16A, Plug-in (225MHz), Dual Trace Amp. \$150 Tek 7A19, Plug-in (800MHz), Single Trace Amp. \$150 Tek 7A26, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 7863A, Plug-in (100MHz), Dual Trace Amp. \$150 Tek 7863A, Plug-in (100MHz), Time Base. \$100 Tek 7892A, Plug-in (300MHz), Dual Trace Base. \$152 Tek 7892A, Plug-in (500MHz), Dual Trace Base. \$200 Tek 7791, Plug-in Digital Delay. \$175 Tek 7791, Plug-in Digital Delay. \$125 Tek 7701, Plug-in Digital Delay. \$125 Tek 7711, Plug-in Digital Delay. \$125 Tek 7715, Plug-in Counter/Timer, DC-225MHz. \$225 Tek 7116, Teb Golf-it Sportum Analyzer \$1,700 Tek 735, Scope (60MHz), Dual Trace. \$175 Tek 436, Scope (100MHz), Dual Trace. \$175 Tek 436, Scope (100MHz), Dual Trace. \$175 Tek 475, Scope (200MHz), Dual Trace. \$375 <
HP 432A, Power Meter wiCable/P478, 01-18GHz Sensor. \$350 HP 432A, Power Meter wic Cable/Sensor. \$150 HP 435A, Power Meter wic Sensor/Cable \$175 HP 655B, Test Oscillator, 10Hz-10MHz \$150 HP 654B, Test Oscillator, 10Hz-10MHz \$150 HP 1990B, Scope Measurement System wi1965A Satad Universal Timer (like new) \$550 HP 3312A, Function Generator, 1Hz-13MHz \$490 HP 3312A, Function Generator, 1Hz-13MHz \$490 HP 3330B, Automatic Synthesizer, 20Hz-13MHz \$490 HP 3330B, Automatic Synthesizer, 20Hz-13MHz \$490 HP 3405A, Ture RMS Meter, AC/DC/dB 100MHz, 1mV-300V \$175 HP 3405A, Ture RMS Meter, AC/DC/dB 100MHz, 1mV-300V \$175 HP 3455A, DMM 5-1/2 Digit \$250 HP 3456A, DMM 5-1/2 Digit \$250 HP 3456A, DMM 4-1/2 Digit \$250 HP 3456A, DMM 4-1/2 Digit \$250 HP 3575A, Digital Phase Gain Meter \$350 HP 3770A, Amplitude/Delay Distortion Analyzer \$425 HP 3779B, Primary MFX Analyzer \$425 HP 3779B, Primary MFX Analyzer \$425 HP 3779B, Primary MFX Analyzer \$425 HP 3781B, Counter, 100MHz, HPIB \$450 HP 5338A, Counter, 100MHz, PIB \$450 HP 5338A, Counter, 100MHz, PIB \$450 HP 5338A, Counter, 500MHz \$450 HP 5334A, Counter, 100MHz, PIB \$550 HP 53007A, VHF Switch \$450 HP 5307A, VHF Switch \$450 HP 5307A, VHF Switch \$450 HP 1004Retered \$450 HP 5307A, VHF Switch \$450 HP	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TM16, Plug-in (225MHz), Single Trace Amp. \$150 Tek 7A16A, Plug-in (225MHz), Single Trace Amp. \$150 Tek 7A19, Plug-in (600MHz), Single Trace Amp. \$150 Tek 7A26, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 780A, Plug-in (100MHz), Dual Trace Amp. \$150 Tek 785A, Plug-in (100MHz), Dual Trace Amp. \$150 Tek 785A, Plug-in (100MHz), Dual Trace Base. \$125 Tek 7870, Plug-in (200MHz), Dual Trace Base. \$175 Tek 7892A, Plug-in (500MHz), Dual Trace Base. \$200 Tek 7701, Plug-in Digital Delay. \$175 Tek 7701, Plug-in Digital Delay. \$175 Tek 7701, Plug-in Digital Delay. \$175 Tek 7701, Plug-in Sampling Unit \$125 Tek 7701, Plug-in Sampling Unit \$176 Tek 7815, Plug-in Sampling Unit \$176 Tek 455, Scope (60MHz), Dual Trace. \$175 Tek 455, Scope (60MHz), Dual Trace. \$175 Tek 4656, Scope (100MHz), Dual Trace. \$175
HP 432A, Power Meter wiCable/9478, 01-18GHz Sensor. \$350	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TA16A, Plug-in (225MHz), Single Trace Amp. \$150 Tek 7A18, Plug-in (200MHz), Jouel Trace Amp. \$150 Tek 7A28, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 7850A, Plug-in (100MHz), Dual Trace Amp. \$150 Tek 786A, Plug-in (100MHz), Dual Trace Amp. \$150 Tek 7870, Plug-in (200MHz), Time Base. \$150 Tek 788D, Plug-in (300MHz), Delayed Time Base. \$150 Tek 788D, Plug-in (300MHz), Dual Trace Base. \$200 Tek 7011, Plug-in Digital Delay. \$175 Tek 7015, Plug-in Counter/Timer, DC-225MHz. \$225 Tek 7015, Plug-in Counter/Timer, DC-225MHz. \$225 Tek 7015, Plug-in Sampling Unit \$175 Tek 465, Scope (100MHz), Dual Trace. \$175 Tek 465, Scope (100MHz), Dual Trace. \$175 Tek 465, Scope (100MHz), Dual Trace. \$475 Tek 475, Scope (200MHz), Dual Trace. \$475 Tek 475, Scope (200MHz), Dual Trace. \$375
HP 432A, Power Meter wiCable/P478, 01-18GHz Sensor. \$350 HP 432A, Power Meter wic Cable/Sensor. \$150 HP 435A, Power Meter wic Sensor/Cable \$175 HP 655B, Test Oscillator, 10Hz-10MHz \$150 HP 654B, Test Oscillator, 10Hz-10MHz \$150 HP 1990B, Scope Measurement System wi1965A Satad Universal Timer (like new) \$550 HP 3312A, Function Generator, 1Hz-13MHz \$490 HP 3312A, Function Generator, 1Hz-13MHz \$490 HP 3330B, Automatic Synthesizer, 20Hz-13MHz \$490 HP 3330B, Automatic Synthesizer, 20Hz-13MHz \$490 HP 3405A, Ture RMS Meter, AC/DC/dB 100MHz, 1mV-300V \$175 HP 3405A, Ture RMS Meter, AC/DC/dB 100MHz, 1mV-300V \$175 HP 3455A, DMM 5-1/2 Digit \$250 HP 3456A, DMM 5-1/2 Digit \$250 HP 3456A, DMM 4-1/2 Digit \$250 HP 3456A, DMM 4-1/2 Digit \$250 HP 3575A, Digital Phase Gain Meter \$350 HP 3770A, Amplitude/Delay Distortion Analyzer \$425 HP 3779B, Primary MFX Analyzer \$425 HP 3779B, Primary MFX Analyzer \$425 HP 3779B, Primary MFX Analyzer \$425 HP 3781B, Counter, 100MHz, HPIB \$450 HP 5338A, Counter, 100MHz, PIB \$450 HP 5338A, Counter, 100MHz, PIB \$450 HP 5338A, Counter, 500MHz \$450 HP 5334A, Counter, 100MHz, PIB \$550 HP 53007A, VHF Switch \$450 HP 5307A, VHF Switch \$450 HP 5307A, VHF Switch \$450 HP 1004Retered \$450 HP 5307A, VHF Switch \$450 HP	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TM16, Plug-in (225MHz), Single Trace Amp. \$150 Tek 7A16A, Plug-in (225MHz), Single Trace Amp. \$150 Tek 7A19, Plug-in (600MHz), Single Trace Amp. \$150 Tek 7A26, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 780A, Plug-in (100MHz), Dual Trace Amp. \$150 Tek 785A, Plug-in (100MHz), Dual Trace Amp. \$150 Tek 785D, Plug-in (200MHz), Dual Trace Base. \$175 Tek 780A, Plug-in (500MHz), Dual Trace Base. \$175 Tek 780A, Plug-in (500MHz), Dual Trace Base. \$200 Tek 7011, Plug-in Digital Delay. \$175 Tek 7015, Plug-in Counter/Timer, DC 225MHz. \$225 Tek 7118, Plug-in Sampling Unit \$175 Tek 34, Current Probe Amp. \$100 Tek 455, Scope (80MHz), Dual Trace. \$175 Tek 465, Scope (100MHz), Dual Trace. \$175 Tek 475, Scope (250MHz), Dual Trace. \$475 Tek 475, Scope (250MHz), Dual Trace. \$475 Tek 475, Scope (60MHz), Dual Trace. \$375
HP 432A, Power Meter wiCable/9478, 01-18GHz Sensor. \$350	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TM160, Pilughi (225MHz), Single Trace Amp. \$150 Tek 7A18, Pilughi (225MHz), Disul Trace Amp. \$75 Tek 7A28, Pilughi (200MHz), Disul Trace Amp. \$150 Tek 7820, Pilughi (200MHz), Time Base. \$150 Tek 7820, Pilughi (200MHz), Disul Trace Base. \$150 Tek 7820, Pilughi (300MHz), Disul Trace Base. \$150 Tek 7820, Pilughi (300MHz), Disul Trace Base. \$175 Tek 7011, Pilughi Digital Delay. \$175
HP 432A, Power Meter wiCable/9478, 01-18GHz Sensor. \$350	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TM16, Plug-in (225MHz), Single Trace Amp. \$100 Tek 7A16A, Plug-in (225MHz), Single Trace Amp. \$150 Tek 7A19, Plug-in (800MHz), Single Trace Amp. \$150 Tek 7A26, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 7826, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 7863A, Plug-in (100MHz), Dual Trace Base. \$100 Tek 7892A, Plug-in (500MHz), Time Base. \$125 Tek 7789, Plug-in (400MHz), Dual Trace Base. \$200 Tek 7791, Plug-in Digital Delay. \$175 Tek 7791, Plug-in Digital Delay. \$175 Tek 7791, Plug-in Digital Delay. \$125 Tek 771, Plug-in Digital Delay. \$125 Tek 771, Plug-in Di
HP 432A, Power Meter wiCable/9478, 01-18GHz Sensor. \$350	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TM16, Plug-in (225MHz), Single Trace Amp. \$150 Tek 7A16A, Plug-in (225MHz), Single Trace Amp. \$150 Tek 7A19, Plug-in (600MHz), Single Trace Amp. \$150 Tek 7A26, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 780A, Plug-in (100MHz), Dual Trace Amp. \$150 Tek 785A, Plug-in (100MHz), Dual Trace Amp. \$150 Tek 785D, Plug-in (200MHz), Dual Trace Base. \$175 Tek 780A, Plug-in (500MHz), Dual Trace Base. \$175 Tek 780A, Plug-in (500MHz), Dual Trace Base. \$175 Tek 7011, Plug-in Digital Delay. \$175 Tek 7012, Plug-in Counter/Timer, DC 225MHz. \$225 Tek 7118, Plug-in Sampling Unit \$175 Tek 34, Current Probe Amp. \$100 Tek 465, Scope (60MHz), Dual Trace. \$175 Tek 465, Scope (100MHz), Dual Trace. \$475 Tek 475, Scope (250MHz), Dual Trace. \$475 Tek 475, Scope (250MHz), Dual Trace. \$475 Tek 475, Scope (60MHz), Dual Trace. \$575
HP 432A, Power Meter wiCable/9478, 01-18GHz Sensor. \$350	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TM16, Plug-in (225MHz), Single Trace Amp. \$100 Tek 7A16A, Plug-in (225MHz), Dual Trace Amp. \$150 Tek 7A19, Plug-in (800MHz), Single Trace Amp. \$150 Tek 7A26, Plug-in (200MHz), Single Trace Amp. \$150 Tek 7863A, Plug-in (100MHz), Dual Trace Amp. \$150 Tek 7863A, Plug-in (100MHz), Dual Trace Base. \$100 Tek 78970, Plug-in (400MHz), Dual Trace Base. \$125 Tek 7892A, Plug-in (500MHz), Dual Trace Base. \$200 Tek 7013, Plug-in Digital Delay. \$175 Tek 7013, Plug-in Digital Delay. \$175 Tek 7015, Plug-in Counter/Timer, DC-225MHz. \$225 Tek 711, Plug-in Bampling Unit. \$175 Tek 712, Thug-in Bampling Unit. \$175 Tek 713, Plug-in Digital Delay. \$175 Tek 714, Thug-in Bampling Unit. \$175 Tek 715, Thug-in Bampling Unit. \$175 Tek 716, Thug-in Bampling Unit. \$175 Tek 718, Scope (50MHz), Dual Trace. \$175 Te
HP 432A, Power Meter wiCable/9478, 01-18GHz Sensor. \$350	Tek TM504, Power Module, 4 Slot. \$150 Tek TM506, Power Module, 6 Slot. \$200 Tek TM506, Power Module, 6 Slot. \$200 Tek TM16, Plug-in (225MHz), Single Trace Amp. \$150 Tek 7A16A, Plug-in (225MHz), Dual Trace Amp. \$150 Tek 7A19, Plug-in (800MHz), Single Trace Amp. \$150 Tek 7A26, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 7826, Plug-in (200MHz), Dual Trace Amp. \$150 Tek 7863A, Plug-in (100MHz), Dual Trace Base. \$150 Tek 7867, Plug-in (200MHz), Time Base. \$125 Tek 7892A, Plug-in (500MHz), Dual Trace Base. \$175 Tek 7892A, Plug-in (500MHz), Dual Trace Base. \$125 Tek 7011, Plug-in Digital Delay. \$175 Tek 7015, Plug-in Counter/Timer, DC-225MHz. \$225 Tek 718, 15-60GHz Spotrum Analyzer \$1,700 Tek 735, Soope (80MHz), Dual Trace. \$175 Tek 436, Soope (100MHz), Dual Trace. \$175 Tek 466, Soope (100MHz), Dual Trace. \$475 Tek 475, Soope (100MHz), Dual Trace. \$475 Tek 475, Soope (100MHz), Dual Trace. \$475 Tek 475, Soope (60MHz), Dual Trace. \$375
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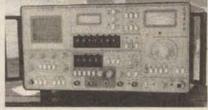
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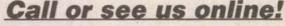
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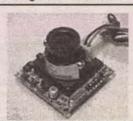
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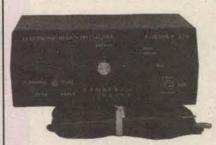
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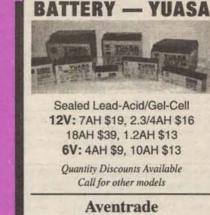
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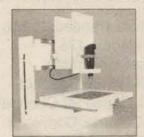
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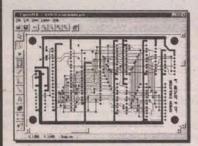
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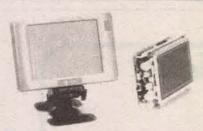
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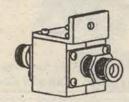
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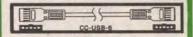


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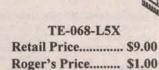
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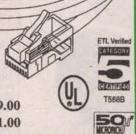


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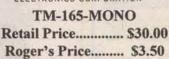
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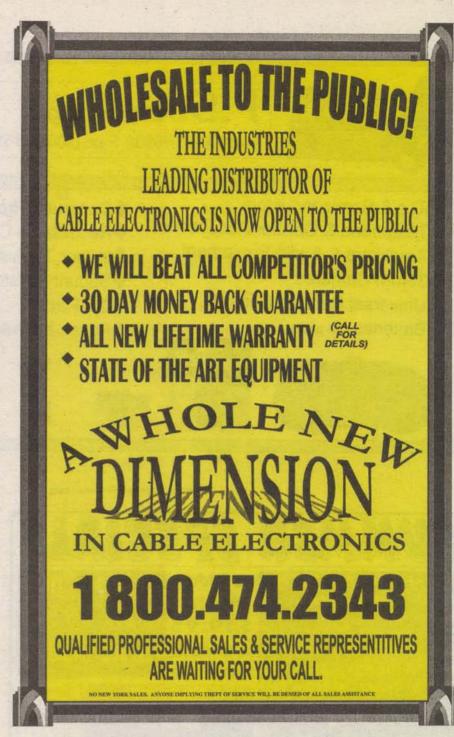
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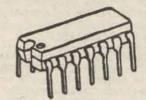
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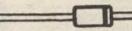


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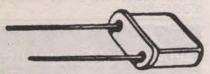
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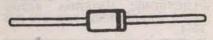
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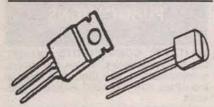




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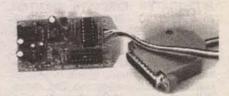
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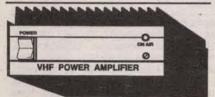
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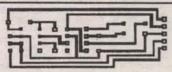
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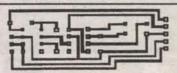
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Super Pro FM Stereo **Radio Transmitter**



cy synthesized FM Stereo transmitter sta-tion in one easy to use, handsome cabhandsome cab-inet. Most radio

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ofters all these features at this price! Kit includes cabinet, whip antenna and 120 VAC supply.

We also offer a high power export version of the FM-100 that's fully assembled with one wait of RF power, for miles of program coverage. The export version can only be shipped outside the USA, or within the US if accompanied by a signed statement that the unit will be exported.

FM-100, Professional FM Stereo Transmitter Kit... FM-100WT, Fully Wired High Power FM Transmitter.......\$429.95

AM Band Radio Transmitter |



Ramsey AM radio transmitters operate in the standard AM broadcast band and are easily set to any clear channel in your area. Our AM-25, 'pro' version, fully synthesized transmitter features easy frequency setting DIP switches for stable, no-drift frequency control, while being jumper setable for higher power output where regulations allow. The entry-level AM-1 uses a tunable transmit oscillator and runs the maximum 100 milliwatts of power. No FCC license is required, expected range is up to 1/4 mile depending upon antenna and conditions. Transmitters accept standard line-level inputs from tape decks, CD players or mike mixers, and run on 12 volts DC. The Pro AM-25 comes complete with AC power adapter, matching case set and bottom loaded wire antenna. Our entry-level AM-1 has an available matching case and knob set for a finished, professional look.

AM-25, Profi	essional AM Transmitter Kit	\$129.95 \$29.95 \$14.95
AM-1, Entry	y level AM Radio Transmitter Kithing Case Set for AM-1	\$29.95
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CCDPH-2, B&W CCD Camera, slim fit pin-h	
CCDPH-2, Color CCD Camera, wide-angle I	
IR-1, IR Illuminator Kit for B&W cameras	\$24.95
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FM Stereo Radio Transmitters



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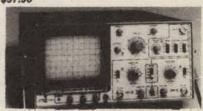
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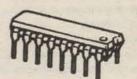
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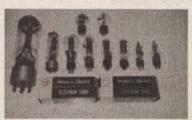
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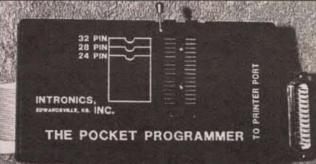


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world and make it do useful work like controlling stepping motors, monitoring fluid levels, or switching appliances on and off. No PC modification necessary for these projects either — every circuit in this book connects directly to the parallel printer port of your PC! Also included are a circuit diagram and listings for control software written in Pascal, C, and BASIC. AND (this is the good part) the accompanying disk contains full source code in all languages plus compiled (.EXE) files — (that means no typing ... yeah!) Whether you want to generate audio tones and speech, drive high power loads and DC relays, or convert DTMF tones to binary values, this book is a great source for information, projects, and ideas. There are also 9 appendices (that's plural for appendix - that hunk of helpful info that didn't fit into any one chapter of the book!) They cover such topics as expanding the parallel port for 24 bit I/O, bidirectional printer port use, and using your PC's game port for input. Controlling The World with Your PC is \$35.00

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Genesis games, the headset has both audio and motion sensing capabilities. Generally speaking, this is ideal for racing, flight, and tank simulators with a first person or rear view perspective, and games with an eye level perspective. System features volume control, sensitivity control, brightness control, tint control, as well as a reset button and mode switches to select your application. Composite video headset system includes headset, tracking tube (for motion sensing), AC adapter, Super NES cable assembly and Sega Genesis cable assembly. A pinout is also included for TV/VCR viewing.

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NOVEMBER 29

CA - SANTA ANA - Swapmeet. ACP parking lot. Mary Russo 714-558-8813 NY - PATCHOGUE - Hamfest. Mid Island ARC; Mike Grant N2OX, 516-736-9126. E-Mail: globalcm@erols.com Web:

http://members.aol.com/midisarc/98fest.html

DECEMBER 1998

Tucker KD4BWE, 334-677-7485

CA - SANTEE - ARC of El Cajon Ham, Computer & Electronic Swapmeet. Santee Drive-in. 619,561,0052

GA - CLAXTON - Hamfest, Veterans Community Center, Hwy. 280 W. VE Exams. Talk-in: 147.075+. Claxton AR Emergency Service, Mr. Ellie Waters WB4CJB, 912-653-4939. E-Mail: ellie@premierweb.net, Wes Kennedy KU4SR, 912-E-Mail: ku4sr@mci2000.com

LA - MINDEN - Christmas Hamfest, Civic Center, 520 Broadway, 8:30am-3pm, VEC Exams, MARA repeater 147,300+, MARA, Inc., Dusty Collins KB5WFE, 318-371-0636.

E-Mail: dustyc@prysm.net Web: http://www.norwesla.com/mara.htm MN - GOLDEN VALLEY - Hamfest. Courage Handi-Ham System, Nancy Meydell, 612-520-0512

NC - GREENSBORO - Hamfest. Coliseum Special Events Center. 9am-3pm. 76 Group, 336-851-1676. http://www.sabwc.com/gsohamfest

DECEMBER 6

CA - LIVERMORE - Hamfest. Livermore ARK, Cliff Kibbe KF6EII, 209-835-6715. E-Mail: larkswap@hotmail.com

DECEMBER 12

CA - FONTANA - Inland Empire ARC Amateur Radio & Electronics Swapmeet. A B Miller High

FL - LAKE CITY - Hamfest & Computer Show. Columbia County Fairgrounds, SR 247, Gateway to FL #4. Columbia ARS, Joe Aymond WD4EOJ, 904-935-2405 6-10pm, E-Mail: wd4eoj@isgroup.net or Colin Boutwell WA5RKR, 904-755-7960, E-Mail: wa5rkr@isgroup.net SC - UNION - Hamfest, Union County ARC, Roger Gregory KI4RG, 864-427-1462. E-Mail: rgregory@carol.net

DECEMBER 19

CA - SANTEE - ARC of El Cajon Ham, Computer & Electronic Swapmeet. Santee Drive-in. 619-561-0052

JANUARY 1999

JANUARY 2

TN - MORRISTOWN - Hamfest & Computer Show. Talley Ward Recreation Bldg. Talk-in: 147.303+ & 53.030-. Lakeway ARC, Perry Hensley N4PH, 423-828-4848 E-Mail: n4ph@juno.com. Kemp Lawson KF4AGB, 423-587-3320. E-Mail: kemplawson@aol.com.

Web: www.usit.net/mfawbush/larc.html

JANUARY 9

SC - GREENWOOD - Hamfest & Computer Show. Greenwood Civic Center, 1610 Hwy. 72 E. 9am-5pm. FCC exams. Talk-in: 147.165+ (open) alternate: 146.52 simplex. Greenwood ARS, Frank Kolar WA9FWO, 864-229-5639.

Web: http://www.w4gwd.org
WI - WACKESHA - Hamfest, Waukesha County Expo Center Forum, 8am-2pm, West Allis RAC, Phil Gural W9NAW, 414-425-3649

JANUARY 9-10

FL - FT. MYERS - Hamfest. Sat: 9am-3pm, Sun: 9am-2pm. Talk-in: 146.880. Ft. Meyers ARC, Colleen Sammons KQ4TR, 941-936-1431. E-Mail: csammons@juno.com

JANUARY 10

IN - SOUTH BEND - Hamfest, Michiana Valley Hamfest Assn., Bob Denniston KA9WNR, 219-291-0252

JANUARY 16

FL - LANTANA - Flea Market. Next to Pizza Hut, 6170 S. Congress Ave. 7am-12pm. Talk-in: 146.67. The Major Armstrong FM Assn., Jeff Beals WA4AW, 561-586-5120. Al West W4SDC,

LA - HAMMOND - Hamfest. Southeast Louisiana ARC, Jack Stang N5XVJ, 504-542-7605. E-Mail: jstang@i-55.com

MI - FLINT - Hamfest, AR & Youth, Clay KF8UI, 810-233-7889. E-Mail: clay@iavbbs.com MO - ST. JOSEPH - Hamfest, Ramada Inn, I-29 @ Frederick Ave. 8am-3pm. Talk-in: 146.85 and 444.925. Missouri Valley ARC & Ray Clay ARC, John Winkler WB0VRA, 816-424-6484. Gaylen Pearson, E-Mail: WB0W@IBM.Net

JANUARY 17

MI - HAZEL PARK - Hamfest. Hazel Park High School, 23400 Hughes St. 8am-2pm. Talk-in: 146.64 (-). Hazel Park ARC, Tom Austin N8TMQ, Tom Krausnick WC9F, HPARC, POB 368, Hazel Park, MI 48030.

NY - YONKERS - Flea Market, Lincoln High School, Kneeland Ave. 9am-3pm. VE Exams. Talk-in: 440.425 PL 156.7, 223.760 PL 67.0, 146.910, 443.350 PL 156.7. Metro 70cm Network Otto Supliski WB2SLQ, 914-969-1053

JANUARY 23

NC - WINSTON-SALEM - FirstFest. Dixle Classic Fairgrounds, Home & Garden Bldg. Forsyth ARC, Inc., 336-723-7388. E-Mail: n4ioz@ibm.net Web: http://www.rbdc.com/-kq4lo/farc.htm Web: http://members.xoom.com/w4nc/

JANUARY 24

OH - DOVER - Hamfest, Tusco ARC, Howard Blind KD8KF, 330-364-5258

JANUARY 29-30

MS - JACKSON - Hamfest, Jackson ARC, Ron. Brown AB5WF, 601-956-1448 or 601-982-0101. E-Mail: ab5wf@juno.com Web: http://www.jxnarc.org

JANUARY 30

AL - GREENVILLE - Hamfest, Butler & Pike County RACES, Jerry McCullough KE4ERO, 334-382-7644. E-Mail: w4mpq@alaweb.com

JANUARY 31

MD - ODENTON - Hamfest. Maryland Mobileers ARC, Bill Ziegler KA6TYY, 410-987-2384. E-Mall: ka6tyy@juno.com

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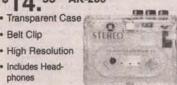
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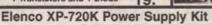
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SC - NORTH CHARLESTON - Hamfest. Charleston ARS, Jenny Myers WA4NGV, 843-747-2324. E-Mail: BRYCEMYERS@AOL.COM

FEBRUARY 6-7

FL - MIAMI - Tropical Hamboree. Fair Expo Center, S.W. 112th Ave. & Coral Way. VE Exams. Talk-in: 146.925, 146.76, 444.525. Dade Radio Club of Miami, Evelyn Gauzens. 305-642-4139, E-Mail: edg@elink.net. 305-226-5346, E-Mail: wd4sfg@bellsouth.net. Web: www.hamboree.org

FEBRUARY 7

OH - LORAIN - Hamfest, Northern Ohio ARS. Mike Willemin W8EU, 440-324-4574

FEBRUARY 12-13-14

FL - ORLANDO - Hamfest, Northern FL Section Conv., Tim Starr AE4NJ, 407-850-9258. E-Mail: AE4NJ@aol.com

Web: http://www.oarc.org/hamcat.html

FEBRUARY 13

NY - WESTFIELD - Hamfest. Westfield Exempt Volunteer Fireman's Assn., 75 Bourne St. 8am-3pm. Talk-in: 145.350 (-). Chautauqua County RAs, Eric Kroon N2PCQ, 716-595-3220. E-Mail: ekroon@netsync.net

FEBRUARY 20

FL - BROOKSVILLE - Hamfest. Spring Hill VFW Post 10209, Spring Hill Dr. between US 41 & Mariner Blvd. Talk-in: 146.715. Hernando County ARA, Ralph Wilson AF4FC, 352-754-9653. Jim Angello KE4SZP, 352-688-5214. E-Mail: iangello@fiber-net.com

Web: www.fiber-net.com/pub/hcara/index.htm
MN - BLAINE - Hamfest. Robbinsdale ARC, Jerry

Dorf N0FWG, 612-537-1722. E-Mail: jerryd@skypoint.com

FEBRUARY 21

NC - ELKIN - Hamfest. Briarpatch & Foothills ARCs, Jimmy Holbrook KB4GKI, 336-957-3820. E-Mail: kb4gki@aol.com Web: http://members.aol.com/kb4ghi/kb4gki.html

FEBRUARY 27

KY - CAVE CITY - Hamfest. Mammoth Cave ARC, 502-651-2363. E-Mail: lbrumett@glasgow ky.com Web: http://www.scrtc.blue.net/mcarc

FEBRUARY 27-28

OH - CINCINNATI - Convention. Great Lakes Div. Conv., William Tittle KA8LAY, 513-661-1861. E-Mail: gldivconvention@juno.com

FEBRUARY 28

NY - MELVILLE - Hamfest. Radio Central ARC, JoAnn Colletti N2IME, 516-399-1877. E-Mail:

OH - CIRCLEVILLE - Hamfest. Teays ARC, Roy Ulko KG8EK, 740-477-8310. E-Mail:

OH - CUYAHOGA FALLS - Hamfest. Cuyahoga Falls ARC, Carl Hervol N8JLQ, 330-497-7047. E-Mail: carlh@pop.raex.com

MARCH 1999

MARCH 5-6-7

NE - NORFOLK - State Convention, Fred Wiebelhaus NOVLX, 402-379-1929. E-Mail: dfwiebel@sufia.net Web: http://members.aol.com/davidn0xbn/evarc.html

MARCH 6-7

FL - NEW PORT RICHEY - Hamfest. Gulf Coast ARC, Rick Brown KF4GXS, 813-842-2127. E-Mail: richar@gte.net

MARCH 7

NY - LINDENHURST - Hamfest. Great South Bay ARC & Suffolk County RC, 516-422-9594. E-Mail: ka2d@li.net Web: http://www.gsbarc.org WI - WAUKESHA - Swapfest, Waukesha County Expo Center, 8am-2pm, VE Exams, Talk-in: 146.82 PL 127.3. SEWFARS, John Breecher N9NWN, 414-835-7035

MARCH 13

MO - KANSAS CITY - Hamfest, Ararat AR Shrine Club, Steve Dowdy WJ0I, 816-941-3392. E-Mail:

WA - PUYALLUP - Hamfest. Mike & Key ARC, Michael Dinkelman N7WA, 253-631-3756 or 425-867-4797. E-Mail: mwdink@eskimo.com

MARCH 13-14

NC - CHARLOTTE - Hamfest & Computerfair. Charlotte Merchandise Mart, 2500 E. Independence Blvd. Mecklenburg ARS, Tim Slay WO4G, 704-382-3234 (W) or 704-948-6283 (H). E-Mail: wo4g@w4bfb.org Web: http://www.w4bfb.org/hamfest.html

MARCH 14

OH - CONNEAUT - Hamfest, Conneaut ARC,

Jack Marttila KA8TUU, 440-593-3353

MARCH 20

FL - STUART - Hamfest. Martin County ARA, David Millard KE4AMW, 561-288-7100

MARCH 20-21

TX - MIDLAND - Hamfest. Midland ARC, Beverly Harwood KC5BNT, 915-686-1841. E-Mail: shamrock@apex2000.net Web: http://www.lxnet/edge/midswap.htm

MARCH 21

NC - KINSTON - Down East Hamfest, Lenoir County Fairgrounds, Hwy. 11 S. Barn-3pm. Doug Burt W4OFO, 252-524-5724

OH - MAUMEE - Hamfest. Toledo Mobile Radio Assn., Brenda Krukowski KB8IUP, 419-243-3836. Web: http://www.tmrahamradio.org

MARCH 27-28

MD - TIMONIUM - Maryland State Convention. Sharon Dobson N3QQC, 410-HAM-FEST (Box 3772), 1-800-HAM-FEST (Box 3772). E-Mail: n3qqc@amsat.org Web: http://www.gbhc.org

APRIL 1999

APRIL 10

NC - MORGANTON - Hamfest & Computer Fair Burke County Fairgrounds, Hwy. 181N (Exit 100 Eastbound, Exit 105 Westbound I-40). 8am-5pm. Talk-in: 147.15 (K4VLY repeater). Catawba Valley, Tom Tayler, 704-433-6205. E-Mail: kc4qpr@vistatech.net

APRIL 11

NC - RALEIGH - RARSFest. State Fairgrounds. Raleigh ARS, Wilbur Goss WD4RDT, 919-266-

APRIL 18

CT - HARTFORD - 1999 Trinity College Fire-Fighting Home Robot Contest. Trinity College campus. Jake Mendelssohn, 190 Mohegan Dr., West Hartford, CT 06117. E-Mail: JMENDEL141@AOL.COM Web: http://www.trincoil.edu/~robot

MAY 1999

NY - YONKERS - Flea Market, Lincoln High School, Kneeland Ave. 9am-3pm. VE Exams. Talk-in: 440.425 PL 156.7, 223.760 PL 67.0, 146.910, 443.350 PL 156.7. Metro 70cm Network, Otto Supliski WB2SLQ, 914-969-1053

SEPTEMBER 1999

SEPTEMBER 26

NY - YONKERS - Flea Market, Lincoln High School, Kneeland Ave. 9am-3pm. VE Exams. Talk-in: 440.425 PL 156.7, 223.760 PL 67.0, 146.910, 443.350 PL 156.7. Metro 70cm Network, Otto Supliski WB2SLQ, 914-969-1053

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7408	.33	.31	.28
7410	.19	.18	.16
7411	.55	.52	.47
7414	.27	.26	.23
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HP 346A, Noise Source, 10MHz-18GHz \$500 HP 3468A, Multimeter, 5.5 Digits \$400 HP 3580A, Spectrum Analyzer, Opt. 02 \$800 HP 4140B, Picoammeter, DC Source \$2,000 HP 4270A, Automatic Capacitance Bridge \$200 HP 436A/0222, Power Meter, HPIB \$800 HP 436A/0222, Power Meter, HPIB \$800 HP 436A, Power Meter w/2 8481A Sensors. \$3,500 HP 5004B, Signature Analyzer \$100 HP 5005B, Signature Multimeter \$350 HP 5005B, Signature Multimeter \$350 HP 5182A, Waveform Recorder, Generator \$500 HP 5316A, Universal Counter \$200 HP 5316A, Universal Counter \$200 HP 5326A/021/040, Frequency Counter, DMM \$255	Tek DM502A, Autoranging DMM \$150 Tek FG502, Function Generator, 1Hz-11MHz \$250 Tek FG504, Function Generator, 001Hz-40MHz \$500 Tek MH501, XY Monitor Scope \$200 Tek P6046, Differential Probe \$300 Tek P6508, Pulse Generator, 50MHz \$300 Tek PS503A, Dual Power Supply \$150 Tek SC502, Scope, 15MHz, Dual Trace \$250 Tek SC503, Scope, 10MHz Storage \$400 Tek SC504, Scope, 80MHz Dual Trace \$500 Tek SG502, Sig. Gen. 5Hz-50KHz TM500 Sys. \$200 Tek TG501, Time Mark Generator \$400 Tek TM503, Mainframe 3 Stot, TM500 \$100
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HP 346A, Noise Source, 10MHz-18GHz \$500 HP 3468A, Multimeter, 5.5 Digits \$400 HP 3580A, Spectrum Analyzer, Opt. 02 \$800 HP 4140B, Piccammeter, DC Source \$2,000 HP 4270A, Automatic Capacitance Bridge \$200 HP 436A/022, Power Meter, HPIB \$800 HP 438A, Power Meter w2 8481A Sensors. \$3,500 HP 5006B, Signature Analyzer \$100 HP 5006B, Signature Analyzer \$300 HP 5006B, Signature Analyzer \$300 HP 5182A, Wavelorm Recorder, Generator \$500 HP 5316A, Universal Counter \$200 HP 5326A/021/040, Frequency Counter, DMM \$250 HP 5335A/020, Universal Counter w/DVM \$800 HP 5335A/030, Frequency Counter, 1300MHz \$1,000 HP 5335A/030, Frequency Counter, 1300MHz \$1,000 HP 5335A/030, Frequency Counter, 1300MHz \$1,000 HP 5335A/030, Frequency Counter, 18GHz \$800 HP 54100D, Digital Scope, 1GHz \$2,000	Tek DM502A, Autoranging DMM \$150 Tek FG502, Function Generator, 1Hz-11MHz \$250 Tek FG504, Function Generator, 001Hz-40MHz \$500 Tek MR501, XY Monitor Scope \$200 Tek P6504, Differential Probe \$300 Tek P6508, Pulse Generator, 50MHz \$300 Tek PS503A, Dual Power Supply \$150 Tek SC502, Scope, 15MHz, Dual Trace \$250 Tek SC504, Scope, 16MHz Storage \$400 Tek SC504, Scope, 80MHz Dual Trace \$500 Tek SG502, Sig, Gen. 5Hz-50KHz TM500 Sys. \$200 Tek TM503, Mainframe 3 Stot, TM500 \$100 Texscan SSG2000, Freq. Syn., 100KHz-2GHz, \$1,800 AM, FM \$1,800 Valhalla 2000, Auto Digital Watt-Ammeter \$200 Vu-Data 5110, Semiconductor Tester, In/out Circuit \$150 Wavetek 1084, Signal Gen. Sweeper, 3,5-4,5GHz \$300
HP 346A, Noise Source, 10MHz-18GHz \$500 HP 3468A, Multimeter, 5.5 Digits \$400 HP 3580A, Spectrum Analyzer, Opt. 02 \$800 HP 4140B, Picoammeter, DC Source \$2,000 HP 4270A, Automatic Capacitance Bridge \$200 HP 436A/022, Power Meter, HPIB \$800 HP 436A, Power Meter w/2 8481A Sensors. \$3,500 HP 5004A, Signature Analyzer \$100 HP 5005B, Signature Analyzer \$300 HP 5006B, Signature Analyzer \$300 HP 5182A, Waveform Recorder, Generator \$300 HP 5182A, Waveform Recorder, Generator \$200 HP 5316A, Universal Counter \$200 HP 5336A/010-00, Frequency Counter, DMM \$250 HP 5336A/010, Frequency Counter \$300 HP 5336A/010, Frequency Counter, \$300 HP 5336A/010, Frequency Counter, \$300 HP 5340A, Frequency Counter, \$300 HP 5340A, Frequency Counter, \$300 HP 5340A, Frequency Counter, \$300 HP 54100D, Digital Scope, 1GHz \$300 HP 5400A, Digital Scope, 1GHz \$2,000	Tek DM502A, Autoranging DMM \$150 Tek FG502, Function Generator, 1Hz-11MHz \$250 Tek FG504, Function Generator, 201Hz-40MHz \$500 Tek MR501, XY Monitor Scope \$200 Tek PG504, Differential Probe \$300 Tek PG508, Pulse Generator, 50MHz \$300 Tek PS503A, Dual Power Supply \$150 Tek SC503, Scope, 15MHz, Dual Trace \$250 Tek SC503, Scope, 10MHz Dual Trace \$400 Tek SC504, Scope, 80MHz Dual Trace \$400 Tek SC501, Sig, Gen. 5Hz-50KHz TM500 Sys. \$200 Tek TG501, Time Mark Generator \$400 Tex TM503, Mainframe 3 Slot, TM500 \$100 Texscan SSG2000, Freq. Syn., 100KHz-2GHz, \$1,800 AM, FM \$1,800 Vu-Data 5110, Semiconductor Tester, In/out Circuit \$200 Vu-Data 5110, Semiconductor Tester, In/out Circuit \$300 Wavetek 1084, Signal Gen. Sweeper, 3.5-4.5GHz \$300 Wavetek 185, Sweep Function Gen. 0001-5MHz \$400
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HP 346A, Noise Source, 10MHz-18GHz	Tek DM502A, Autoranging DMM \$150 Tek FG502, Function Generator, 1Hz-11MHz \$250 Tek FG504, Function Generator, 001Hz-40MHz \$500 Tek MR501, XY Monitor Scope \$200 Tek P6504, Differential Probe \$300 Tek P6508, Pulse Generator, 50MHz \$300 Tek PS503A, Dual Power Supply \$150 Tek SC502, Scope, 15MHz, Dual Trace \$250 Tek SC504, Scope, 80MHz Storage \$400 Tek SC504, Scope, 80MHz Dual Trace \$500 Tek SG502, Sig. Gen. 5Hz-50KHz TM500 Sys. \$200 Tek TM503, Mainframe 3 Stot, TM500 \$100 Texscan SSG2000, Freq. Syn., 100KHz-2GHz, \$1,800 AM, FM \$1,800 Valhalla 2000, Auto Digital Watt-Ammeter \$200 Vu-Data 5110, Semiconductor Tester, In/out Circuit \$150 Wavetek 1084, Signal Gen. Sweeper, 3.5-4.5GHz \$300 Wavetek 1950, XY Monitor, Dual Trace \$400 Wavetek 452, Filter, Dual Hil-Lo, HHz-10KHz \$450 Wavetek 4530A, FFT Spectrum Analyzer 0-109KHz \$500
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HP 346A, Noise Source, 10MHz-18GHz \$500 HP 3468A, Multimeter, 5.5 Digits \$400 HP 3468A, Spectrum Analyzer, Opt. 02 \$800 HP 4140B, Picoammeter, DC Source \$2,000 HP 4270A, Automatic Capacitance Bridge \$200 HP 438A, Power Meter w/2 8481A Sensors. \$3,500 HP 5004A, Signature Analyzer \$100 HP 5005B, Signature Multimeter \$355 HP 5004A, Signature Multimeter \$355 HP 5006A, Signature Multimeter \$355 HP 5006A, Signature Analyzer \$300 HP 5325A, Waveform Recorder, Generator \$300 HP 5316A, Universal Counter wDVM \$250 HP 5334A/020, Universal Counter wDVM \$250 HP 5335A/030, Frequency Counter, 1300MHz \$300 HP 5340A, Frequency Counter, 1300MHz \$300 HP 5340A, Frequency Counter, 1300MHz \$300 HP 54100D, Digital Scope, 1GHz \$2,000 HP 54200A, Digital Storage Scope, Dual Trace, 200/MG/S \$1,000 HP 6112A, Power Supply, 0-40V, 0.5A \$200 HP 8165A, Programmable Signal Source, .0001-50MHz \$300 HP 8150B, Sweep Oscillator, 2-18GHz \$4,000 HP 8350B, Sweep Oscillator Mainframe \$3,000 HP 8410C/8412B, Network Analyzer w/8411A/Dct, 18, 18GHz	Tek DM502A, Autoranging DMM \$150 Tek FG502, Function Generator, .1Hz-11MHz \$250 Tek FG504, Function Generator, .001Hz-40MHz \$500 Tek MH501, XY Monitor Scope \$200 Tek P6046, Differential Probe \$300 Tek P6508, Pulse Generator, 50MHz \$300 Tek P6508A, Dula Power Supply \$150 Tek SC502, Scope, 15MHz, Dual Trace \$250 Tek SC503, Scope, 10MHz Storage \$400 Tek SC504, Scope, 80MHz Dual Trace \$500 Tek SC504, Scope, 80MHz Dual Trace \$200 Tek Tek SC504, Scope, 80MHz Dual Trace \$400 Tek Tek Tek Scope, 80MHz Dual Trace \$400 Tek Tek Tek Scope, 80MHz Dual Trace \$1,800 Valo Tek Tek Tek Scope, 80MHz Dual Trace \$200 Valo Tek Tek Tek Scope, 80MHz Dual Trace \$400 Wavetek 185, Sweep Function Gen0001-5MHz \$400 Wavetek 952, Filter, Dual Hi/Lo, 1Hz-10KHz \$450 Wavetek 957, Signal Generator, 7
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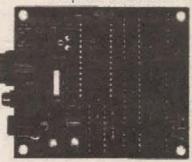






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TECH FORUM

Continued from page 44

HFFAX reception. A good pointer is http://ourworld.compuserve.com/ homepages/HFFAX/toc6.htm.

> G. L. Roylance via Internet

ANSWER TO #109814 - OCT. 1998

How you decompress your hard drive is entirely based upon which compression mechanism/program was used to compress it. There are many out there, such as Stacker, SuperStor, Doublespace, Drivespace, DriveMax, etc., and they each have different decompression methods.

Kurt Richter via Internet

ANSWER TO #10984 - OCT. 1998

You requested a way to input/output data between two computers using the serial ports. I was somewhat confused by what exactly you wanted to do, but for simple commands, DOS has just what you asked

I think the CTTY command is available in DOS 5.0 and lower, but can be used with any version after it is added to the SETVER list [type HELP SETVER, and HELP CTTY at the DOS prompt for more info).

CTTY basically re-directs keyboard input and screen output to a serial port, or other device as directed. See below for more information.

To output commands from the second computer serial port to the first, just use the echo command with the re-director. The following is an old DOS trick for testing modems, but can be modified for your use.

This is a quick way to test a modem to see if you have interrupt or software conflicts. Boot DOS using F5 (loads nothing).

At the DOS prompt ENTER: [the following assumes the modem is on COM 2].

echo ATDT > com2 (you should hear dial tone).

echo ATH > com2 (should make the modem hang up).

NOTE: On some Pentium sys-

tems with the on-board serial ports, you may have to issue the first command twice (the first time will just wake up the port).

All you should need for an interconnection cable is a three-wire cable, ground, transmit, and receive with the last two crossed.

> DB25 DB25 or on a DB9 RED TD 2 --- 2 3 TD GREEN RD 3 — 3 2 RD BLACK GRD 7 — 7 5 GRD

And from PC Mag info: The CTTY command. Purpose: Replaces the standard input and output (keyboard and screen or CON) with a different I/O device. Used rarely.

Syntax: CTTY device. Remarks: You must be sure that the specified device is both an input and output device. Use CTTY CON to reset for normal operations.

Example: CTTY AUX. All screen messages will be sent to the AUX device (the first serial port) and all keyboard input will come from that device.

You mentioned something about building a circuit to do something that would let you use two keyboards in parallel via the serial port. It would seem to me that you could do that with some simple C programming much easier.

> Randy Boettjer Oakview, CA

ANSWER TO #10982 - OCT. 1998

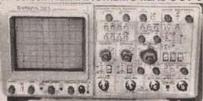
Blocking the unknowns with your Caller ID box is a very bad idea. You will block out all operator-assisted calls such as collect calls, possibly any calls from 911 [if such ever occurs), any calls from some cellphone companies, any international calls, and possibly any call from a region of the US that doesn't support Caller ID.

There are probably other occasions as well. Unknown callers are a known backdoor to the Caller ID system, and this backdoor is there for

Continued on page 85

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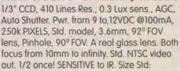
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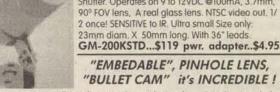
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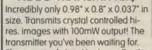
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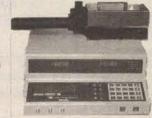
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SECURITY ELECTRONICS SYSTEMS AND CIRCUITS

by Ray Marston

Ray Marston describes a variety of add-on automobile security circuits in this final episode of the series.

ers - is wired in series with S1. This device passes no current until its applied voltage exceeds 18V, and acts like a near-short to voltages greater than 18V. Thus, in this circuit, S1 passes zero DC current when it is closed, but kills

INTRODUCTION

All previous episodes of this series have dealt with security circuits that are designed for use in domestic, commercial, or industrial applications. By contrast, this concluding episode deals exclusively with fairly simple 'add-on' security circuits designed for use in automobiles fitted with normal 12V negative-ground electrical

Modern automobiles virtually bristle with various 'security' devices and gadgets that are designed to enhance the vehicle's safety, reliability, mechanical efficiency, and immunity to theft.

If you own a reasonably modern (post 1994) automobile, it is probably already so wellequipped with good security devices that you will not need to add any more. If, on the other hand, your vehicle dates back beyond 1989, you may be able to gain by fitting one or more of the simple circuits that are described in this article, or by using one or more of the various commercial 'add-on' vehicle security units that are widely available.

The circuits described here include simple engine immobilizers and anti-theft alarms, ice-hazard, low-fuel-level, and 'lights-areon' alarms, a headlight time-delay switch, and a timed auto-turn-off rear-screen heater controller.

VEHICLE IMMOBILIZER CIRCUITS

Most immobilizers work by disabling the vehicle's engine, thus minimizing a thief's chances of starting or driving the automobile. The simplest and most effective way to immobilize a vehicle fitted with a normal petrol (gasoline) engine is to physically remove its ignition system's rotor-

This task (which was compulsory in the UK during WW2) only takes half a minute to perform, and is recommended whenever a vehicle is left parked in a public area for more than a few days, but is too inconvenient a practice for every-day use.

Instead, simple and convenient immobilizers can take the form of a secret switch (or remotely-controlled relay contacts) wired into some vital electrical part of the vehicle's engine; Figures 1 to 4 show some basic circuits of this type.

Figures 1 and 2 show how immobilizers can be wired into the

engine's ignition system. In Figure 1(a), switch S1 is wired across the engine's contactbreaker (CB) points; when S1 is open, the ignition operates normally, but when it is closed, the CB points are shorted out and the engine is unable to operate. This simple circuit gives excellent protection, particu-

larly if the wiring is carefully concealed at the CB end, but S1 must be able to handle the coil's high operating current when it is closed, and be able to withstand the CB point's typical 600V peak-to-peak 'ringing' voltages when the engine is operating normally.

The improved immobilizer circuit of Figure 1(b) does not suffer from the above snags. Here, an inexpensive and easily available 18V transient suppressor diode (D1) - which acts like a pair of back-to-back zen-

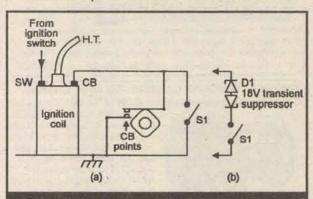


Figure 1. Contact-breaker immobilizer, operates when switch is closed.

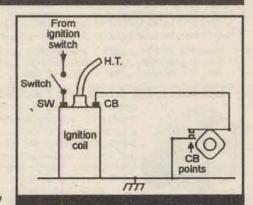


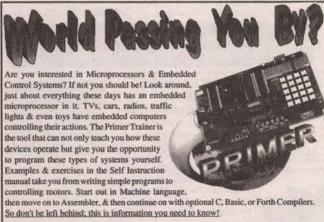
Figure 2. Ignition immobilizer, operates when switch is open.

the ignition systems vital 'ringing' voltages when an attempt is made to start the engine. This circuit gives superb anti-theft protection.

In Figure 2, the immobilizer switch is wired in series with the vehicle's ignition switch, so that the engine operates only when the switch is closed. The protection offered by this widely-used type of circuit is not quite as good as that of Figure 1, since a moderately skilled thief can easily bypass the immobilizer and ignition switches by simply hooking a wire from the battery to the SW terminal of the ignition coil.

Figure 3 shows how a heavyduty immobilizer switch can be wired into the vehicle's electric starter system, so that the starter only operates if this switch is closed. This system gives better protection than that of Figure 2, but is not as good as Figure 1 because the starter solenoid can be operated manually on many old vehicles, and also because the starter and immobilizer switches can be bypassed by a single length of wire.

Finally, Figure 4 shows how



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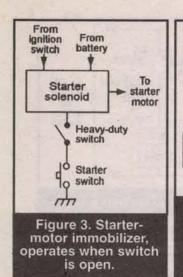
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Switch

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Figure 4.

Fuel-pump

immobilizer,

operates

when switch

is open. an immobilizer switch can be wired in series with the electric fuel pump on suitable vehicles, so that the pump only operates when this switch is closed. Note that this system lets a thief start the engine and drive for a short distance on the carburetor's residual fuel, which is quickly used up.

A weakness of the Figure 1 to 4 circuits is that they must all be turned on and off manually, and thus only give protection if the owner remembers to turn them on. By contrast, Figure 5 shows an immobilizer that turns on automatically when an attempt is made to start the engine, but can be turned off by briefly operating a hidden push-button switch. A small 'reminder' LED turns on when the engine is disabled by the immobilizer. This circuit thus gives a high level of protection, since it does not depend on the memory of its owner, and operates as follows.

The coil of 12V relay RLA is shunted by series-connected R1 and an LED, which illuminates when RLA is on, and this combination is wired in series with 1000µF capacitor C1, which is shunted by series-connected n.o. relay contacts RLA/1 and n.c. push-button switch S1. This RLA-C1 combination is wired between the ignition coil's SW terminal and ground, and the relay's RLA/2 n.o. contacts are wired across the vehicle's CB points (using a Figure 1b connection).

Normally, C1 is fully discharged; consequently, when the ignition switch is first closed a surge of current flows through RLA coil via C1, and the relay turns on and the LED illuminates. As the relay goes on, contacts RLA/1 close and lock the relay on via S1, and contacts RLA/2 close and short out the vehicle's CB points, thus immobilizing the engine. The relay stays on until S1 is briefly opened, at which point the relay unlatches and C1 charges up rapidly via the relay coil, and the relay and LED then turn off. As the relay turns off, it removes the short from the vehicle's CB points, and the engine is

able to operate in the normal way.

ANTI-THEFT ALARM CIRCUITS

Vehicle anti-theft alarms come in a variety of basic types, and the most reliable of these are the types that are switched on/off externally (rather than internally) and are activated via simple door-controlled microswitches or via a battery-voltage sensing circuit.

In modern vehicles, the external on/off control function is usually obtained via an IR remote-control system, but on older vehicles, it can be obtained cheaply and simply via a prominent key-switch (or a concealed toggle switch) fitted to the outside of the vehicle. Figures 6 to 8 show practical alarm systems of these types that are designed for use in older vehicles; each of these circuits can also act as an immobilizer and, if required, operates the vehicle's horn and lights and immobilizes the engine under the 'alarm' condition.

In the Figure 6 and 7 circuits, microswitches that are built into the vehicle are used (when the alarm system is enabled) to trip a pair of self-latching relays when. any of the car doors, hood, or trunk are opened; these relays immobilize the engine and operate the horn and headlights either directly or via additional timing circuitry.

Two suitable front-door

microswitches are built into most vehicles as standard fittings and are used to operate the courtesy or dome lights; additional domelight-operating microswitches which are readily available from

key switch. When the key switch is closed, current flows through both relays via D1 if any of the door switches close, or flows through them via D2 if any of the auxiliary switches close. In either

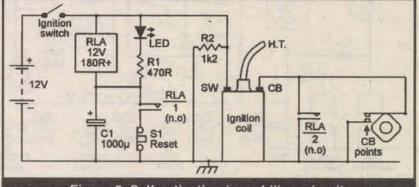


Figure 5. Self-activating immobilizer circuit.

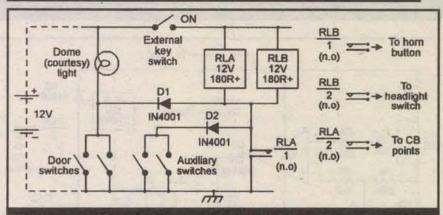


Figure 6. Basic microswitch-activated anti-theft alarm/immobilizer.

specialist 'vehicle security' retailers - can easily be fitted to the rear doors. Similar microswitches can be used as 'auxiliary' switches to protect the hood and trunk (bonnet and boot).

The operation of the Figure 6 circuit is very simple. The alarm is enabled by closing the external

case, both relays turn on.

As RLA goes on, contacts RLA/1 close and lock both relays on, and contacts RLA/2 close and short out the vehicle's CB points (using a Figure 1b connection), thus immobilizing the vehicle. Simultaneously, contacts RLB/1 close and switch on the car horn



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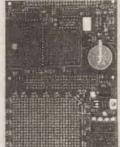
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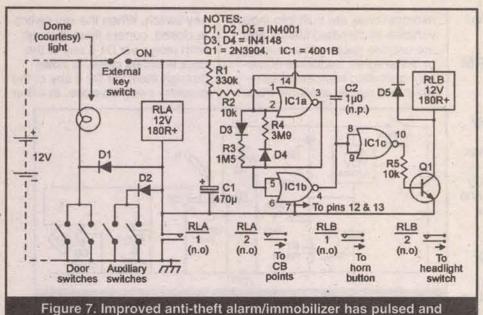
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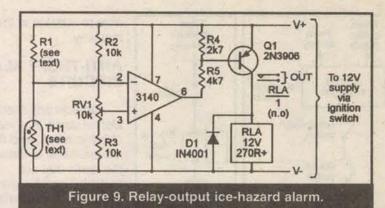
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Figure 8. Basic voltage-sensing alarm circuit.

(or a siren unit), giving an audible indication of the intrusion, and contacts RLB/2 close and switch on the headlights (or activate a headlight flasher unit), giving a visual identification of the violated vehicle. The horn and light (etc.) remain on until the key-switch is opened.

Obvious weaknesses of the simple Figure 6 circuit are that, if it is activated and is not switched



off manually within a reasonable space of time (typically 15 minutes), it will probably break local noise-control regulations, will probably damage the horn, and will eventually flatten the vehicle's battery. Figure 7 shows a way of modifying the Figure

6 circuit so that the horn and lights turn off automatically after about four minutes, but the immobilizer stays active until turned off via the key switch, thus eliminating all of the above problems.

In Figure 7, RLA turns on and self-latches in the same way as in the Figure 6 circuit, but as contacts RLA/1 close, they connect the full battery voltage across the RLB-driving timer-gated asymmetrical pulse generator formed from a 4001B CMOS IC and Q1. This generator is activated for about four minutes, via R1-C1, whenever

RLA is turned on by a 'break-in' detector, and repeatedly pulses RLB (and thus the vehicle's lights and horn) on and off, for unequal periods, for the duration of this four-minute period.

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During this 'pulsing' period, the 'off' time of RLB is controlled by C2-D3-R3 and approximates 1.5 seconds, and the 'on'-time is controlled by C2-D4-R4 and approximates four seconds, and the vehicle's horn thus generates a distinctive and easily recognized warning signal. Note that C2 is a non-polarized (n.p.) capacitor.

Finally, to complete this look at anti-theft alarm circuits, Figure 8 shows the practical circuit of a simple voltage-sensing type of alarm unit that can be used in place of the basic RLA-driving network used in the Figure 6 and 7 designs. Circuit operation relies on the fact that (when the vehicle's engine is not operating) a small but sharp drop occurs in the vehicle's battery voltage whenever a courtesy light is automatically turned on by the opening of a front door, or when the ignition is switched on. This sudden drop in voltage is detected and made to operate RLA. The system has the advantage that its 'alarm' signals are derived directly from the vehicle's battery, rather than via various microswitches, but it is not quite as reliable as a conventional microswitch-activated alarm sys-

The operation of the Figure 8 circuit - which is connected across the vehicle's battery via S1 - is fairly simple. Here, potential divider R1-R2-R3 is wired across the circuit's supply lines, and the output of this divider is fed, via RV1-R4, to the inverting (pin 2) input terminal of the 741 op-amp, which is wired in the open-loop mode, but is taken to the noninverting (pin 3) input via a simple (R5-C1-R6) time-delay 'memory' network. A small offset voltage can be applied between the two input terminals via RV1

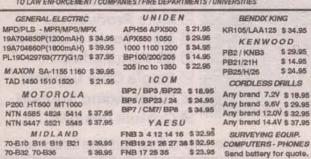
Suppose then that the RV1 offset control is adjusted so that the pin 2 voltage is fractionally higher than that of pin 3 under normal 'steady voltage' conditions and, that under this condition, the output of the op-amp is driven to negative saturation. Now if a small but abrupt fall occurs in the supply voltage, this fall is transferred immediately to pin 2 of the op-amp, but does not immediately reach pin 3 because of the timedelay or memory action of C1.

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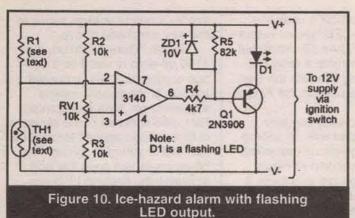
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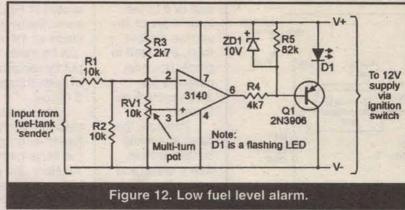
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Figure 11. Basic circuit of a typical fuel level gauge.

Consequently, pin 2 briefly goes negative relative to pin 3, and as it does so, the output of the op-amp is driven briefly to positive saturation, thus giving a positive output pulse. This pulse is used to charge C2 via D1, and C2 drives Q1-Q2 and relay RLA on via R7. As RLA goes on, contacts RLA/1 close and self-latch the relay, and contacts RLA/2 close and immobilize the vehicle via its CB points.

Note that this circuit responds only to sudden drops in voltage, and is not influenced by stable absolute values of battery voltage

The Figure 8 circuit can be used directly in place of the RLA network in the Figure 6 or 7 circuits. When installing the circuit in a vehicle, RV1 must be carefully adjusted so that the alarm turns on reliably when the courtesy (dome) light goes on, without being excessively sensitive to the small shifts that occur in the battery voltage due to its chemical action.

To find the correct setting of RV1, temporarily disable selflatching contacts RLA/1, and temporarily replace the courtesy lamp with one having roughly half its normal current rating.

Now adjust RV1 just past the point where RLA fails to activate when the lamp goes on, and then turn RV1 back a fraction, so that RLA is just activated by the courtesy light. Now refit the original courtesy light, and recheck the action. If reliable action is obtained, re-enable the RLA/1 contacts.

INSTALLING ANTI-THEFT ALARMS

The anti-theft alarms described in the last section are all designed to be turned on and off via an externally mounted switch, which may take the form of a carefully hidden toggle switch or a prominently mounted keyswitch. In either case, the switch must be mounted so that neither it or its wiring is vulnerable to damage by weather, dirt, or potential car thieves.

Once the alarm's external on/off switch has been fitted, the next installation job is to fit suitable microswitches to activate the system. Two suitable switches are already fitted to most vehicles, and are used to operate the dome or courtesy light. Additional switches must be fitted to the rear doors, and must also be fitted to the trunk and hood if full anti-theft protection is to be obtained.

Note that if your vehicle is fitted with a voltage-sensing type of

alarm system, these microswitches must be used to switch a normal filament lamp; the higher the load current used, the more reliable will be the operation of the alarm circuit; the microswitches can all be wired in parallel and used to drive a single load. When installation is complete, give your system a complete functional check, taking care not to annoy your neighbors in the process.

ICE-HAZARD ALARMS

Ice-hazard alarms activate when the vehicle's ignition is turned on and the air temperature several inches above the road surface is at or below the 0°C freezing point of water. The alarms thus indicate a risk of meeting ice under actual driving conditions. Two useful ice-hazard alarms are shown in this section, and can easily be fitted to most automobiles. Both units use a low-cost n.t.c. thermistor mounted outside of the vehicle, near its front and several inches above the road surface - as a thermal sensor that gives a good

indication of the actual road temperature. The first circuit,

shown in Figure 9, connects to the vehicle's 12V supply via its ignition switch, and turnson relay RLA under the 'ice-hazard' condition; the RLA/1 contacts can be used to activate any desired type of

external alarm device. In this circuit, the 3140 op-amp is used as a voltage comparator, in which a presettable reference voltage is applied to its pin 3 input via RV1, a temperature-sensitive variable voltage is applied to pin 2 from the R1-TH1 potential divider, and the action is such that the pin 6 output of the op-amp switches low and activates Q1 and RLA if the variable voltage exceeds the reference voltage.

In practice, the output voltage of the R1-TH1 divider rises as the TH1 temperature falls, and — if the circuit is correctly set up trips relay RLA at a TH1 temperature of precisely 0°C.

This circuit's thermistor can be any n.t.c. disc or bead type that has a resistance in the range 1K5 to 5K0 at 25°C (the normallyspecified 'nominal resistance value' temperature of most thermistors). Typically, the TH1 resistance at 0°C is about treble the 25°C value and, in this circuit, the R1 value should roughly equal TH1's '0°C' value; thus, if TH1 has a nominal 25°C value of 1K5. R1 needs a value of about 4K5.

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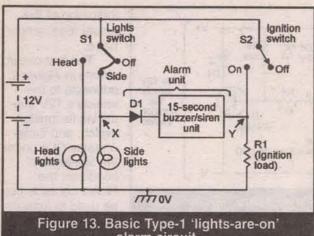
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alarm circuit.

Note, however, that the precise R1 value is not critical, since balance-control RV1 can compensate for errors in the range -50% to +100% in the R1 value. The actual methods of mounting TH1 and setting RV1 are described later in this section.

In most practical ice-hazard alarm applications, the hazard condition may continue intermittently during several hours of driving, and it is thus best to use a flashing-LED type of 'hazard alarm' indicator, rather than a continuously-active audible-warning type. Figure 10 shows the Figure 9 circuit modified to give a flashing-LED alarm output directly, rather than via a relay. In this case, Q1 is wired as an emitterfollower, and drives on D1 low-cost flashing LED device when the op-amp output switches low. Note that R4-ZD1 and Q1's base-emitter volt-drop limit D1's maximum applied voltage to a safe value of 9.4 volts.

When building either of these ice-hazard alarms, note that thermistor TH1 must be mounted in a small 'head' that is fixed to the lower front of the vehicle and connected to the main alarm-unit via twin flex. To make the head, solder the thermistor to a small tagboard and solder its leads to the twin flex. Coat the whole assembly with waterproof varnish, so that moisture will not affect its apparent resistance, then mount it in a small plastic or metal box

and fix it to the lower front of the vehicle. Before fixing the head in place, however, calibrate the alarm system as follows.

Immerse the head in a small container filled with a water and ice mixture. Use a thermometer to measure the temperature of the mixture, and add

shown in Figure 12, it uses the same flashing-LED type of output stage as the Figure 10 circuit, but can be made to give a relay output by replacing this with the type of output stage used in the Figure

Most reasonably-modern vehicles are fitted with an analog fuel-level gauge circuit that takes the basic form shown in Figure 11. Here, the gauge is actually a hot-wire (bimetal) current meter that is wired in series with a 'sender' unit that is mounted in the fuel tank and consists of a float-driven rheostat that presents

a high resistance (and a low current meter reading) when the tank is empty, and a low resistance (and a high current meter reading) when the tank is full. Note that the output voltage of the sender rises as the fuel level falls, and a low fuel level alarm can thus take the basic form of a simple

sender's output voltage varies in the way described above.

In the Figure 12 circuit, the 3140 op-amp is wired as a voltage comparator, with a pre-set fraction of the supply voltage applied to pin 3 via multiturn pot RV1, and with half of the sender's output voltage applied to pin 2 via the R1-R2 potential divider. The op-amp's output goes low and activates the flashing LED (via Q1) when the pin 2 voltage rises above the pre-set pin 3 value. To set up the circuit, wait until the fuel falls to the required 'danger' level, then connect the unit to the vehicle's supply via the ignition switch and trim RV1 so that the flashing LED just turns on. Check that the flashing LED turns off when the fuel level is increased by a modest amount.

LIGHTS-ARE-ON ALARMS

Most modern automobiles are fitted — as standard equipment with a lights-are-on reminder unit that emits a low-power audible alarm signal that warns the driver - as he/she opens the driver's door - if the car lights have

been left on. 'Lights-are-on' alarm units of this basic type are easy to build and are fairly easy to add to most older types of vehicle, and come in two basic types. Type-1 is for use in very old vehicles that are not fitted with a courtesy light that is switched automatically via a conventional dooractivated

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microswitch, and Type-2 is for use in vehicles that are fitted with such a courtesy light system.

Figure 13 illustrates the basic operating principles of a Type-1 lights-are-on alarm circuit. Here, the actual alarm consists of a lowpower 15-second buzzer or siren

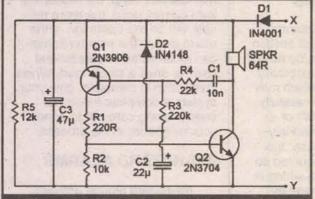


Figure 14. Practical Type-1 'lights-are-on alarm unit.

ice until a steady reading of 0°C is obtained. Now adjust RV1 so that the alarm (RLA or the flashing LED) just turns on; raise the temperature slightly, and check that the alarm turns off again. If satisfactory, the head and the alarm system can now be fixed to the vehicle.

A LOW FUEL LEVEL ALARM

One of the most annoying things that can happen to a car driver is to run out of fuel after having failed to notice the advance-warnings shown on the vehicle's fuel gauge. This event can easily be avoided by fitting the vehicle with a simple circuit that monitors the fuel gauge and activates a flashing-LED alarm under potential 'danger' conditions. A circuit of this type is

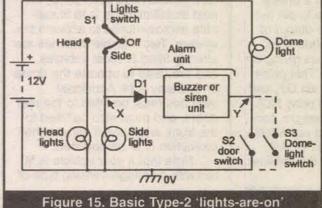


Figure 15. Basic Type-2 'lights-are-on' alarm circuit.

over-voltage alarm. A suitable 'flashing-LED' alarm circuit is shown in Figure 12.

Before starting to build the Figure 12 circuit, check that you can gain easy access to the tankmounted sender unit or the rear of the fuel gauge, and that the

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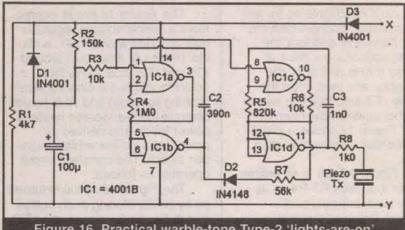
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00 +12V 100µ RLA RLA 12V 270R+ (n.o)D2 IN4001 Q1 2N3904 ₹R1 39k R2 120k To headlight switch (n.0)D1 02 IN4148 R4 12k nv m Figure 17. A headlight time-delay switch circuit.

Figure 16. Practical warble-tone Type-2 'lights-are-on alarm unit.

unit that has its supply lines wired in series with diode D1 so that current can only flow through the unit (and thus activate the buzzer/siren) when point-X is manyvolts positive to point-Y. And, in the diagram, this situation only occurs when 'lights' switch S1 is in the ON (Side or Head) position and 'ignition' switch S2 is turned OFF. Thus, if the lights are left on, the alarm unit sounds-off as soon as the ignition is switched off, but mutes automatically after 15 seconds.

Figure 14 shows a simple but practical version of a Type-1 'lights-are-on' alarm unit. Here, Q1-Q2 are wired as a modified complementary astable multivibrator that has its power supplied via D1 and uses a 64R low-power speaker as the collector load of Q2, which is a 2N3704 type and has a peak collector current rating of 800mA.

The astable's action is such that it generates a loud and fairly high alarm tone when power is initially applied, but the volume and frequency then decay steadily down to zero over a period of about 15 seconds. The decay time is controlled by R3-C2, and the initial frequency is controlled

by R3-R4 and C1. To use the unit, simply connect its 'X' and 'Y' points in the way shown in Figure

Figure 15 illustrates the basic operating principles of the Type-2 lights-are-on alarm. It is similar to the Type-1 system, except that the alarm unit is wired between 'lights' switch S1 and dome-lightactivating door-switch S2, so that the alarm only sounds if the lights are on when the driver's door is

The above Type-2 system is used on most modern vehicles, in which the dome light uses separate circuits for its 'courtesy' and

'reading' lights. A snag with most older vehicles is that they use a single light-bulb to perform both of these functions, with the 'reading' switch wired in parallel with S2, as shown by S3 in Figure 15 and, as a consequence, the alarm can be activated by either of these switches.

The easiest way around this snag is to use an auto-turn-off alarm unit that, like the Type-1 unit, only sounds for a dozen or so seconds when activated. The alarm unit can thus take the simple 'monotone' form shown in Figure 14, or can take the more attractive 'warble-tone' form

shown in the Figure 16 circuit

The Figure 16 circuit is based on warble-tone circuits shown in Part 3 of this series. In brief, however, IC1a-IC1b and R4-C2 are wired as a gated l.f. (lowfrequency) astable and IC1c-IC1d and R5-C3 form a gated h.f. (high-frequency) astable. Both astables are gated via the R2-C1 time-constant network, and are on when C1's output is below half-supply volts and off when C1's output is above half-supply volts.

When the astables are gated on, the I.f. astable frequencymodulates the h.f. astable (via D2-R7-R6), which has its output fed to piezo output transducer Tx via R8.

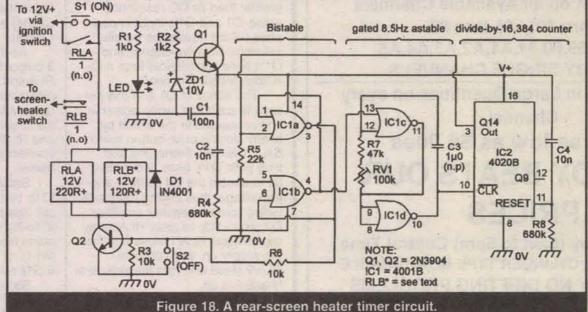
When power is connected to the Figure 16 circuit, C1 is initially fully discharged, so both astables are gated on and generate a warbletone sound in the piezo Tx, but C1 then

charges up via R2 and after a delay of about 15 seconds (determined by R2-C1) gates both astables off, silencing the piezo Tx.

When the unit's power connections are removed, C1 rapidly (in a second or so) discharges via D1-R1, and the unit is then ready to repeat its operating sequence when power is connected again.

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turn a car's headlights on for just a few minutes, during which the owner can leave and lock the vehicle, walk along a drive or pathway that is well lit by the headlights, and then enter the security of a safe building before the lights automatically turn off again. Figure 17 shows a practical transistor version of such a circuit.

In Figure 17, Q1 is an emitter follower that uses R3-R4 as its emitter load, but has 'bootstrapped' resistor R2 wired between its base and emitter, so that R2's impedance — as seen from Q1's base — is many times greater than its DC resistance value. C1 and Q1's input impedance (which equals the parallel values of R2's impedance and Q1's base impedance) form a C-R time-constant network.

The action of Q1 and this network is such that, when power is first connected to the circuit by briefly closing push-button switch S1, C1 is fully discharged and thus pulls Q1's base and emitter up to almost the full positive supply voltage, thus driving relay-activating common-emitter amplifier Q2 on via R3; as relay RLA turns on, contacts RLA/1 close and lock the supply on, and contacts RLA/2 close and turn the vehicle's headlights on.

As soon as power is connected to the circuit, C1 starts to charge up via the very high parallel impedances of R2 and Q2's base, and Q2's emitter voltage (and the current fed into Q2's base via R3) starts to decay exponentially until, after a delay of about two minutes, these values fall so low that RLA turns off. thus breaking the supply connection as RLA/1 opens and turning off the headlights as RLA/2 opens. C1 discharges rapidly via R1-D1 when the circuit's power connection is broken.

A REAR-SCREEN HEATER TIMER

Automobile rear-screen heaters draw typical operating currents of about 15 amps and thus place a heavy strain on the vehicle's electrical generating system. If the heater is inadvertently left on for long periods, this strain can greatly reduce the generator's reliability and working

Consequently, most modern automobiles are fitted with pushbutton operated rear-screen heater controllers that turn the heater off automatically after an operating period of about 16 minutes. Reliability-enhancing units of this basic type can easily be added to older vehicles and, to conclude this series, Figure 18 shows a practical add-on circuit of

The Figure 18 circuit incorporates a simple voltage regulator built around transistor Q1, a stable 16-minute timer built around IC1 and IC2, and relays RLA (which controls the circuit's semilatching function) and RLB (which controls the rear-screen heater's power feed), and derives its power feed via the vehicle's ignition switch. The complete circuit operates as follows.

The Figure 18 circuit is turned on by briefly closing push button switch S1. As S1 closes, the LED illuminates, a stable 9.4V supply is applied to the IC1-IC2 timer circuit via Q1, and 'reset' pulses are fed to the IC1a-IC1b bistable (via C2-R4) and the IC2 counter (via

C4-R8).

As the bistable resets, its pin 3 output flips high and turns on RLA and RLB via Q2; as the relays turn on, the RLA/1 contacts close, shunting S1 and locking-on the circuits supply connection, and RLB/1 contacts close and connect power to the rear-screen heater.

Simultaneously, as the IC1a-IC1b bistable resets, its pin 4 output flips low and turns on the IC1c-IC1d gated astable, which starts feeding clock pulses into pin 10 of the IC2 counter at an 8.5Hz rate.

Sixteen minutes later, in the arrival of the astable's 8192nd clock pulse, the pin 3 output of IC2 flips high and changes the state of the IC1a-IC1b bistable, which simultaneously gates off the astable and removes Q2's base drive, thus turning off both relays; as RLA turns off, it removes the timer's supply connection, and as RLB turns off, it removes power from the rearscreen heater.

Thus, when the vehicle's ignition is turned on, the Figure 18 circuit connects power to the rearscreen heater as soon as S1 is closed, but removes it again automatically after 16 minutes. If desired, the timing period can be ended prematurely by briefly closing S2, thus turning off both relays.

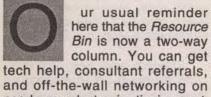
The circuit's timing period can, if you wish, be set to exactly 16 minutes by temporarily connecting an LED and 2K7 series resistor between pins 12 and 8 (0V) of IC2 and trimming RV1 so that the LED operates with precise 30-second on and off periods.

When building this circuit, note that RLA's contacts have to pass maximum currents of less than 200mA, and RLA can thus be almost any general-purpose relay, but that RLB's contacts have to pass the full operating current of the rear-screen heater (typically 15A), and RLB must thus be a dedicated heavy-duty 'automobile' relay. NV

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There's a near infinite supply of this stuff. Round and round.

The "Never be Underbid" Ploy

There's at least one company with an unusual surplus bidding strategy. They always seem to make absolutely certain they are the lowest bidder on any item. Every time. As a matter of professional pride, they'll make sure they are never underbid.

Naturally, they are also the lowest bid on items that nobody else bid on. Otherwise known as the winner. As you might suspect, their hit rate ends up kinda low. I estimate it at a few percent overall. But they still seem to get great heaping mountains of stuff. Just by bidding on nearly everything that does not eat.

The results would seem rather akin to the "send your wife to the top name on the list" chain letter. Where sheer quantity takes precedence over quality. But a few absolute gems are virtually cer-

For this low bid ploy to work, you will have to continuously run around the country in a large truck. You also must have a very definite storage and disposal plan.

Plus a good feel for what you can get away with.

The feds often require minimum bids (typically \$5.00 or

\$10.00) on the local auctions. So do be sure to ask. Other minimums (such as \$2,400.00 for a RRboxcar) are carefully spelled out. As far as I know, rejecting a high token bid on a local sale is very rare.

But on national sales, the feds do reserve their right to throw out any bids that "unfairly take advantage" of either themselves or other bidders. The criteria for an "insufficient price" rejection seems sorta bizarre.

Apparently, the cost percentage, the number of other token bidders, former item bids, and how bad it makes the rest of the sale look all get taken into account. There is some evidence that anything under 25 cents per thousand dollars acquisition cost of high value items usually gets rejected outright. But \$2.00 per thousand awards on lower demand items seem routinely accepted.

Accepted low price bids seem less generous on obvious values such as machine tools or aircraft

On the other hand, I have seen the feds reject bids which were 10 times higher what a sane individual would spend for core memory or paper tape punches. Old electronics often has a negative value. The rejected bids are shown on the bid result pages. The message here is that token bids work. So long as your items are either not much in demand, hard to get to, need heavy rework, or are obscurely described. And so long as the market remains erratic rather than efficient. The trap to watch out for is hitting on only one token bid at a site that is a long or inconvenient trip away.

Needless to say, the feds do not take lightly to "no show" bids. They get even more upset if you stiff them on a VISA card. And if you don't pick up your stuff by pumpkin time," you can lose all rights to it.

Even if paid for.

Normal pickup interval is 10 days. They tend to get very upset if you try for even a slight exten-

The Bidding Process

A useful surplus strategy might be based on buying for a penny on the dollar, selling for a dime, and trying to make a nine percent profit in the process. But note that there is a total glut in the electronic test equipment market. Lean and mean is your only ploy that works. So, your best bet is to buy surplus to build up a dream lab. Or for other personal uses.

It is best to take your time

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about the process. I grab the dynamic listing as soon as it comes up and throw it in a timeordered box. I then try to find out what each item is along with its acquisition cost. The official catalog is finally added, and bid prices are then worried over for one week before the actual bid. I do try to bid a day or two before the deadline. Note that their fax machines tend to jam up near the bid closing time.

Most of the bidding can be done online. Simply use mouse clicks and follow the instructions.

RESOURCE BIN

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If an end-user certificate will be needed (this is fairly rare), then it Patience and extreme politeis best sent via fax at the time

your bid is accepted.

Winners only are usually notified with a phone call, followed by fax and mail. Payment is easiest with VISA over the fax. At DRMO, VISA, certified checks, or exact cash. Any personal checks above \$25.00 are not allowed.

Payment must, of course, preceed any pickup.

Getting the Goods

Getting on a military base can be somewhat of a hassle. But the process usually will go something like this: Somewhere near the main gate will be a visitor contact area. You'll go there and show them your driver's licence, registration, the rental contract (if any), and proof-of-insurance. They'll issue you a day pass.

ness are essential. So is a resonable demeanor. Those "mad bomber," "dirty hippy," or "flaming-ly accessorized" looks don't seem to set all that well. It is also very important to pay extreme attention to all details. Every time.

Access ease depends upon the base. Huachucha opts for the full drill. D-M Tucson just waves you through. And Luke's DRMO is outside the gate.

The DRMO will often be a fenced area in an obscure corner of the base. Be certain to listen to all directions. Otherwise, you may get run over by a tank. You should park outside the DRMO office and then make contact with them. They then should tell you exactly where to go for pickup.

Banker's hours seem the DRMO norm. Weekdays only with most sites closed by 2 p.m..

The feds will help you load to your open conveyence only. Whatever they can safely do with a forklift. No other loading help is normally provided.

If you have someone else pick up your stuff for you, you are supposed to prefile an authorized shipper form to the DRMO ahead of time. But so far, I've gotten away with the loader having a carefully detailed printout of an authorization E-Mai, or faxing a suitable sheet of paper.

Remember, it is their gig. They can make up any rules they

\$24.00 Jeeps?

One of the most persistent urban lore myths of all time is the \$24.00 Jeep. Surprisingly, it turns out that these WW II derelicts

have (and extremely rarely continue) to be sold. The only little kicker is that these are not street legal. So they always are carefully cut in half before each sale.

These make great bookends if you have a big enough library.

It does turn out that at least one Yuppy direct mail reseller has newly been buying these up and dropping usable parts into new frames and then upgrading them to street legal. The final cost is high enough, though, that you would really want to have one of these real bad. You can find a much better Jeep in a local shop-

The feds have a big time recycling program on Humvees, so these are virtually never sold surplus.

Once.

Lots of street legal trucks and other military vehicles do get sold surplus. Many of these tend to be badly worn or have other serious problems. For some obscure reason, a lot of these ride like an army truck. Very careful inspection is the key. Be especially wary of that word "residue." Also if an "approximate quantity one" ever shows up in the description. Bidding tends to end up rather competitive on these, and they often may go for way more than they are really worth.

Free Surplus?

Most of the stuff on the sales is also available free. If you are a part of a military, government, state, or local agency. Your local city government could, say, request camping gear for sponsored Boy Scout use. Or athletic items for the city park. Or an Indian res can (and recently did) get a horse. Or a struggling volunteer fire group could try and score used turnout gear, tankers, and even crash trucks.

These uses take precedence over public sales. Full details appear on the "insider" half of the fed's mil surplus website. Needless to say, if you try to personally profit from any such scam, they will stake you to an anthill. And leave you there till the next meeting of the steering commit-

Your secret is to scan the fed's raw inventory property search to find the stuff before they get locked into any specific public sale. There are a lot of bureaucratic hassles involved.

For More Help

Your usual starting point here is at http://www.drms.com. Everything you need is theoretically on this site. Note the ".com." Not ".gov" or ".mi,l" but it does take some digging and practice to get to all the really useful stuff.

One thing you might consider is to find an agent. A relative or friend or whoever who just happens to live across the street from a remote DRMO office. Having them preview, pick up, triage, and stash the stuff can greatly simplify the process.

Conversely, when you are properly positioned and want to be an agent (for a reasonable fee or part of the stash), give me a call or E-Mail me at don@tinaja.com. I particularly could use Barstow and Edwards help.

My resource sidebars here give you the address, phone, and fax number for most of the DRMO offices. Those with an asterisk are on a hit list and have received serious death threats.

You can get your own online copies at www.tinaja.com/resbn01.html. Lots of samples of gotten goodies at www.tinaja.com/bargte01.html. The best stuff here includes Tek 2213 scopes, giant HP pen plotters, great AC motors, complete and like-new printed circuit plate thru labs, lots of Tek, HP, and Fluke premium gear, and (yup — you guessed it) a humongous 50 KW load bank. The latter FOB Thatcher.

I'll be happy to answer mil surplus questions as per our helpline. And more structured help is found at my www.tinaja.com/info01. html.

This Month's Contest

For our contest this month, just tell me your mil surplus story. Preferably as a tragedy or farce.

There should be a largish pile of my new Incredible Secret Money Machine III going to the dozen or so better entries, plus an all-expense-paid (FOB Thatcher, AZ) tinaja quest for two that will go to the very best of all.

To be fair to everyone, all entries must get written and submitted via snail mail. Send all your written entries to me here at Synergetics, rather than to Nuts & Volts editorial.

Let's hear from you. NV

Microcomputer pioneer and guru Don Lancaster is the author of 35 books and countless tech articles.

Don is the webmaster of his Guru's Lair found at http://www.tinajacoml/tinaja. You can reach Don at Synergetics, Box 809, Thatcher, AZ 85552. Or send any messages to don@tinaja.com.

TECH FORUM

Continued from page 74

these and other emergency occasions. Don't deadbolt the emergency escape.

Kurt Richter via Internet

ANSWER TO #10989 - OCT. 1998

Innotech Systems, Inc. makes a broad line of remote control ICs. Their IC4001 is a universal transmitter that can control up to four devices.

Their IC1001 IR is a remote control receiver IC. Data sheets for these and other similar devices are available in .PDF format and their web page is http://www.innotechsystems.com/shrtfrm.htm.

Tom Tillander Bay village, OH

ANSWER TO #9981 - SEPT. 1998

Use very thin copper foil, backed with adhesive (aluminum oxidizes too soon) or conductive paint on the inside of the case, greatest leakage remaining is around the ports and keyboard.

Fashion a metallic cover for any unused I/O port, and be sure all current external connecters mate metal to metal, and maintain electrical continuity on all shield components.

The keyboard is tricky if not already shielded by OEM. Each laptop design requires some ingenuity to prevent shorting your system board against the EMI shielding. Always remember if your plug-in items are using fully shielded cables.

Rick Kajander via Internet

ANSWER TO #9982 - SEPT. 1998

The SAFE 250 is probably a 24-volt operation. Typically, the UPS is higher voltage for higher output for the same reason autos went from six volts in the pre-1960s to 12 volts.

By having a higher source volt-

ANSWER TO #109812 - OCT. 1998

The easiest way to accomplish the switching that you require is to use a single diode as a switch.

You place the power supply parallel with the battery pack and place a diode on the battery positive lead so that the battery feeds the computer through this diode.

When the wall power runs the computer, it has a slightly higher voltage than the battery pack which means the battery won't flow through the diode to the computer until the

Battery

Power supply

(H)

wall power fails.

0

Computer

When the wall power fails, the diode will switch into conduction within a few microseconds, or nanoseconds, and will power the computer from the battery without the characteristic surge that most relays cause.

You can still add a trickle charger to the back side of the battery pack using a small diode [4001] and resistor combination to regulate the current flow to the battery from either a separate transformer or from the original power supply that runs the

computer.

There will be a voltage drop across the battery feed diode, so choose a diode that has the lowest possible drop. Choose one with the lowest recover time and correct amperage also.

Chris Bieber, CA

age, the current is lowered. The key to the voltage of operation aside from some of the frequencies may vary due to lower voltage, is the transformer used to transform the chopped 24 volts up to a 110-volt squarewave output.

The turns ratio of the transformer is typically 5:1, to give a 5 tomes increase in the input voltage. Using 12 volts to get the 110-volt squarewave will require a transformer with a turns ratio of 10:1. So, if your SAFE 250 is a 24 volt input, then it will not operate from 12 volts without a major transformer modification.

There are several UPSs that are 12-volt operated. Some of the smaller Triplite are ones I have worked

with. If yours happens to be one designed for 12-volt operation, then the only thing you have to do is get it to switch into UPS Mode, and normally this is accomplished by removing the 110-volt input supply. However, they will not usually switch into the backup mode without first having the 110-volt source then disconnecting.

You can look in the unit and find the switching relay — and manually operate — or supply voltage to the coil to operate it. You can also wire a mechanical switch across the contacts. The configuration can vary from one to another. Could be single pole or double pole as needed.

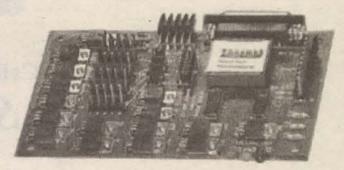
Ed Pruitt Keller, TX

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by Joseph J. Carr

Flipping Out Over Flip-Flops

igital logic functions can be made from combinations of AND, OR, and NOT gates.
Even the NAND and NOR functions are only variants of NOT-OR and NOT-AND configurations.

One of the problems with gates is that they are transient circuits; that is, they are incapable of storing information even for a short period of time. Flip-flops, on the other hand, are circuits that can store single-bits of information. Many forms of solidstate computer memory devices are little more than arrays of flip-flops

S

R

S

R

Ø

Figure 1.

Figure 2.

organized in a manner that allows storage of digital words in a comput-

Most flip-flops are bistable devices, i.e., they have two stable output states. The flip-flop is not particularly concerned which state is in existence at any given time. Being bistable, it is happy in either state. If the output is labeled Q, we find that either Q = HIGH or Q = LOW is an acceptable state, and will be stable. Some flip-flips are equipped with two complementary outputs, labeled Q and NOT-Q (or bar-Q).

R-S Flip-Flops

One of the simplest flip-flops is the reset-set (R-S) flip-flop. These circuits can be made from either NAND or NOR gates, although the performance attributes are different for the two different forms. The NOR-logic configuration and the associated symbol is shown in Figure 1. Note that the circuit has two outputs: Q and NOT-Q. This is an example of a complementary output flip-flop. These outputs always have the opposite state. If Q = HIGH, then NOT-Q = LOW, and vice

> S flip-flop, the output changes state when an appropriate input is momentarily brought HIGH from its resting operation of the NORsummarized below:

0

1. When both S and

simultaneously

HIGH,

versa. In the NOR-logic R-LOW position. Only a brief pulse at the input is needed to effect the change. The rules of logic R-S flip-flop are

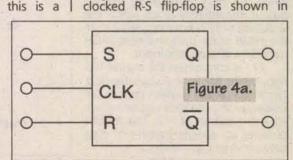
R inputs are LOW, no change occurs in the output.

2. If both S and R brought

0 0 CLOCK O Figure 3. 0 0

Q

Q



disallowed state. This input condition should be avoided.

3. Bringing the 5 input momentarily HIGH will set the output, i.e., makes Q = HIGH and NOT-O = LOW.

4. Bringing the R input momentarily HIGH resets the flip-flop, i.e., makes Q = LOW and NOT-Q = HIGH.

The basic NOR gate R-S flip-flop can be constructed from either TTL, CMOS, or other logic family NOR

gate arrays.
The NAND-logic R-S flip-flop uses inverted logic, i.e., the output state changes are caused by bringing the appropriate input LOW. An example of a NAND-logic R-S flip-flop and its symbol are shown in Figure 2.

Because the inputs are active-LOW, this circuit is sometimes called a NOT-R-S flip-flop. In this text, however, it is more convenient to simply refer to both NAND-logic and NOR-logic circuits as simply R-S flip-flops. The NAND/NOR distinction is made in the text, where necessary, or by the schematic.

The output conditions of the NAND-logic R-S flip-flop are shown below.

1. If the S and R inputs are simultaneously LOW, then a disallowed state exists. This state must be avoid-

2. If both S and R inputs are made simultaneously HIGH, then no change in the inputs will occur.

3. If the S input is momentarily brought LOW, while the R input remains HIGH, then Q = HIGH and the NOT-Q = LOW. The flip-flop is in the "set" state.

4. If the R input is momentarily brought LOW, while the S input remains HIGH, then the flip-flop is reset, i.e., Q = LOW and NOT-Q = HIGH.

The R-S flip-flop is used frequently in applications where a pulse applied to the S or R input sets a condition, and then a subsequent pulse is used to reset the circuit to its initial condition.

Clocked R-S Flip-Flops

The operation of the two previous R-S flip-flops - the NAND-logic and NOR-logic - was unconditional. The output state changed immediately when an appropriate input pulse was received. This is called asynchronous operation.

The clocked R-S flip-flop in Figure 3 is able to operate synchronously; i.e., the output will change state only when the input pulse coincides with a clock pulse. This behavior is obtained by adding a pair of NAND gates to the NAND-logic R-S flip-flop circuit.

The commonly used schematic diagram circuit symbol for the clocked R-S flip-flop is shown in



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Figure 4A, while the timing diagram is in Figure 4B. The clock circuit produces a chain of squarewaves at the CLK input (also called "C" in some cases). Note that the Q output does not change state immediately when the S input pulse goes HIGH. The output waits until the clock input is also HIGH. Similarly, the output is not reset until the clock pulse and R input pulses are coincident. Because of this feature, the literature for some scientific instruments calls the clocked R-S flip-flop a coincidence detector.

Master-Slave Flip-Flops

It is often difficult, or impossible, to transfer data through a circuit in an orderly manner. We often get into high-speed digital analogies of the old-fashioned "relay race" problem. Recall that type of problem in circuits where two electromechanical relay switches are supposed to close simultaneously. If one relay is a little sluggish, or the other is a little snappier than the other (or both!), then there is a brief instant where one is open and the other is still closed, or vice versa. This condition often produces unpredictable or even disastrous results. The same action exists in digital circuits where the culprit is differences in device propagation time, i.e., the time required for a pulse to travel through the circuit to effect an output change.

Note that two clocked R-S flipflops and an inverter can be used to synchronize data transfer. The circuit, which is shown in Figure 5, is called a master-slave flip-flop, also sometimes called the RST flip-flop.

In Figure 5, the inputs to FF1 are the inputs to the circuit as a whole, i.e., the inputs to the master-slave FF. The outputs of the master-slave FF are the outputs of flip-flop FF2. Also, the clock affects FF2 directly, but must be inverted before being applied to FF1. Both flip-flops only go active when their respective clock inputs are HIGH.

A timing diagram for this circuit is shown in Figure 6. Recall from above that FF1 is enabled when the overall clock pulse is LOW, and FF2 is enabled when it is HIGH (because of the inverter action).

When the pulse is applied to the S input, nothing happens at Q1 (the Q output of FF1) until the clock pulse drops LOW again. At that time, Q1 snaps HIGH, thereby making the S input of FF2 HIGH also. But at this time the block pulse is LOW, so no change occurs at the FF2 output terminal. When the next clock pulse arrives, however, the FF2 clock input goes HIGH (Q1 and S2 are still HIGH), so the Q output of FF2 goes HIGH.

Similarly, the reset pulse arrives when the clock is LOW, so the Q1 output immediately drops LOW. The Q output of FF2, however, remains in the HIGH state until the next HIGH transition of the clock input.

FF1 is considered the master flipflop, while FF2 is the slave flip-flop. The action at FF1 is given time to settle before the changes can be reflected in the output of FF2. This feature provides an orderly transfer of data between input and output.

Type-D Flip-Flops

A Type-D flip-flop is a modified RST flip-flop that has only one input (labeled D for "data"). See Figure 7. The type-D flip-flop will transfer data (HIGH or LOW) from the D input to the Q output only when the clock terminal is HIGH. The following rules

govern the behavior of the type-D flip-flop.

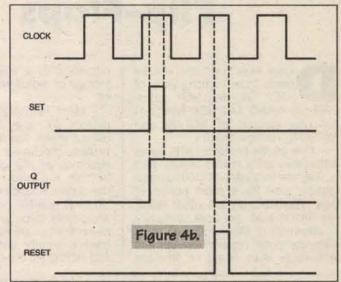
1. When the clock input goes HIGH, the data (HIGH or LOW state) present on the D input is transferred to the Q output.

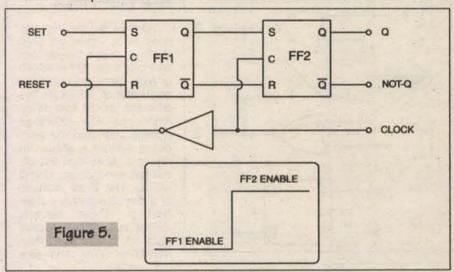
2. If the clock input remains HIGH, then the Q output will follow changes in the data at the D input.

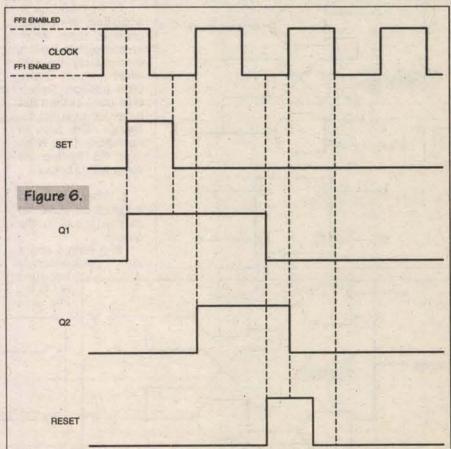
3. If the clock input

remains LOW, then the Q output will retain the last data that was present on the D input at the instant the clock dropped LOW.

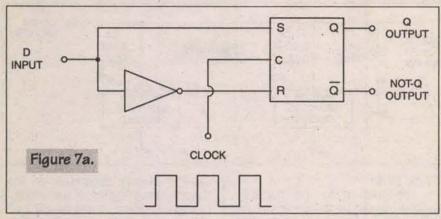
Because of the behavior presented in the above rules, the type-D flip-flop is sometimes called a data latch, or simply latch. The circuit symbol for the type-D flip-flop is shown in

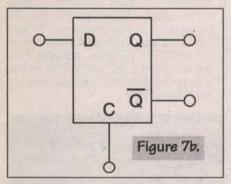






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We can see these rules more graphically in Figures 8A through 8C. Consider first Figure 8A. Recall that the data on the D input will be transferred to the Q output only when the clock terminal is HIGH. At time TO in Figure 8A, the clock goes HIGH, and the D input is LOW, so the Q output is also LOW.

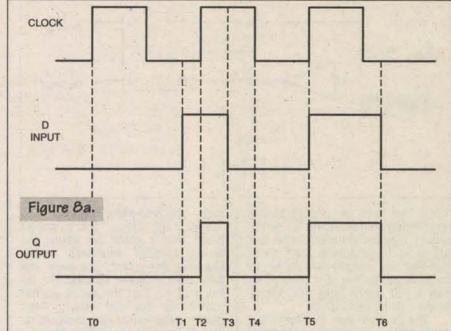
At time T1, the D input goes

HIGH, but cannot affect the Q output because the clock is LOW. The clock goes HIGH at T2, so the output will also goes HIGH. The output pulse exists only for the interval T2-T3 because the HIGH condition on the D input only coincides with that inter-

At time T5, both the D and clock inputs go HIGH, but note that the D line remains HIGH even after the block pulse disappears. By the third rule, then, the output must remain HIGH after the clock pulse passes.

Another situation is described by Figure 8B. In this case, the clock line goes HIGH and remains HIGH. The Q output, therefore, is in an unlatched condition, so will follow the data applied to the D input. Because the D input data is a squarewave, the output will also be a squarewave.

Still another condition is shown in Figure 8C. Again the D input data is a squarewave or pulse train, but



the block is not permanently HIGH in this example. At time T1, both the clock and the D input are HIGH, so the Q output is also HIGH. At time T2, the clock drops LOW, but since D is HIGH at that instant, the output will remain in the HIGH condition. Note that the D input can change at will, without affecting the output, as long as the clock input remains LOW. But at the time T5, the clock goes HIGH, and since the D line is LOW, the output goes LOW also. At time T6, however, the D line goes HIGH, while the clock is still HIGH, so the

output goes HIGH.

Digital Circuit Power Supplies

When I was in grad school, I worked for the university as an electronics technician repairing medical equipment (which paid three times what a graduate teaching assistant made!). One day, there was a knock on my workshop door, and a fellow was standing there with a rat's nest wired homebrew digital project in his



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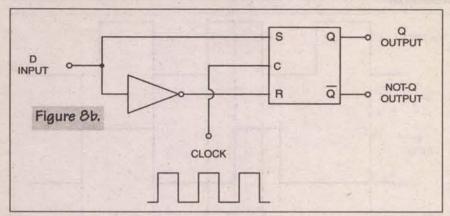


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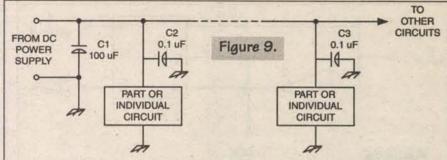
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hands. He was an undergraduate engineering student doing his senior project. "Doctor Frabbitz [not his real name] said you'd help me." Since Prof. Frabbitz basically held the key to my professional future, I allowed as how I just might help this fellow. Besides, he looked forlorn.

The problem was that he had a relatively large digital project built on perf-board with an odd combination of wire-wrap (poorly done), solder-

point-to-point wiring, and tack. "dead bug" chips. There wasn't much that I could do about the (proper wire-wrap wiring wiring would've been best, but even that falls down at higher speeds). The fellow told me that the circuit worked sometimes, but not others. After painstakingly eliminating the possibility of loose solder connections, I noticed that there were a lot of TTL devices on the card and NOT ONE



CAPACITOR!

The solution to the student's problem would be to re-wire the circuit properly, and then use an ade-quate number of bypass capacitors in the DC power supply circuitry. Figure 9 shows the usual approach. At the point where the DC power supply is connected to the board, a high value electrolytic capacitor is used. Different textbooks recommend values anywhere from 100 µF to 1,000 µF for the capacitor (C1 in Figure 9).

The point of using the capacitor is to form a local current reservoir to

> handle instantaneous needs, so I tend to use values in the lower end of the range - (the correct

value is partially dependent on the current re-quirements of the circuit). In addition, there should be a 0.1 uF capacitor at each device or other active circuit. This capacitor should be as close as possible to the V+ terminal on the individual chip. There are small 0.1 µF units available that are quite compact, and will fit in the standard 0.100-inch hole spacings on perf-board. NV

Connections ...

I can be reached by snail mail at P.O. Box 1099, Falls Church, VA 22041, or via E-Mail at CARRJJ@AOL.COM.

Reading List: RF Exposure to Hams (A Balanced Approach)

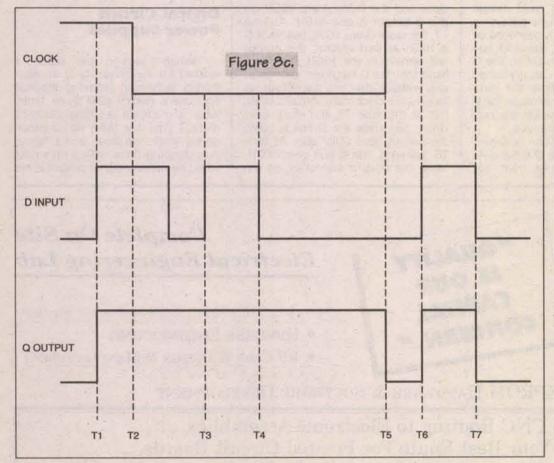
There are some new regulations from the FCC regarding RF radiation exposure from ham rigs. Some hams must file paperwork with the FCC. In addition, if you live near any radio transmitting antenna, you will want to be aware of the problems so that you can guard against affecting your own health.

There is a lot of baseless talk about this subject. Both sides are about equally shrill and equally baseless. The problem is not as severe as the pro side would have you believe, but it's also not a "no problem" situation either. If you are concerned with this potential problem, and how the problem can be cured, then I recommend that you obtain a copy of a

new book published by ARRL.

The ARRL has been active in this issue for quite a long time, and has -- what I believe - is a common sense approach that wisely walks a middle ground (the science is too soft to be certain about either extreme). It is called RF Exposure and You (ISDN 0-87259-662-1) by Ed Hare (WIRFI).

Hare breaks the subject down in a way that ordinary people can understand. The price is \$15.00, which is certainly cheap for that size book (especially one that contains information that may help you retain your health). It is available from ham radio stores, or direct from ARRL at http://www.arrl.org. I also found it listed at Amazon Books, so check out http://www.amazon.com.





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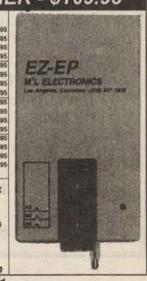
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New Product News

Continued from page 4

AUDIO NOISE REDUCTION SYSTEM

he model NRS1500 noise reduction system assumes that a signal below a predetermined amplitude is noise. It also senses and attenuates noise by measuring the frequency content of the audio signal and then filters noise that occurs above the highest signal frequency. Combining both of these techniques can achieve 25 dB noise reduction by using "single-ended" operation which eliminates the need for the encode decode process.

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vide a high level of effectiveness without sonic artifacts normally associated with noise reduc-

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The NRS1500 is an ideal choice for broad-

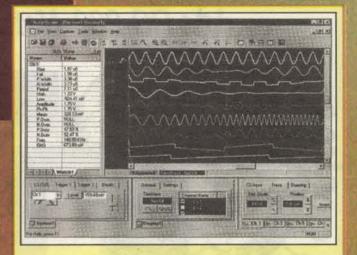


cast studios, commercial recording studios, radio amateurs, and other consumer and professional audio applications while preserving full signal fidelity and transparency.

The NRS1500 is priced at \$189.00.

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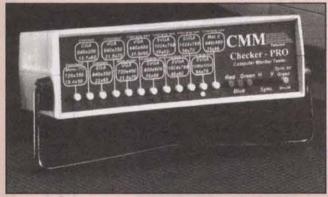
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On the bench, the Checker Pro allows a great deal of flex-ibility. The technician can quickly switch modes using the push buttons, add sync on green, turn off any of the colors, and turn off either horizontal or vertical sync. The Checker Pro provides various test patterns for VGA monitors. Its unique color bar/eight-step gray scale pattern allows color balance and tracking to be quickly evaluated and/or adjusted.

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ENHANCED DACQ-25 PRODUCT LINE

ase2 Computer Corp. announces the availability of the newly redesigned DACQ-25 acquisition module and version 2.0 of its DataMaster analysis software package.

The new DACQ-25 can now be directly connected to many commonly used sensors which previously required custom interface cir-The latest release of DataMaster software offers a fully user configurable interface for displaying and printing data analysis results, perfect for building your own application or experiment.

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over 10,000 samples a second down to one sample every 30 seconds.

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BASE2 COMPUTER CORP. P.O. BOX 950, DEPT. NV PASADENA, CA 91102 818-730-8024 E-MAIL: base2@pacbell.net WEB: www.loop.com/~base2 Norld: RS-232 Network Control Methods and Applications

Mixed Control

by Ryan Sheldon, National Control Devices (404) 244-2432 http://members.aol.com/ncdcat

for the Masses

n the past couple of months, I have discussed Graphic LCDs and how they can be controlled from a Visual Basic application. This month, I want to go back a little further and tie together some of my earlier articles to demonstrate a powerful computer control system.

This month's control system is based on technologies outlined in previous months of "The Computer Controlled World." This article demonstrates how heating and cooling systems can be controlled using the serial port of your desktop computer.

The hardware may seem overkill for the application, but its true capabilities are only limited by software. In effect, increasing the sophistication of the software greatly enhances the capabilities of the hardware. As many users have already discovered, the hardware is relatively universal and is ideally suited for both complicated and simple control applications.

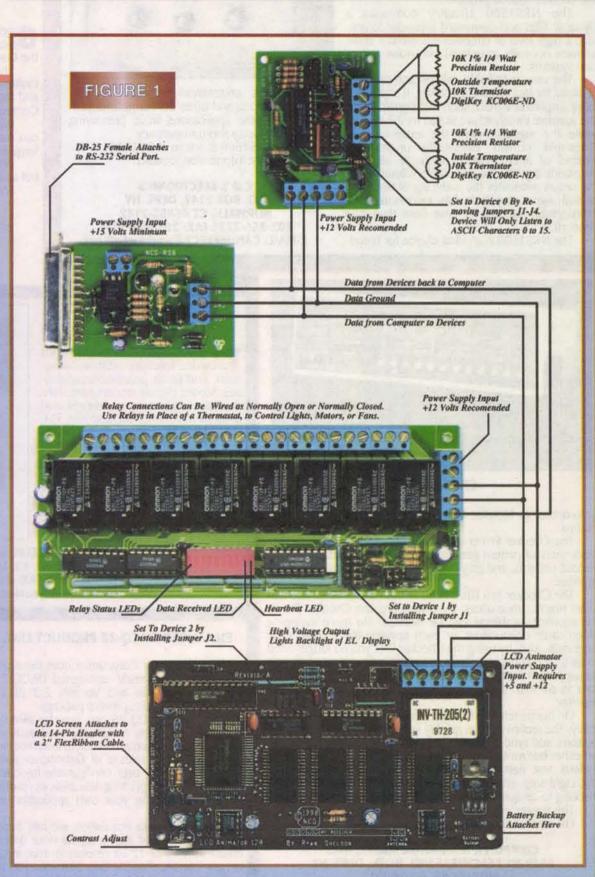
The technologies illustrated are designed to be networkable components of a larger control system such as a desktop PC. A networkable control system such as this offers upgradability and modularity by allowing you to choose the electronics that closely match the needs of your specific application.

Later in this article, I will discuss software issues that make the whole system work. I think you will be surprised at how little software is actually involved. But for now, I want to talk about the networking and its role in our thermostat on steroids.

Rules for RS-232 Networking

If you have been reading my articles, you know that you can attach up to 16 RS-232 networkable devices on a single RS-232 serial port in any combination. Controlling these devices is very easy if you know the following rules:

- Your serial port can send or receive ASCII characters 0 to 255.
- 2) Each device attached to a single RS-232 serial port listens to a range of 16 ASCII characters:
 - a) A device set to address 0 listens to



ASCII characters 0 to 15.

- b) A device set to address 1 listens to ASCII characters 16 to 31.
- A device set to address 2 listens to ASCII characters 32 to 47.
- d) A device set to address 15 listens to

ASCII characters 240 to 255.

The device number is always set in hardware using a set of four jumpers.

4) The device number is always set in software using a number from 0 to 15.

You can mix and match A/D converters, relay drivers, graphic and character LCD displays, as well as input scanners, output modules, and all the other things discussed in previous articles ... all on a single serial port. Just

remember that each device should be set to a different device number and each device number is referred to in software as a number from 0 to 15.

The Project

This month, I want to highlight a simple control system using four devices. The first device is a serial booster used for communicating RS-232 data to and from multiple devices. The second device is an AD8 analogto-digital converter used for reading analog data such as light and temperature levels into the computer. The third device is an R85 relay driver, which is used as a general-purpose software controlled bank of eight switches. And the final device is the LCD Animator 128, used to display status information of the entire system in a remote location.

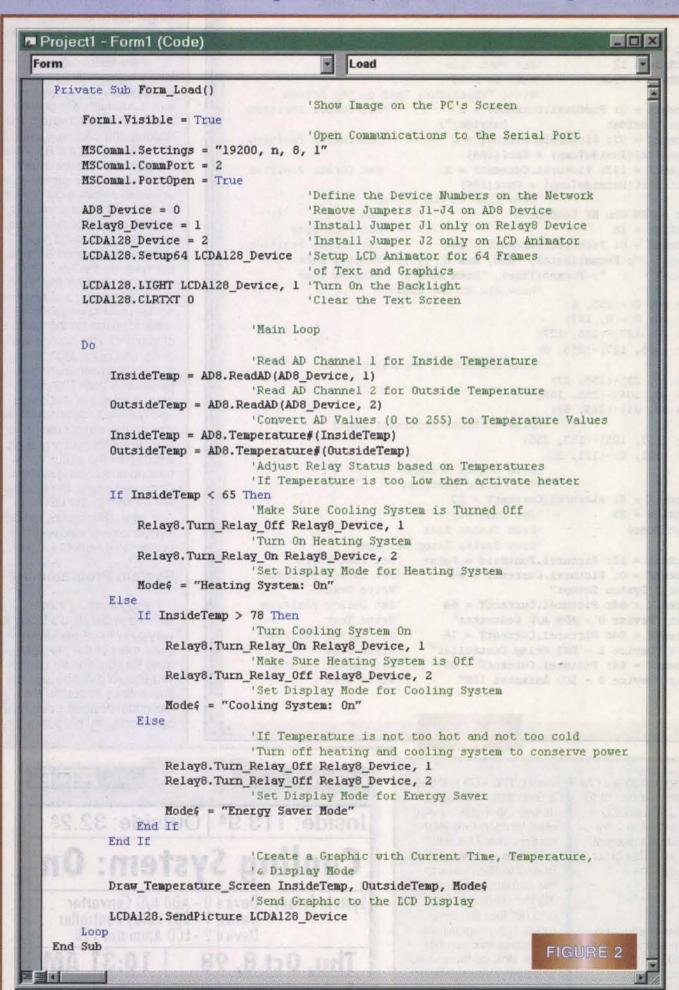
System Wiring

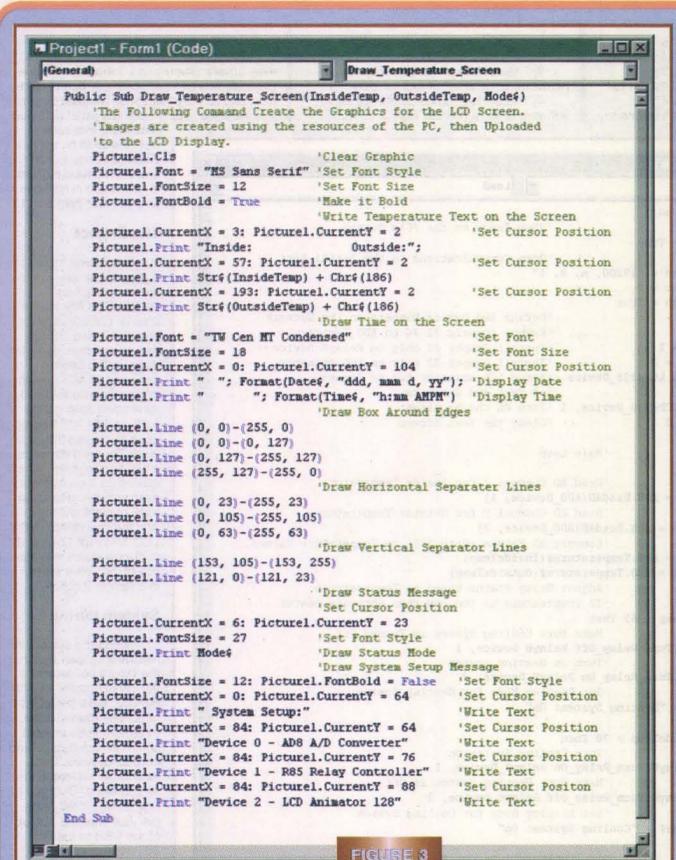
Wiring the system is relatively simple. Attach the DB-25 connector of the serial booster to your RS-232 serial port. Once attached, you will have three terminals used to communicate data to and from all devices. Their function is self-explanatory: Ground, Output, and Input ... pretty simple. Just wire the output of the RSB to the RS-232 input of all three devices. Wire the input of the RSB to the output of the R85 and the AD8 controllers. The LCD Animator 128 does not send data back to the computer, so only two wires are required for complete operation. Please see Figure 1 for a detailed wiring diagram.

System Jumpering

Setting up the jumpers is very simple. All devices should be set to receive data at 19200 baud. The AD8 should

Nuts & Volts Magazine/November 1998





The program will then evaluate the current temperature and determine if the heating or cooling system needs to be turned on. If the current temperature is within an acceptable temperature range, both the heating and cooling systems will be deactivated

If the temperature is too low, a heater will be activated. Similarly, if the temperature is too high, the cooling system will be activated. The heating and cooling system is controlled using the R85 relay controller. This general-purpose relay driver serves as a universal software-controlled switch, perfect for controlling lights, heaters, coolers, fans, and other real-world hardware. Never exceed 5 amps per relay on the R85, or 10 amps per relay on the R810.

At this point, a subroutine will be used to generate a graphic image on the screen of your PC. This screen will make use of the PC's fonts and drawing commands to generate a 256x128 pixel graphic image of the inside and outside temperatures, as well as the current date and time. In addition, the graphic will display the status of the heating and cooling system. Once generated, the graphic will be sent to the LCD Animator 128 display, indicating the current status of the system to a remote location.

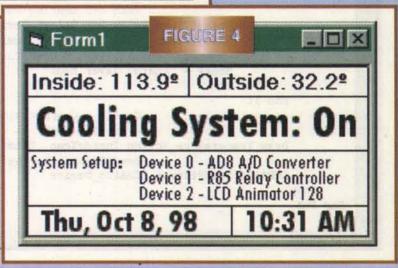
System Programming

Programming these devices under Visual Basic is very easy because I have done most of the programming for you. For simplicity, you should probably use my subroutines to control the individual devices. Later, you can modify my programs for

be set to device 0 by removing jumpers J1 to J4. The R85 relay controller should be set to device 1 by installing jumper J1. The LCD Animator 128 should be set to device 2 by installing jumper J2. See the user's manual of each device for an explicit explanation of jumpers and other hardware options.

Theory of Operation

Once the hardware has been attached to your computer, you will use simple commands to communicate to and from the attached devices. The demonstration program will read the inside and outside temperature using the AD8 analog-to-digital converter. The AD8 will use a thermistor on each of its two input channels to read temperature information. The AD8 will send two numbers (each from 0 to 255) back to the computer representing the current indoor and outdoor temperatures. The program will then pass this number into a look-up table used to convert the numbers 0 to 255 into actual temperatures.







your specific application. If this sounds a little intimidating, let me reassure you that using these devices only requires a few lines of code. So follow along, and I will explain what I have done that makes these devices so easy to

I have been working hard to create a series of modules that allow you to do just about anything with a single line of code. Once modules are loaded into your program, you can easily access my subroutines for controlling each individual device.

For example, three devices will be outlined in this article. So, three modules will be used to control each of the three devices. I have named each of these three control modules to identify the product name of each

For example, if you wanted to talk to the relay driver, you would use the Relay8 module. To turn on a relay, you would use the command:

Relay8.Turn_Relay_On Device, Relay

Device is a number from 0 to 15. Since the relay will be configured in this article as device 1, you could use the following command:

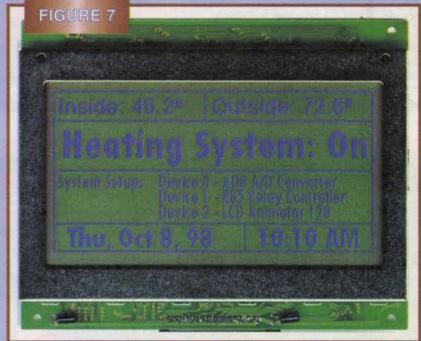
Relay8.Turn_Relay_On 1, Relay

More appropriately, we have defined the constant "Relay_Device = 1" so to control the relay driver, you should use the following statement (just to maintain good programming practice):

Relay8.Turn_Relay_On Relay_Device, Relav

Relay is a number from 1 to 8 identifying which relay should be activated.

Table 1 shows some other example calls to my subroutines, just so you can more easily read what I am doing in the programming



example in Figure 2.

If you don't want to use constants, you can directly send the device number to control each device as shown in Table 2.

Figure 2 illustrates the main program used to read temperature data, control the relays, and the graphic LCD display. The main program starts by opening COM2 at 19.2K baud. Next, device numbers are assigned in software to each of the three attached devices. The AD8 is set to 0, the R85 is set to 1, and the LCD Animator is set to device 2.

The LCD Animator is initialized by calling the Setup64 subroutine within the LCDA128 module. Once initialized, the backlight is turned on and the text layer of the LCD is cleared.

The entire program repeats in an endless cycle within the Do/Loop statements. The cycle begins by reading the inside temperature, then the outside temperature. The Inside/OutsideTemp variables now hold an A/D value from 0 to 255. The AD8.Temperature# function converts this number to an actual temperature value.

The temperature is then evaluated. If the inside temperature is less than 65 degrees, a heater is activated by turning on relay 2. The cooling system is turned off at the same time by turning off relay 1.

If the temperature is greater than 78 degrees, the cooling sys-

tem is turned on by activating relay 1. The heater is turned off by turning off relay 2. If the temperature is within 65 to 78

degrees, both the heating and cooling systems are deactivated. The Mode\$ variable stores the current status of the heating/cooling system in user-readable text. The current Mode will be later displayed on the LCD displays.

Next, the program calls the Draw Temperature Screen subroutine. This subroutine takes advantage TABLE 1

Print AD8.ReadAD AD8_Device, 1 Print AD8.ReadAD AD8_Device, 2 Relay8.Turn_Relay_On Relay_Device, 1

Relay8.Turn_Relay_Off Relay_Device, 7 'Turn off Relay 7 on Relay 8 controller
LCDA128.Light LCDA128_Device, 1

LCDA128.Light LCDA128_Device, 0

Turn off Backlight of LCD Animator 128

Turn off Backlight of LCD Animator 128

'Print A/D Value of Channel 1 on AD8 'Print A/D Value of Channel 2 on AD8

Print AD8.ReadAD 0, 1 Print AD8.ReadAD 0, 2 Relay8.Turn_Relay_On 1, 1 Relay8.Turn_Relay_Off 1, 7 LCDA128.Light 2, 1 LCDA128.Light 2, 0

'Print A/D Value of Channel 1 on AD8, Device 0 'Print A/D Value of Channel 2 on AD8, Device 0 Turn on Relay 1 on Relay 8 controller, Device 1
Turn off Relay 7 on Relay 8 controller, Device 1
Turn on Backlight of LCD Animator 128, Device 2 'Turn off Backlight of LCD Animator 128, Device 2 TABLE 2

of Visual Basic's powerful graphics and text capabilities to generate a 256x128 graphic that holds the current time, date, temperature, and heating/cooling status. Figure 3 illustrates the commands used to generate this screen. Figure 4 shows the graphics on the screen of the PC. Once the graphics are generated, the command

LCDA128.SendPicture LCDA128_Device sends the status information to the LCD Animator 128.

Figure 5 illustrates an example image uploaded to the LCD Animator when the temperature falls too low.

Figure 6 illustrates an example image uploaded to the LCD Animator when the temperature is within an acceptable range.

Figure 7 illustrates an example image uploaded to the LCD Animator when the temperature raises too high.

As you can see, programming these devices is really very simple and the applications are unlimited. Some people are using the R85 relay controller for controlling lights, gates, alarms, and even opening and closing windows. The AD8 is used to read data into the computer such as light and temperature levels. In many cases, people often use mul-

tiple AD8s to read multiple signals into the computer from several locations. The RSB serial booster allows you to attach up to 16 devices to a single serial port at baud rates up to 38.4K over a distance of 800+ feet.

Expandability

You can attach other devices to this network as well. You could add more AD8 A/D converters, LCD Animators, and relay drivers. You could also add new devices to this network such as audio/video switchers, stepper motor controllers, servo motor controllers, and DC motor controllers. Each device needs its own device number in software from 0 to 15, and a corresponding device number set using jumpers J1-J4 on each individual

I hope you have enjoyed this month's

Computer Controlled World. Please feel free to call or write with your questions or comments. All Visual Basic source code is available directly from me, just send me an E-Mail at ncdryan@aol.com and I will return your mail with source code attached. NV

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by Chris Murdock

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